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REFERENCE: U-2525C

PROJECT: 34821

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

**STRUCTURE**  
**SUBSURFACE INVESTIGATION**

COUNTY GUILFORD  
PROJECT DESCRIPTION GREENSBORO EASTERN LOOP  
I-85 BYPASS (-L-)FROM US 29 NORTH OF  
GREENSBORO TO EAST OF LAWDALE DRIVE  
PROJECT DESCRIPTION SITE NO.1, STRUCTURE NO.1  
(BRIDGE NO.1240) ON SR 2526 (SUMMIT AVE)  
OVER GREENSBORO EASTERN LOOP I-85 BYPASS (-L-)

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| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
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| N.C.  | U-2525C                     | 1         | 12           |

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**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
SUBSURFACE INVESTIGATION  
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

**SOIL DESCRIPTION**

SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, *VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6*

**SOIL LEGEND AND AASHTO CLASSIFICATION**

| GENERAL CLASS.                 | GRANULAR MATERIALS (≤ 35% PASSING #200)                               |             |                                 |                         |                         |                         |                         | SILT-CLAY MATERIALS (> 35% PASSING #200) |                         |                         | ORGANIC MATERIALS |  |  |  |
|--------------------------------|---|-------------|---------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|--|-------------------------|-------------------------|-------------------|--|--|--|
|                                | A-1   | A-3         | A-2                             | A-4                     | A-5                     | A-6                     | A-7                     | A-1, A-2                                 | A-3                     | A-4, A-5                | A-6, A-7          |  |  |  |
| GROUP CLASS.                   | A-1-a   | A-1-b       | A-2-4                           | A-2-5                   | A-2-6                   | A-2-7                   |                         |  |                         |                         |                   |  |  |  |
| SYMBOL                         |   |             |                                 |                         |                         |                         |                         |  |                         |                         |                   |  |  |  |
| % PASSING #10 #40 #200         | 50 MX 30 MX 15 MX   | 50 MX 25 MX | 51 MN 35 MX 35 MX               | 40 MX 35 MX             | 41 MN 35 MX             | 41 MN 35 MX             | 40 MX 36 MN             | 41 MN 36 MN                              | 40 MX 36 MN             | 41 MN 36 MN             |                   |  |  |  |
| MATERIAL PASSING #40 LL PI     | - 6 MX  | - NP        | 40 MX 41 MN 10 MX 11 MN         | 40 MX 41 MN 10 MX 11 MN | 40 MX 41 MN 10 MX 11 MN | 40 MX 41 MN 10 MX 11 MN | 40 MX 41 MN 10 MX 11 MN | 40 MX 41 MN 10 MX 11 MN                  | 40 MX 41 MN 10 MX 11 MN | 40 MX 41 MN 10 MX 11 MN |                   |  |  |  |
| GROUP INDEX                    | 0   | 0           | 0                               | 4 MX                    | 8 MX                    | 12 MX                   | 16 MX                   | NO MX                                    |                         |                         |                   |  |  |  |
| USUAL TYPES OF MAJOR MATERIALS | STONE FRAGS. GRAVEL, AND SAND   | FINE SAND   | SILTY OR CLAYEY GRAVEL AND SAND | SILTY SOILS             | CLAYEY SOILS            |                         |                         |  |                         |                         |                   |  |  |  |
| GEN. RATING AS SUBGRADE        | EXCELLENT TO GOOD   |             |                                 | FAIR TO POOR            |                         |                         | FAIR TO POOR            | POOR                                     | UNSATURABLE             |                         |                   |  |  |  |
|                                | PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30 |             |                                 |                         |                         |                         |                         |  |                         |                         |                   |  |  |  |

**CONSISTENCY OR DENSENESS**

| PRIMARY SOIL TYPE                          | COMPACTNESS OR CONSISTENCY                                       | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)     | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) |
|--|--|--|--|
| GENERALLY GRANULAR MATERIAL (NON-COHESIVE) | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE       | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50         | N/A  |
| GENERALLY SILT-CLAY MATERIAL (COHESIVE)    | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30 | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4   |

**TEXTURE OR GRAIN SIZE**

| U.S. STD. SIEVE SIZE OPENING (MM) | 4    | 10   | 40   | 60   | 200   | 270   |
|-----------------------------------|------|------|------|------|-------|-------|
|                                   | 4.75 | 2.00 | 0.42 | 0.25 | 0.075 | 0.053 |
| Boulder (BLDR.)                   |      |      |      |      |       |       |
| Cobble (COB.)                     |      |      |      |      |       |       |
| Gravel (GR.)                      |      |      |      |      |       |       |
| Coarse Sand (CS, SD.)             |      |      |      |      |       |       |
| Fine Sand (F SD.)                 |      |      |      |      |       |       |
| Silt (SL.)                        |      |      |      |      |       |       |
| Clay (CL.)                        |      |      |      |      |       |       |
| GRAIN SIZE                        | 305  | 75   | 2.0  | 0.25 | 0.05  | 0.005 |
| MM                                |      |      |      |      |       |       |
| IN.                               | 12   | 3    |      |      |       |       |

**SOIL MOISTURE - CORRELATION OF TERMS**

| SOIL MOISTURE SCALE (ATTERBERG LIMITS) | FIELD MOISTURE DESCRIPTION | GUIDE FOR FIELD MOISTURE DESCRIPTION                                |
|--|----------------------------|---|
| LL - LIQUID LIMIT                      | - SATURATED - (SAT.)       | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE |
| PL - PLASTIC LIMIT                     | - WET - (W)                | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE               |
| OM - OPTIMUM MOISTURE SHRINKAGE LIMIT  | - MOIST - (M)              | SOLID; AT OR NEAR OPTIMUM MOISTURE                                  |
| SL - SHRINKAGE LIMIT                   | - DRY - (D)                | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE                |

**PLASTICITY**

|                    | PLASTICITY INDEX (PI) | DRY STRENGTH |
|--------------------|-----------------------|--------------|
| NON PLASTIC        | 0-5                   | VERY LOW     |
| SLIGHTLY PLASTIC   | 6-15                  | SLIGHT       |
| MODERATELY PLASTIC | 16-25                 | MEDIUM       |
| HIGHLY PLASTIC     | 26 OR MORE            | HIGH         |

**COLOR**

DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.

**GRADATION**

**WELL GRADED** - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.  
**UNIFORMLY GRADED** - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.  
**GAP-GRADED** - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.

**ANGULARITY OF GRAINS**

THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: **ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.**

**MINERALOGICAL COMPOSITION**

MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.

**COMPRESSIBILITY**

SLIGHTLY COMPRESSIBLE LL < 31  
MODERATELY COMPRESSIBLE LL = 31 - 50  
HIGHLY COMPRESSIBLE LL > 50

**PERCENTAGE OF MATERIAL**

|                         | GRANULAR SOILS | SILT - CLAY SOILS | OTHER MATERIAL       |
|-------------------------|----------------|-------------------|----------------------|
| TRACE OF ORGANIC MATTER | 2 - 3%         | 3 - 5%            | TRACE 1 - 10%        |
| LITTLE ORGANIC MATTER   | 3 - 5%         | 5 - 12%           | LITTLE 10 - 20%      |
| MODERATELY ORGANIC      | 5 - 10%        | 12 - 20%          | SOME 20 - 35%        |
| HIGHLY ORGANIC          | > 10%          | > 20%             | HIGHLY 35% AND ABOVE |

**GROUND WATER**

- WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING
- STATIC WATER LEVEL AFTER 24 HOURS
- PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA
- SPRING OR SEEP

**MISCELLANEOUS SYMBOLS**

- ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION
- SOIL SYMBOL
- ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT
- INFERRED SOIL BOUNDARY
- INFERRED ROCK LINE
- ALLUVIAL SOIL BOUNDARY
- DIP & DIP DIRECTION OF ROCK STRUCTURES
- TEST BORING
- AUGER BORING
- CORE BORING
- MONITORING WELL
- PIEZOMETER INSTALLATION
- SLOPE INDICATOR INSTALLATION
- CONE PENETROMETER TEST
- SOUNDING ROD
- TEST BORING WITH CORE
- SPT N-VALUE

**RECOMMENDATION SYMBOLS**

- UNDERCUT
- SHALLOW UNDERCUT
- UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE
- UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK
- UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL

**ABBREVIATIONS**

- AR - AUGER REFUSAL
- BT - BORING TERMINATED
- CL - CLAY
- CPT - CONE PENETRATION TEST
- CSE - COARSE
- DMT - DILATOMETER TEST
- DPT - DYNAMIC PENETRATION TEST
- e - VOID RATIO
- F - FINE
- FOSS. - FOSSILIFEROUS
- FRAC. - FRACTURED, FRACTURES
- FRAGS. - FRAGMENTS
- HI. - HIGHLY
- MED. - MEDIUM
- MICA - MICACEOUS
- MOD. - MODERATELY
- NP - NON PLASTIC
- ORG. - ORGANIC
- PMT - PRESSUREMETER TEST
- SAP. - SAPROLITIC
- SD. - SAND, SANDY
- SL. - SILT, SILTY
- SLI. - SLIGHTLY
- TCR - TRICONE REFUSAL
- w - MOISTURE CONTENT
- V - VERY
- VST - VANE SHEAR TEST
- WEA. - WEATHERED
- W - UNIT WEIGHT
- W<sub>d</sub> - DRY UNIT WEIGHT
- S - BULK
- SS - SPLIT SPOON
- ST - SHELBY TUBE
- RS - ROCK
- RT - RECOMPACTED TRIAXIAL
- CBR - CALIFORNIA BEARING RATIO

**EQUIPMENT USED ON SUBJECT PROJECT**

- DRILL UNITS:
  - CME-45C
  - CME-55
  - CME-550
  - VANE SHEAR TEST
  - PORTABLE HOIST
  - 
  -
- ADVANCING TOOLS:
  - CLAY BITS
  - 6" CONTINUOUS FLIGHT AUGER
  - 8" HOLLOW AUGERS
  - HARD FACED FINGER BITS
  - TUNG-CARBIDE INSERTS
  - CASING  W/ ADVANCER
  - TRICONE  STEEL TEETH
  - TRICONE  TUNG-CARB.
  - CORE BIT
  - HILTI CORE DRILL (PVMT)
- HAMMER TYPE:
  - AUTOMATIC  MANUAL
- CORE SIZE:
  - B  -H
  - N
- HAND TOOLS:
  - POST HOLE DIGGER
  - HAND AUGER
  - SOUNDING ROD
  - VANE SHEAR TEST

**ROCK DESCRIPTION**

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

- WEATHERED ROCK (WR)  
NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.
- CRYSTALLINE ROCK (CR)  
FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.
- NON-CRYSTALLINE ROCK (NCR)  
FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.
- COASTAL PLAIN SEDIMENTARY ROCK (CP)  
COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.

**WEATHERING**

- FRESH** - ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.
- VERY SLIGHT (IV SLI.)** - ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.
- SLIGHT (SLI.)** - ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.
- MODERATE (MOD.)** - SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.
- MODERATELY SEVERE (MOD. SEV.)** - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. *IF TESTED, WOULD YIELD SPT REFUSAL*
- SEVERE (SEV.)** - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF*
- VERY SEVERE (IV SEV.)** - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF*
- COMPLETE** - ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

**ROCK HARDNESS**

- VERY HARD** - CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.
- HARD** - CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.
- MODERATELY HARD** - CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.
- MEDIUM HARD** - CAN BE GROUDED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.
- SOFT** - CAN BE GROUDED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.
- VERY SOFT** - CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

**FRACTURE SPACING**

| TERM             | SPACING             | TERM                | THICKNESS         |
|------------------|---------------------|---------------------|-------------------|
| VERY WIDE        | MORE THAN 10 FEET   | VERY THICKLY BEDDED | 4 FEET            |
| WIDE             | 3 TO 10 FEET        | THICKLY BEDDED      | 1.5 - 4 FEET      |
| MODERATELY CLOSE | 1 TO 3 FEET         | THINLY BEDDED       | 0.16 - 1.5 FEET   |
| CLOSE            | 0.16 TO 1 FOOT      | VERY THINLY BEDDED  | 0.03 - 0.16 FEET  |
| VERY CLOSE       | LESS THAN 0.16 FEET | THICKLY LAMINATED   | 0.008 - 0.03 FEET |
|                  |                     | THINLY LAMINATED    | < 0.008 FEET      |

**INDURATION**

- FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.**
- FRIABLE** - RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.
- MODERATELY INDURATED** - GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.
- INDURATED** - GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.
- EXTREMELY INDURATED** - SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

**TERMS AND DEFINITIONS**

- ALLUVIUM (ALLUV.)** - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
- AQUIFER** - A WATER BEARING FORMATION OR STRATA.
- ARENACEOUS** - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
- ARGILLACEOUS** - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
- ARTESIAN** - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
- CALCAREOUS (CALC.)** - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
- COLLUVIUM** - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
- CORE RECOVERY (REC.)** - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
- DIKE** - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
- DIP** - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
- DIP DIRECTION (DIP AZIMUTH)** - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
- FAULT** - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
- FISSILE** - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
- FLOAT** - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOADED FROM PARENT MATERIAL.
- FLOOD PLAIN (FP)** - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
- FORMATION (FM)** - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
- JOINT** - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
- LEDGE** - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
- LENS** - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
- MOTTLED (MOT.)** - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
- PERCHED WATER** - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
- RESIDUAL (RES.) SOIL** - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
- ROCK QUALITY DESIGNATION (ROD)** - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
- SAPROLITE (SAP.)** - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
- SILL** - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
- SLICKENSIDE** - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
- STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)** - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
- STRATA CORE RECOVERY (SREC.)** - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
- STRATA ROCK QUALITY DESIGNATION (SROD)** - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
- TOPSOIL (TS.)** - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

BENCH MARK: BL-70 - N:872842, E:1780684

ELEVATION: 860.80 FEET

**NOTES:**

FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.

RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.

GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.

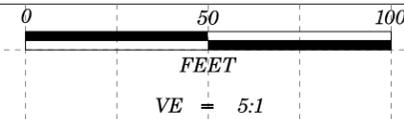
GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.

SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

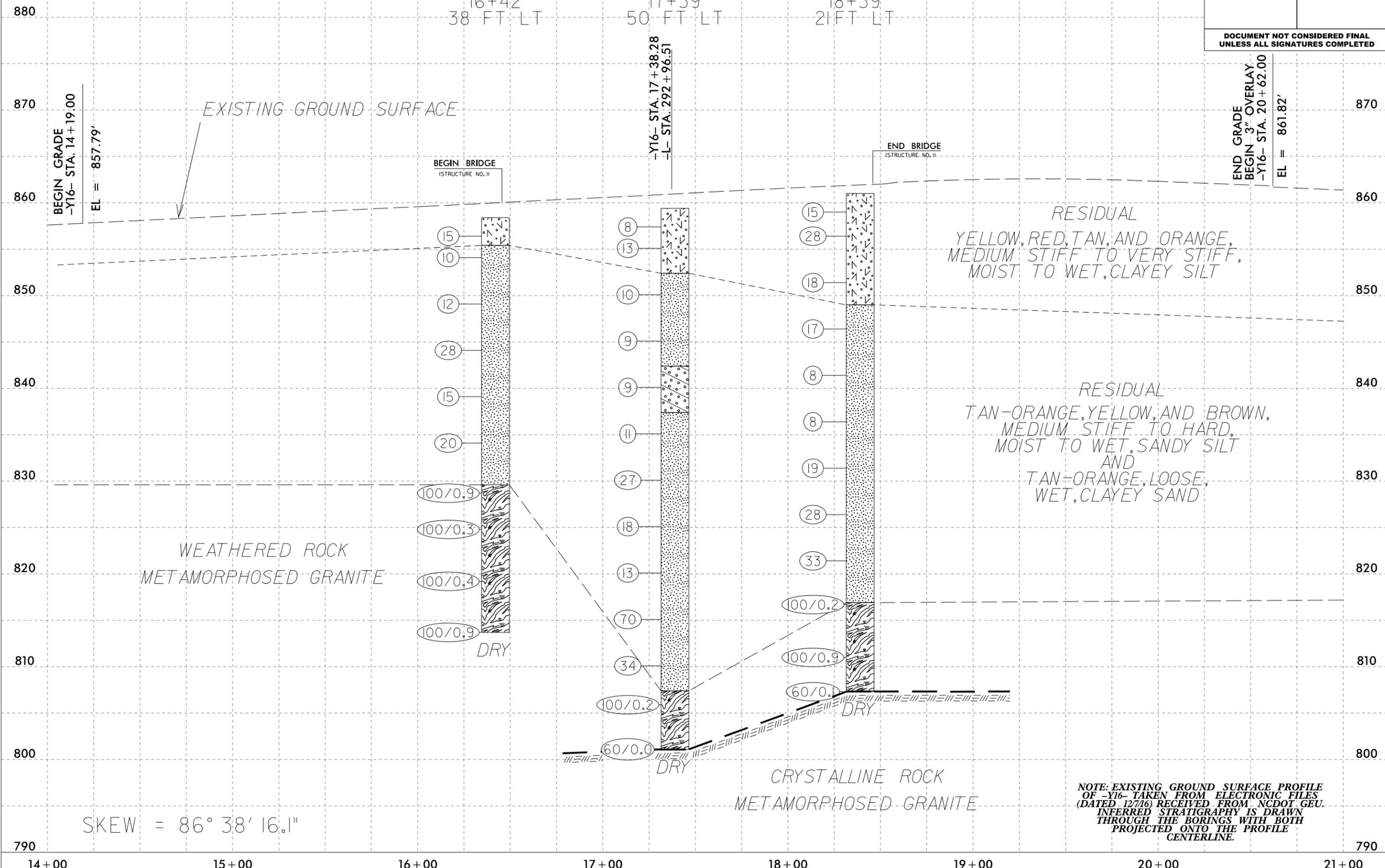


5/14/99

# PROFILE ALONG -Y16- CENTERLINE (STRUCTURE NO. 1)



|  |                       |
|--|-----------------------|
| PROJECT REFERENCE NO.<br><b>U-2525C</b>                          | SHEET NO.<br><b>4</b> |
| ROADWAY DESIGN ENGINEER  | HYDRAULICS ENGINEER   |
| DOCUMENT NOT CONSIDERED FINAL<br>UNLESS ALL SIGNATURES COMPLETED |                       |



SKIEW = 86° 38' 16.1"

**NOTE: EXISTING GROUND SURFACE PROFILE OF -Y16- TAKEN FROM ELECTRONIC FILES (DATED 12/16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILE CENTERLINE.**

14+00 15+00 16+00 17+00 18+00 19+00 20+00 21+00

6/23/16

875 75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75 875

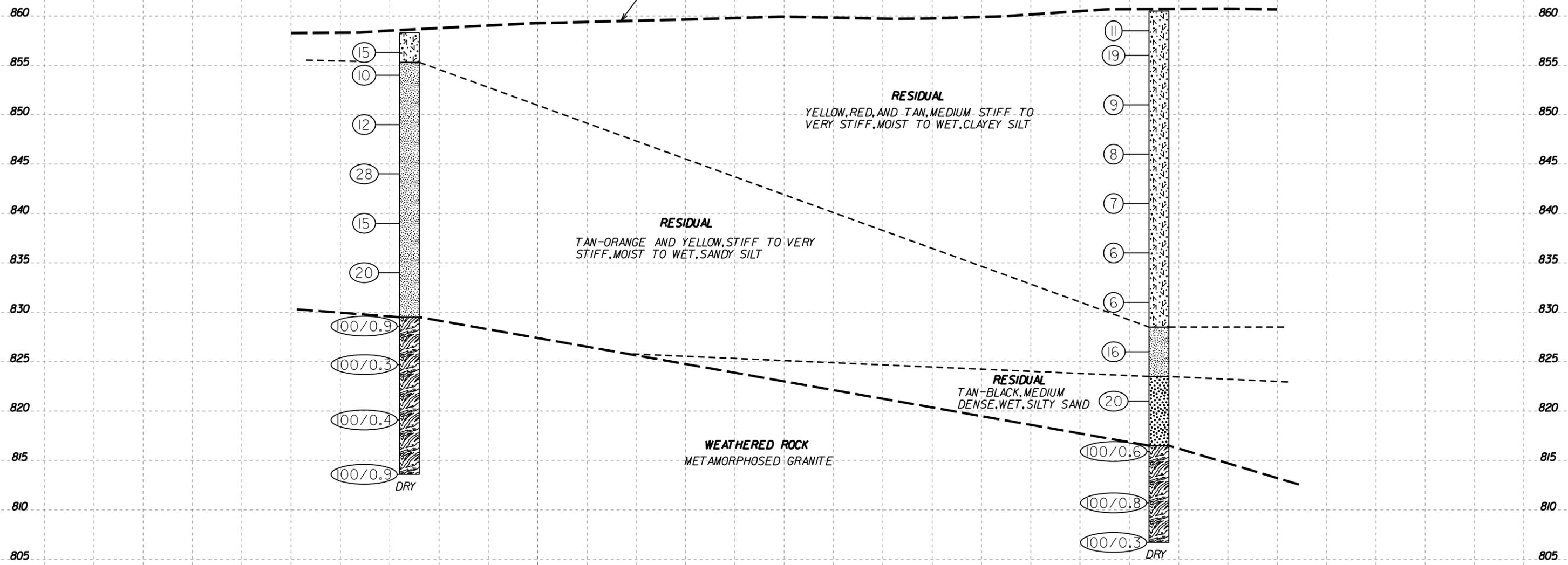
# CROSS SECTION ALONG END BENT NO.1 OF STRUCTURE NO.1

EBI-A  
16+42  
38 FT LT

EBI-B  
16+41  
38 FT RT



EXISTING GROUND SURFACE



16+45  
-Y16-

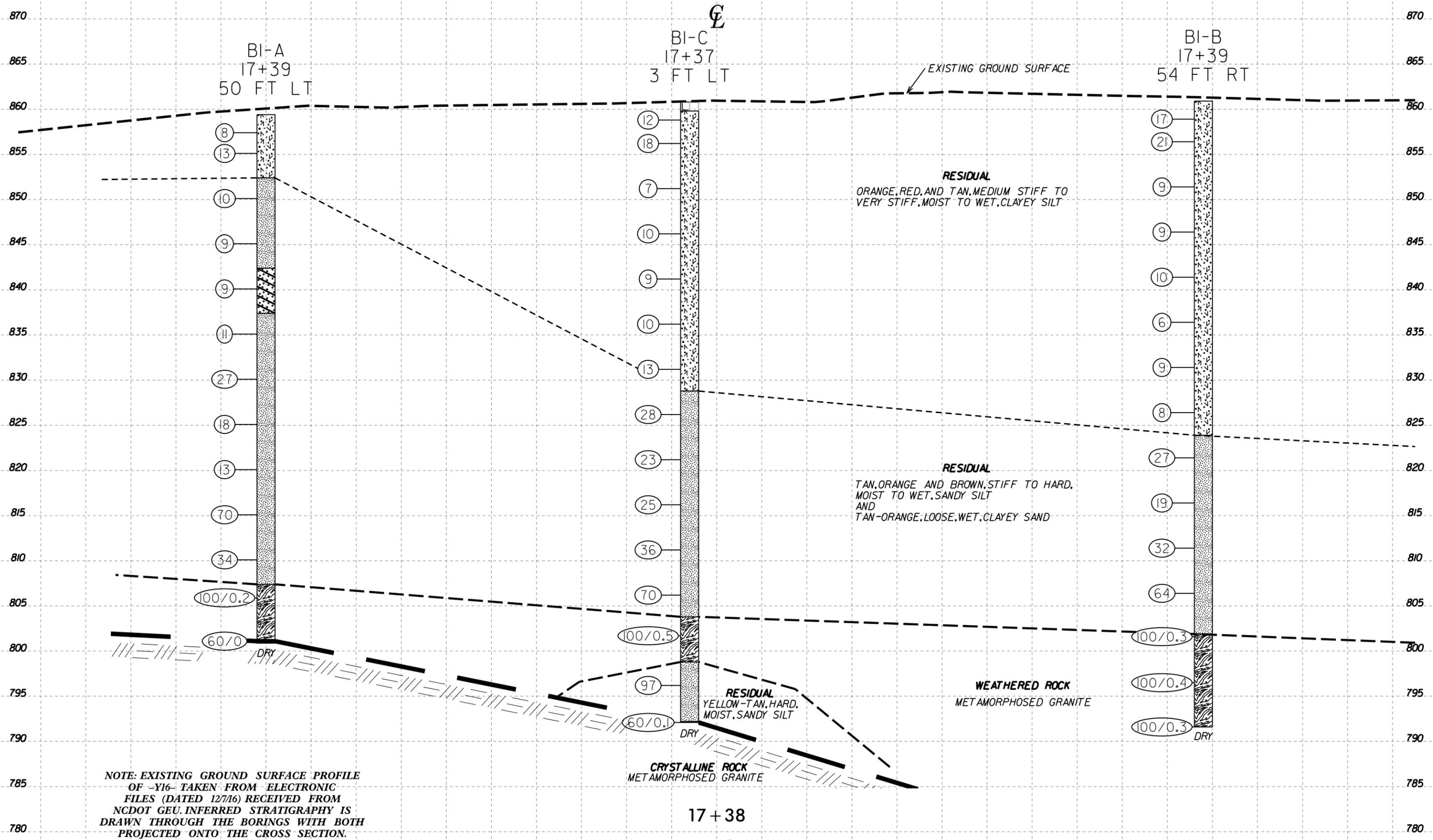
NOTE: EXISTING GROUND SURFACE PROFILE OF -Y16- TAKEN FROM ELECTRONIC FILES (DATED 12/7/16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.

780 785 790 795 800 805 810 815 820 825 830 835 840 845 850 855 860 865 870 875

6/23/16

875 75 70 65 60 55 50 45 40 35 30 25 20 15 10 5 0 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75 875

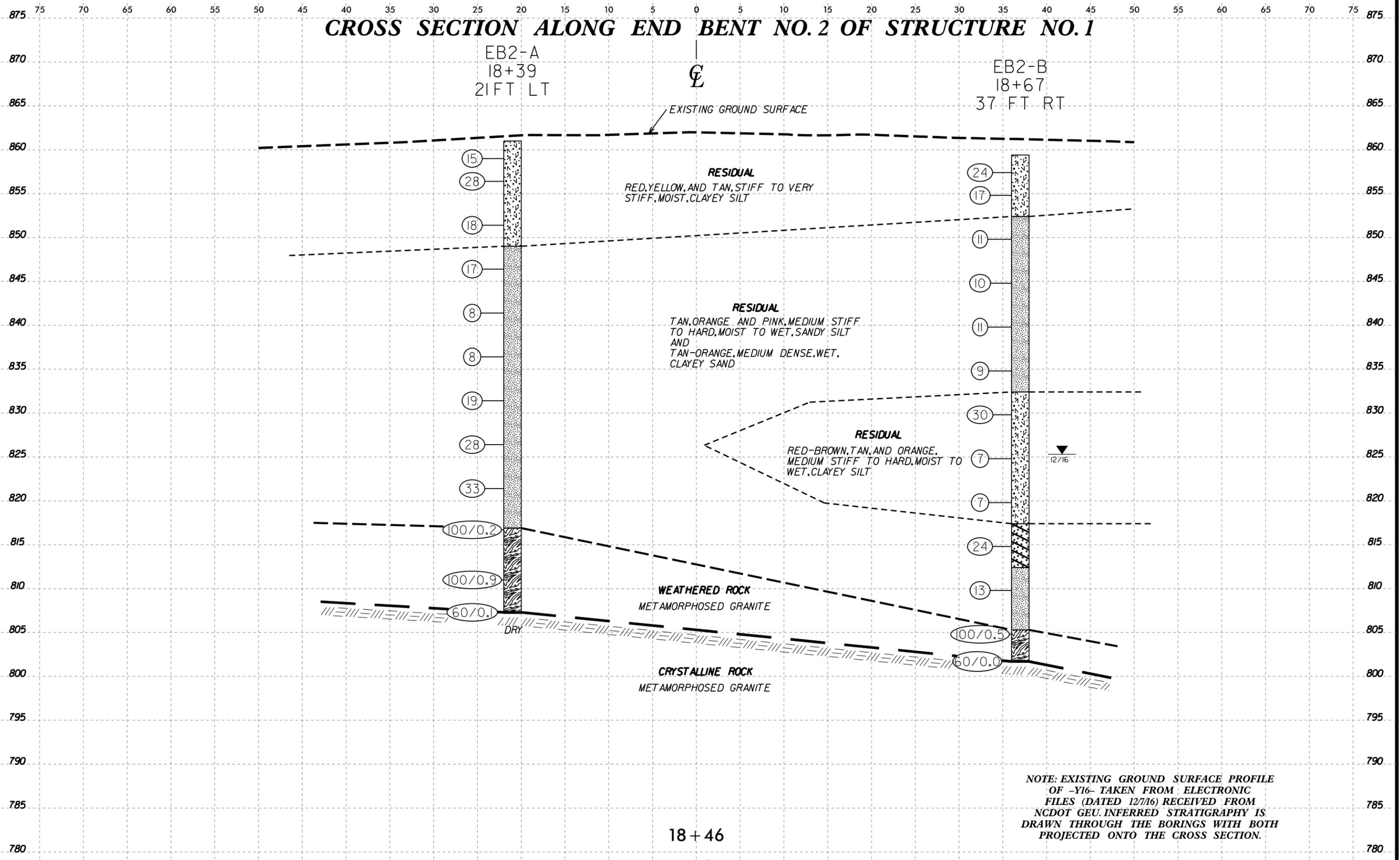
# CROSS SECTION ALONG BENT NO.1 OF STRUCTURE NO.1



NOTE: EXISTING GROUND SURFACE PROFILE OF -Y16- TAKEN FROM ELECTRONIC FILES (DATED 12/7/16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.

780 785 790 795 800 805 810 815 820 825 830 835 840 845 850 855 860 865 870 875

6/23/16



18+46  
-Y16-

NOTE: EXISTING GROUND SURFACE PROFILE OF -Y16- TAKEN FROM ELECTRONIC FILES (DATED 12/16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.



# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |       | GEOLOGIST C.T. Tang, EI |                 |    |    |     |           |         |                           |            |     |   |
|---|-----------------|---------------------|-------------------------|---------------------|-------|-------------------------|-----------------|----|----|-----|-----------|---------|---------------------------|------------|-----|---|
| SITE DESCRIPTION Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                 |                     |                         |                     |       |                         | GROUND WTR (ft) |    |    |     |           |         |                           |            |     |   |
| BORING NO. B1-A   |                 | STATION 17+39       |                         | OFFSET 50 ft LT     |       | ALIGNMENT -Y16-         |                 |    |    |     |           |         |                           |            |     |   |
| COLLAR ELEV. 859.4 ft   |                 | TOTAL DEPTH 58.3 ft |                         | NORTHING 872,949    |       | EASTING 1,780,670       |                 |    |    |     |           |         |                           |            |     |   |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |                 |                     | DRILL METHOD Mud Rotary |                     |       | HAMMER TYPE Automatic   |                 |    |    |     |           |         |                           |            |     |   |
| DRILLER J. Anderson   |                 | START DATE 12/13/16 |                         | COMP. DATE 12/13/16 |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |         |                           |            |     |   |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG MOI | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |     |   |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |         |                           |            |     |   |
| 860   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |         |                           | 859.4      | 0.0 | GROUND SURFACE  |
|   | 858.4           | 1.0                 | 1                       | 2                   | 6     |                         |                 |    |    |     |           |         |                           |            |     | <b>RESIDUAL</b><br>Orange, Red and Tan, Clayey Silt, with Trace Roots |
| 855   | 856.1           | 3.3                 | 3                       | 5                   | 8     |                         |                 |    |    |     |           |         |                           |            |     |   |
|   | 851.1           | 8.3                 | 3                       | 5                   | 5     |                         |                 |    |    |     |           |         |                           |            |     | Tan and Orange, Sandy Silt  |
| 850   | 846.1           | 13.3                | 4                       | 4                   | 5     |                         |                 |    |    |     |           |         |                           |            |     |   |
| 845   | 841.1           | 18.3                | 3                       | 4                   | 5     |                         |                 |    |    |     |           |         |                           |            |     | Tan-Orange, Clayey Sand   |
| 840   | 836.1           | 23.3                | 3                       | 5                   | 6     |                         |                 |    |    |     |           |         |                           |            |     | Tan, Brown and Yellow, Sandy Silt (Saprolite)                         |
| 835   | 831.1           | 28.3                | 13                      | 12                  | 15    |                         |                 |    |    |     |           |         |                           |            |     |   |
| 830   | 826.1           | 33.3                | 6                       | 9                   | 9     |                         |                 |    |    |     |           |         |                           |            |     |   |
| 825   | 821.1           | 38.3                | 3                       | 4                   | 9     |                         |                 |    |    |     |           |         |                           |            |     |   |
| 820   | 816.1           | 43.3                | 15                      | 29                  | 41    |                         |                 |    |    |     |           |         |                           |            |     |   |
| 815   | 811.1           | 48.3                | 6                       | 13                  | 21    |                         |                 |    |    |     |           |         |                           |            |     |   |
| 810   | 806.1           | 53.3                | 100/0.2                 |                     |       |                         |                 |    |    |     |           |         |                           |            |     |   |
| 805   | 801.1           | 58.3                | 60/0                    |                     |       |                         |                 |    |    |     |           |         |                           |            |     |   |
|   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |         |                           |            |     |   |

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |       | GEOLOGIST C.T. Tang, EI |                 |    |    |     |           |         |                           |            |  |       |  |
|---|-----------------|---------------------|-------------------------|---------------------|-------|-------------------------|-----------------|----|----|-----|-----------|---------|---------------------------|------------|--|-------|--|
| SITE DESCRIPTION Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                 |                     |                         |                     |       |                         | GROUND WTR (ft) |    |    |     |           |         |                           |            |  |       |  |
| BORING NO. B1-B   |                 | STATION 17+39       |                         | OFFSET 54 ft RT     |       | ALIGNMENT -Y16-         |                 |    |    |     |           |         |                           |            |  |       |  |
| COLLAR ELEV. 860.9 ft   |                 | TOTAL DEPTH 69.3 ft |                         | NORTHING 872,886    |       | EASTING 1,780,754       |                 |    |    |     |           |         |                           |            |  |       |  |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |                 |                     | DRILL METHOD Mud Rotary |                     |       | HAMMER TYPE Automatic   |                 |    |    |     |           |         |                           |            |  |       |  |
| DRILLER J. Anderson   |                 | START DATE 12/14/16 |                         | COMP. DATE 12/14/16 |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |         |                           |            |  |       |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG MOI | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |  |       |  |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |         |                           |            |  |       |  |
| 865   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |         |                           |            |  | 860.9 | 0.0  |
|   | 859.9           | 1.0                 | 2                       | 5                   | 12    |                         |                 |    |    |     |           |         |                           |            |  |       | <b>RESIDUAL</b><br>Red, Tan, and Orange, Clayey Silt, with Trace Roots on Top 2.5' |
| 860   | 857.4           | 3.5                 | 4                       | 9                   | 12    |                         |                 |    |    |     |           |         |                           |            |  |       |  |
|   | 852.4           | 8.5                 | 3                       | 4                   | 5     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 855   | 847.4           | 13.5                | 2                       | 4                   | 5     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 850   | 842.4           | 18.5                | 3                       | 4                   | 6     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 845   | 837.4           | 23.5                | 3                       | 3                   | 3     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 840   | 832.4           | 28.5                | 2                       | 4                   | 5     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 835   | 827.4           | 33.5                | 2                       | 3                   | 5     |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 830   | 822.4           | 38.5                | 6                       | 12                  | 15    |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 825   | 817.4           | 43.5                | 6                       | 7                   | 12    |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 820   | 812.4           | 48.5                | 7                       | 13                  | 19    |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 815   | 807.4           | 53.5                | 11                      | 21                  | 43    |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 810   | 802.4           | 58.5                | 37                      | 100/0.3             |       |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 805   | 797.4           | 63.5                | 31                      | 100/0.4             |       |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 800   | 792.4           | 68.5                | 45                      | 100/0.3             |       |                         |                 |    |    |     |           |         |                           |            |  |       |  |
| 795   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |         |                           |            |  |       |  |
|   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |         |                           |            |  |       |  |

NCDOT BORE DOUBLE U2525C\_GEO\_BRD0004\_BH.GPJ NC\_DOT\_GDT\_10/3/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

|   |                     |                         |                         |
|---|---------------------|-------------------------|-------------------------|
| WBS 34821.1.1   | TIP U-2525C         | COUNTY GUILFORD         | GEOLOGIST C.T. Tang, EI |
| SITE DESCRIPTION Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                     |                         | GROUND WTR (ft)         |
| BORING NO. B1-C   | STATION 17+37       | OFFSET 3 ft LT          | ALIGNMENT -Y16-         |
| COLLAR ELEV. 860.8 ft   | TOTAL DEPTH 68.7 ft | NORTHING 872,918        | EASTING 1,780,707       |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |                     | DRILL METHOD Mud Rotary | HAMMER TYPE Automatic   |
| DRILLER J. Anderson   | START DATE 12/20/16 | COMP. DATE 12/20/16     | SURFACE WATER DEPTH N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |      |  |
|-----------|-----------------|------------|------------|-------|-------|----------------|----|----|----|-----|-----------|-----|---------------------------|------------|------|--|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     | ELEV. (ft)                | DEPTH (ft) |      |  |
| 865       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
| 860       | 859.8           | 1.0        | 3          | 6     | 6     |                |    |    |    |     |           |     |                           | 860.8      | 0.0  | GROUND SURFACE   |
|           |                 |            |            |       |       |                |    |    |    |     |           |     |                           | 859.8      | 1.0  | Asphalt (6 inches) over Concrete (6 inches)  |
|           | 857.2           | 3.6        | 5          | 8     | 10    | 12             |    |    |    |     |           |     |                           |            |      | <b>RESIDUAL</b><br>Yellow-Brown and Red-Tan, Clayey Silt, with Trace Rock Fragments and Some Mica                          |
| 855       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 852.2           | 8.6        | 3          | 3     | 4     | 7              |    |    |    |     |           |     |                           |            |      |  |
| 850       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 847.2           | 13.6       | 4          | 5     | 5     | 10             |    |    |    |     |           |     |                           |            |      |  |
| 845       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 842.2           | 18.6       | 3          | 4     | 5     | 9              |    |    |    |     |           |     |                           |            |      |  |
| 840       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 837.2           | 23.6       | 3          | 4     | 6     | 10             |    |    |    |     |           |     |                           |            |      |  |
| 835       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 832.2           | 28.6       | 3          | 5     | 8     | 13             |    |    |    |     |           |     |                           |            |      |  |
| 830       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 827.2           | 33.6       | 9          | 12    | 16    | 28             |    |    |    |     |           |     |                           | 828.8      | 32.0 | Brown and Tan, Sandy Silt  |
| 825       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 822.2           | 38.6       | 10         | 10    | 13    | 23             |    |    |    |     |           |     |                           |            |      |  |
| 820       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 817.2           | 43.6       | 6          | 12    | 13    | 25             |    |    |    |     |           |     |                           |            |      |  |
| 815       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 812.2           | 48.6       | 13         | 14    | 22    | 36             |    |    |    |     |           |     |                           |            |      |  |
| 810       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 807.2           | 53.6       | 18         | 34    | 36    | 70             |    |    |    |     |           |     |                           |            |      |  |
| 805       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 802.2           | 58.6       | 100/0.5    |       |       | 100/0.5        |    |    |    |     |           |     |                           | 803.8      | 57.0 | <b>WEATHERED ROCK</b><br>(Metamorphosed Granite)   |
| 800       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 797.2           | 63.6       | 31         | 42    | 55    | 97             |    |    |    |     |           |     |                           | 798.8      | 62.0 | <b>RESIDUAL</b><br>Yellow-Tan, Sandy Silt  |
| 795       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 792.2           | 68.6       | 60/0.1     |       |       | 60/0.1         |    |    |    |     |           |     |                           | 792.2      | 68.6 | <b>CRYSTALLINE ROCK</b><br>(Metamorphosed Granite)   |
|           |                 |            |            |       |       |                |    |    |    |     |           |     |                           | 792.1      | 68.7 | Boring Terminated with Standard Penetration Test Refusal at Elevation 792.1 ft in Crystalline Rock (Metamorphosed Granite) |

NCDOT BORE DOUBLE U2525C\_GEO\_BRD0004\_BH.GPJ NC\_DOT\_GDT\_10/3/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

|  |                            |                                |                                |
|--|----------------------------|--------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.1   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD         | <b>GEOLOGIST</b> C.T. Tang, EI |
| <b>SITE DESCRIPTION</b> Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                            |                                | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> EB2-A  | <b>STATION</b> 18+39       | <b>OFFSET</b> 21 ft LT         | <b>ALIGNMENT</b> -Y16-         |
| <b>COLLAR ELEV.</b> 861.0 ft   | <b>TOTAL DEPTH</b> 53.7 ft | <b>NORTHING</b> 873,012        | <b>EASTING</b> 1,780,750       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> BRI8284 45 Track 89% 02/26/2016  |                            | <b>DRILL METHOD</b> Mud Rotary | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> J. Anderson   | <b>START DATE</b> 12/13/16 | <b>COMP. DATE</b> 12/13/16     | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |         |        | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |  |
|-----------|-----------------|------------|------------|---------|--------|----------------|----|----|----|-----|-----------|-----|---------------------------|--|
|           |                 |            | 0.5ft      | 0.5ft   | 0.5ft  | 0              | 25 | 50 | 75 | 100 |           |     |                           |  |
| 865       |                 |            |            |         |        |                |    |    |    |     |           |     |                           |  |
| 860       | 860.0           | 1.0        | 2          | 7       | 8      |                |    |    |    |     |           |     |                           | 861.0 GROUND SURFACE 0.0   |
| 855       | 857.4           | 3.6        | 5          | 9       | 19     |                |    |    |    |     |           |     |                           | <b>RESIDUAL</b><br>Yellow and Red, Clayey Silt, with Trace Roots   |
| 850       | 852.4           | 8.6        | 3          | 7       | 11     |                |    |    |    |     |           |     |                           |  |
| 845       | 847.4           | 13.6       | 5          | 7       | 10     |                |    |    |    |     |           |     |                           | 849.0 Tan, Orange and Black, Sandy Silt, with Trace Rock Fragments 12.0  |
| 840       | 842.4           | 18.6       | 3          | 3       | 5      |                |    |    |    |     |           |     |                           |  |
| 835       | 837.4           | 23.6       | 2          | 3       | 5      |                |    |    |    |     |           |     |                           |  |
| 830       | 832.4           | 28.6       | 5          | 8       | 11     |                |    |    |    |     |           |     |                           |  |
| 825       | 827.4           | 33.6       | 9          | 11      | 17     |                |    |    |    |     |           |     |                           |  |
| 820       | 822.4           | 38.6       | 14         | 17      | 16     |                |    |    |    |     |           |     |                           |  |
| 815       | 817.4           | 43.6       | 62         | 100/0.2 |        |                |    |    |    |     |           |     |                           | 816.9 WEATHERED ROCK (Metamorphosed Granite) 44.1  |
| 810       | 812.4           | 48.6       | 24         | 40      | 60/0.4 |                |    |    |    |     |           |     |                           |  |
|           | 807.4           | 53.6       | 60/0.1     |         |        |                |    |    |    |     |           |     |                           | 807.3 CRYSTALLINE ROCK (Metamorphosed Granite) 53.6<br>Boring Terminated with Standard Penetration Test Refusal at Elevation 807.3 ft in Crystalline Rock (Metamorphosed Granite) 53.7 |

|  |                            |                                |                                |
|--|----------------------------|--------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.1   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD         | <b>GEOLOGIST</b> C.T. Tang, EI |
| <b>SITE DESCRIPTION</b> Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                            |                                | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> EB2-B  | <b>STATION</b> 18+67       | <b>OFFSET</b> 37 ft RT         | <b>ALIGNMENT</b> -Y16-         |
| <b>COLLAR ELEV.</b> 859.4 ft   | <b>TOTAL DEPTH</b> 57.7 ft | <b>NORTHING</b> 873,007        | <b>EASTING</b> 1,780,814       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> BRI8284 45 Track 89% 02/26/2016  |                            | <b>DRILL METHOD</b> Mud Rotary | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> J. Anderson   | <b>START DATE</b> 12/14/16 | <b>COMP. DATE</b> 12/14/16     | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |   |
|-----------|-----------------|------------|------------|-------|-------|----------------|----|----|----|-----|-----------|-----|---------------------------|---|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     |                           |   |
| 860       |                 |            |            |       |       |                |    |    |    |     |           |     |                           | 859.4 GROUND SURFACE 0.0  |
| 855       | 858.4           | 1.0        | 7          | 10    | 14    |                |    |    |    |     |           |     |                           | <b>RESIDUAL</b><br>Red and Tan, Clayey Silt   |
| 850       | 855.8           | 3.6        | 4          | 7     | 10    |                |    |    |    |     |           |     |                           | 852.4 Tan-Pink and Tan-Orange, Sandy Silt 7.0   |
| 845       | 850.8           | 8.6        | 3          | 5     | 6     |                |    |    |    |     |           |     |                           |   |
| 840       | 845.8           | 13.6       | 3          | 4     | 6     |                |    |    |    |     |           |     |                           |   |
| 835       | 840.8           | 18.6       | 4          | 4     | 7     |                |    |    |    |     |           |     |                           |   |
| 830       | 835.8           | 23.6       | 3          | 4     | 5     |                |    |    |    |     |           |     |                           |   |
| 825       | 830.8           | 28.6       | 8          | 13    | 17    |                |    |    |    |     |           |     |                           | 832.4 Red-Brown, Tan and Orange, Clayey Silt, with Some Mica and Quartz Fragments 27.0  |
| 820       | 825.8           | 33.6       | 3          | 3     | 4     |                |    |    |    |     |           |     |                           |   |
| 815       | 820.8           | 38.6       | 2          | 3     | 4     |                |    |    |    |     |           |     |                           |   |
| 810       | 815.8           | 43.6       | 5          | 8     | 16    |                |    |    |    |     |           |     |                           | 817.4 Tan-Orange, Clayey Sand 42.0  |
| 805       | 810.8           | 48.6       | 4          | 5     | 8     |                |    |    |    |     |           |     |                           | 812.4 Tan, Sandy Silt 47.0  |
|           | 805.8           | 53.6       | 39         | 100   |       |                |    |    |    |     |           |     |                           | 805.3 WEATHERED ROCK (Metamorphosed Granite) 54.1   |
|           | 801.7           | 57.7       | 60/0.0     |       |       |                |    |    |    |     |           |     |                           | 801.7 Boring Terminated with Standard Penetration Test Refusal at Elevation 801.7 ft on Crystalline Rock (Metamorphosed Granite) 57.7 |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG004\_BH.GPJ NC\_DOT\_GDT\_10/3/17

## SITE PHOTOGRAPHS



PHOTOGRAPH #1: VIEW OF -Y16- LOOKING NORTH FROM NEAR CENTER OF PROPOSED BRIDGE.



PHOTOGRAPH 2: VIEW OF -Y16- LOOKING SOUTH FROM NEAR CENTER OF PROPOSED BRIDGE.

REFERENCE: U-2525C

PROJECT: 34821

**CONTENTS**

| <u>SHEET NO.</u> | <u>DESCRIPTION</u>   |
|------------------|----------------------|
| 1                | TITLE SHEET          |
| 2                | LEGEND (SOIL & ROCK) |
| 3                | SITE PLAN            |
| 4-5              | WALL ENVELOPES       |
| 6-9              | BORING LOGS          |

**STATE OF NORTH CAROLINA**  
 DEPARTMENT OF TRANSPORTATION  
 DIVISION OF HIGHWAYS  
 GEOTECHNICAL ENGINEERING UNIT

**RETAINING WALL**  
**SUBSURFACE INVESTIGATION**

COUNTY GUILFORD  
 PROJECT DESCRIPTION STRUCTURE NO.1 ON SR2526  
(SUMMIT AVE.) OVER GREENSBORO EASTERN  
LOOP I-86 BYPASS (-L-)  
 SITE DESCRIPTION RETAINING WALLS AT  
END BENT NO.1 AND NO.2

| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
|-------|-----------------------------|-----------|--------------|
| N.C.  | U-2525C                     | 1         | 9            |

**CAUTION NOTICE**

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PERSONNEL

C. TANG, EI

CAROLINA DRILLING

J. ANDERSON

J. COLLINS

INVESTIGATED BY C. TANG, EI

DRAWN BY D. BROWN, PE

CHECKED BY E. MAYR, PE

SUBMITTED BY D. BROWN, PE

DATE OCTOBER 2017



DocuSigned by:

Donald W. Brown Jr.

10/9/2017

SIGNATURE

DATE

C06817F5F770411

**DOCUMENT NOT CONSIDERED FINAL  
UNLESS ALL SIGNATURES COMPLETED**

**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**  
**SUBSURFACE INVESTIGATION**  
**SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

**SOIL DESCRIPTION**  
 SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 208, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, *VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6*

**SOIL LEGEND AND AASHTO CLASSIFICATION**

| GENERAL CLASS.                 | GRANULAR MATERIALS (≤ 35% PASSING #200) |             |                                 |              |              |             |              | SILT-CLAY MATERIALS (> 35% PASSING #200) |             |             | ORGANIC MATERIALS                                       |                      |            |          |
|--------------------------------|---|-------------|---------------------------------|--------------|--------------|-------------|--------------|--|-------------|-------------|---|----------------------|------------|----------|
|                                | A-1                                     | A-3         | A-2                             | A-2-4        | A-2-5        | A-2-6       | A-2-7        | A-4                                      | A-5         | A-6         | A-7   | A-1, A-2             | A-3        | A-4, A-5 |
| GROUP CLASS.                   | A-1-a                                   | A-1-b       | A-2-4                           | A-2-5        | A-2-6        | A-2-7       | A-4          | A-5                                      | A-6         | A-7         | A-1, A-2  | A-3                  | A-4, A-5   | A-6, A-7 |
| SYMBOL                         |   |             |                                 |              |              |             |              |  |             |             |   |                      |            |          |
| % PASSING #10 #40 #200         | 50 MX 30 MX 15 MX                       | 50 MX 25 MX | 51 MN 35 MX                     | 35 MX        | 35 MX        | 35 MX       | 36 MN        | 36 MN                                    | 36 MN       | 36 MN       | GRANULAR SOILS  | SILT-CLAY SOILS      | MUCK, PEAT |          |
| MATERIAL PASSING #40 LL PI     | -                                       | -           | 40 MX 10 MX                     | 41 MN 10 MX  | 40 MX 11 MN  | 41 MN 11 MN | 40 MX 11 MN  | 41 MN 11 MN                              | 40 MX 11 MN | 41 MN 11 MN | SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER | HIGHLY ORGANIC SOILS |            |          |
| GROUP INDEX                    | 0                                       | 0           | 0                               | 4 MX         | 8 MX         | 12 MX       | 16 MX        | NO MX                                    |             |             |   |                      |            |          |
| USUAL TYPES OF MAJOR MATERIALS | STONE FRAGS. GRAVEL, AND SAND           | FINE SAND   | SILTY OR CLAYEY GRAVEL AND SAND | SILTY SOILS  | CLAYEY SOILS |             |              |  |             |             |   |                      |            |          |
| GEN. RATING AS SUBGRADE        | EXCELLENT TO GOOD                       |             |                                 | FAIR TO POOR |              |             | FAIR TO POOR | POOR                                     | UNSATURABLE |             |   |                      |            |          |

PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30

**CONSISTENCY OR DENSENESS**

| PRIMARY SOIL TYPE                          | COMPACTNESS OR CONSISTENCY                                       | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)     | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) |
|--|--|--|--|
| GENERALLY GRANULAR MATERIAL (NON-COHESIVE) | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE       | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50         | N/A  |
| GENERALLY SILT-CLAY MATERIAL (COHESIVE)    | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30 | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4   |

**TEXTURE OR GRAIN SIZE**

| U.S. STD. SIEVE SIZE OPENING (MM) | 4    | 10   | 40   | 60   | 200   | 270   |
|-----------------------------------|------|------|------|------|-------|-------|
|                                   | 4.75 | 2.00 | 0.42 | 0.25 | 0.075 | 0.053 |
| BOULDER (BLDR.)                   |      |      |      |      |       |       |
| COBBLE (COB.)                     |      |      |      |      |       |       |
| GRAVEL (GR.)                      |      |      |      |      |       |       |
| COARSE SAND (CS, SD.)             |      |      |      |      |       |       |
| FINE SAND (F SD.)                 |      |      |      |      |       |       |
| SILT (SL.)                        |      |      |      |      |       |       |
| CLAY (CL.)                        |      |      |      |      |       |       |
| GRAIN SIZE                        | 305  | 75   | 2.0  | 0.25 | 0.05  | 0.005 |
| MM                                |      |      |      |      |       |       |
| IN.                               | 12   | 3    |      |      |       |       |

**SOIL MOISTURE - CORRELATION OF TERMS**

| SOIL MOISTURE SCALE (ATTERBERG LIMITS) | FIELD MOISTURE DESCRIPTION | GUIDE FOR FIELD MOISTURE DESCRIPTION                                |
|--|----------------------------|---|
| LL - LIQUID LIMIT                      | - SATURATED - (SAT.)       | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE |
| PL - PLASTIC LIMIT                     | - WET - (W)                | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE               |
| OM - OPTIMUM MOISTURE SHRINKAGE LIMIT  | - MOIST - (M)              | SOLID; AT OR NEAR OPTIMUM MOISTURE                                  |
| SL - SHRINKAGE LIMIT                   | - DRY - (D)                | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE                |

**PLASTICITY**

| NON PLASTIC        | PLASTICITY INDEX (PI) | DRY STRENGTH |
|--------------------|-----------------------|--------------|
| SLIGHTLY PLASTIC   | 0-5                   | VERY LOW     |
| MODERATELY PLASTIC | 6-15                  | SLIGHT       |
| HIGHLY PLASTIC     | 16-25                 | MEDIUM       |
|                    | 26 OR MORE            | HIGH         |

**COLOR**

DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.

**GRADATION**

WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.  
 UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.  
 GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.

**ANGULARITY OF GRAINS**

THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.

**MINERALOGICAL COMPOSITION**

MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.

**COMPRESSIBILITY**

SLIGHTLY COMPRESSIBLE LL < 31  
 MODERATELY COMPRESSIBLE LL = 31 - 50  
 HIGHLY COMPRESSIBLE LL > 50

**PERCENTAGE OF MATERIAL**

|                         | GRANULAR SOILS | SILT - CLAY SOILS | OTHER MATERIAL       |
|-------------------------|----------------|-------------------|----------------------|
| TRACE OF ORGANIC MATTER | 2 - 3%         | 3 - 5%            | TRACE 1 - 10%        |
| LITTLE ORGANIC MATTER   | 3 - 5%         | 5 - 12%           | LITTLE 10 - 20%      |
| MODERATELY ORGANIC      | 5 - 10%        | 12 - 20%          | SOME 20 - 35%        |
| HIGHLY ORGANIC          | > 10%          | > 20%             | HIGHLY 35% AND ABOVE |

**GROUND WATER**

WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING  
 STATIC WATER LEVEL AFTER 24 HOURS  
 PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA  
 SPRING OR SEEP

**MISCELLANEOUS SYMBOLS**

ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION  
 SOIL SYMBOL  
 ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT  
 INFERRED SOIL BOUNDARY  
 INFERRED ROCK LINE  
 ALLUVIAL SOIL BOUNDARY

DIP & DIP DIRECTION OF ROCK STRUCTURES  
 TEST BORING  
 AUGER BORING  
 CORE BORING  
 MONITORING WELL  
 PIEZOMETER INSTALLATION

SLOPE INDICATOR INSTALLATION  
 CONE PENETROMETER TEST  
 SOUNDING ROD  
 TEST BORING WITH CORE  
 SPT N-VALUE

**RECOMMENDATION SYMBOLS**

UNDERCUT  
 SHALLOW UNDERCUT  
 UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE  
 UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK  
 UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL

**ABBREVIATIONS**

AR - AUGER REFUSAL  
 BT - BORING TERMINATED  
 CL - CLAY  
 CPT - CONE PENETRATION TEST  
 CSE - COARSE  
 DMT - DILATOMETER TEST  
 DPT - DYNAMIC PENETRATION TEST  
 e - VOID RATIO  
 F - FINE  
 FOSS. - FOSSILIFEROUS  
 FRAC. - FRACTURED, FRACTURES  
 FRAGS. - FRAGMENTS  
 HI. - HIGHLY

MED. - MEDIUM  
 MICA - MICACEOUS  
 MOD. - MODERATELY  
 NP - NON PLASTIC  
 ORG. - ORGANIC  
 PMT - PRESSUREMETER TEST  
 SAP. - SAPROLITIC  
 SD. - SAND, SANDY  
 SL. - SILTY, SILTY  
 SLI. - SLIGHTLY  
 TCR - TRICONE REFUSAL  
 w - MOISTURE CONTENT  
 V - VERY

VST - VANE SHEAR TEST  
 WEA. - WEATHERED  
 UG - UNIT WEIGHT  
 UG - DRY UNIT WEIGHT

**SAMPLE ABBREVIATIONS**  
 S - BULK  
 SS - SPLIT SPOON  
 ST - SHELBY TUBE  
 RS - ROCK  
 RT - RECOMPACTED TRIAXIAL  
 CBR - CALIFORNIA BEARING RATIO

**EQUIPMENT USED ON SUBJECT PROJECT**

DRILL UNITS:  
 CME-45C  
 CME-55  
 CME-550  
 VANE SHEAR TEST  
 PORTABLE HOIST

ADVANCING TOOLS:  
 CLAY BITS  
 6" CONTINUOUS FLIGHT AUGER  
 8" HOLLOW AUGERS  
 HARD FACED FINGER BITS  
 TUNG-CARBIDE INSERTS  
 CASING  W/ ADVANCER  
 TRICONE \* STEEL TEETH  
 TRICONE \* TUNG-CARB.  
 CORE BIT  
 HILTI CORE DRILL (PVMT)

HAMMER TYPE:  
 AUTOMATIC  MANUAL

CORE SIZE:  
 -B  -H  
 -N

HAND TOOLS:  
 POST HOLE DIGGER  
 HAND AUGER  
 SOUNDING ROD  
 VANE SHEAR TEST

**ROCK DESCRIPTION**

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

**WEATHERED ROCK (WR)**  
 NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.

**CRYSTALLINE ROCK (CR)**  
 FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.

**NON-CRYSTALLINE ROCK (NCR)**  
 FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.

**COASTAL PLAIN SEDIMENTARY ROCK (CP)**  
 COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.

**WEATHERING**

FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.

VERY SLIGHT (V SL.) ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.

SLIGHT (SL.) ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.

MODERATE (MOD.) SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.

MODERATELY SEVERE (MOD. SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. *IF TESTED, WOULD YIELD SPT REFUSAL*

SEVERE (SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF*

VERY SEVERE (V SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF*

COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

**ROCK HARDNESS**

VERY HARD CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.

HARD CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.

MODERATELY HARD CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.

MEDIUM HARD CAN BE GROUDED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.

SOFT CAN BE GROUDED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.

VERY SOFT CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

| FRACTURE SPACING |                     | BEDDING             |                   |
|------------------|---------------------|---------------------|-------------------|
| TERM             | SPACING             | TERM                | THICKNESS         |
| VERY WIDE        | MORE THAN 10 FEET   | VERY THICKLY BEDDED | 4 FEET            |
| WIDE             | 3 TO 10 FEET        | THICKLY BEDDED      | 1.5 - 4 FEET      |
| MODERATELY CLOSE | 1 TO 3 FEET         | THINLY BEDDED       | 0.16 - 1.5 FEET   |
| CLOSE            | 0.16 TO 1 FOOT      | VERY THINLY BEDDED  | 0.03 - 0.16 FEET  |
| VERY CLOSE       | LESS THAN 0.16 FEET | THICKLY LAMINATED   | 0.008 - 0.03 FEET |
|                  |                     | THINLY LAMINATED    | < 0.008 FEET      |

**INDURATION**

FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.

FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.

MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.

INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.

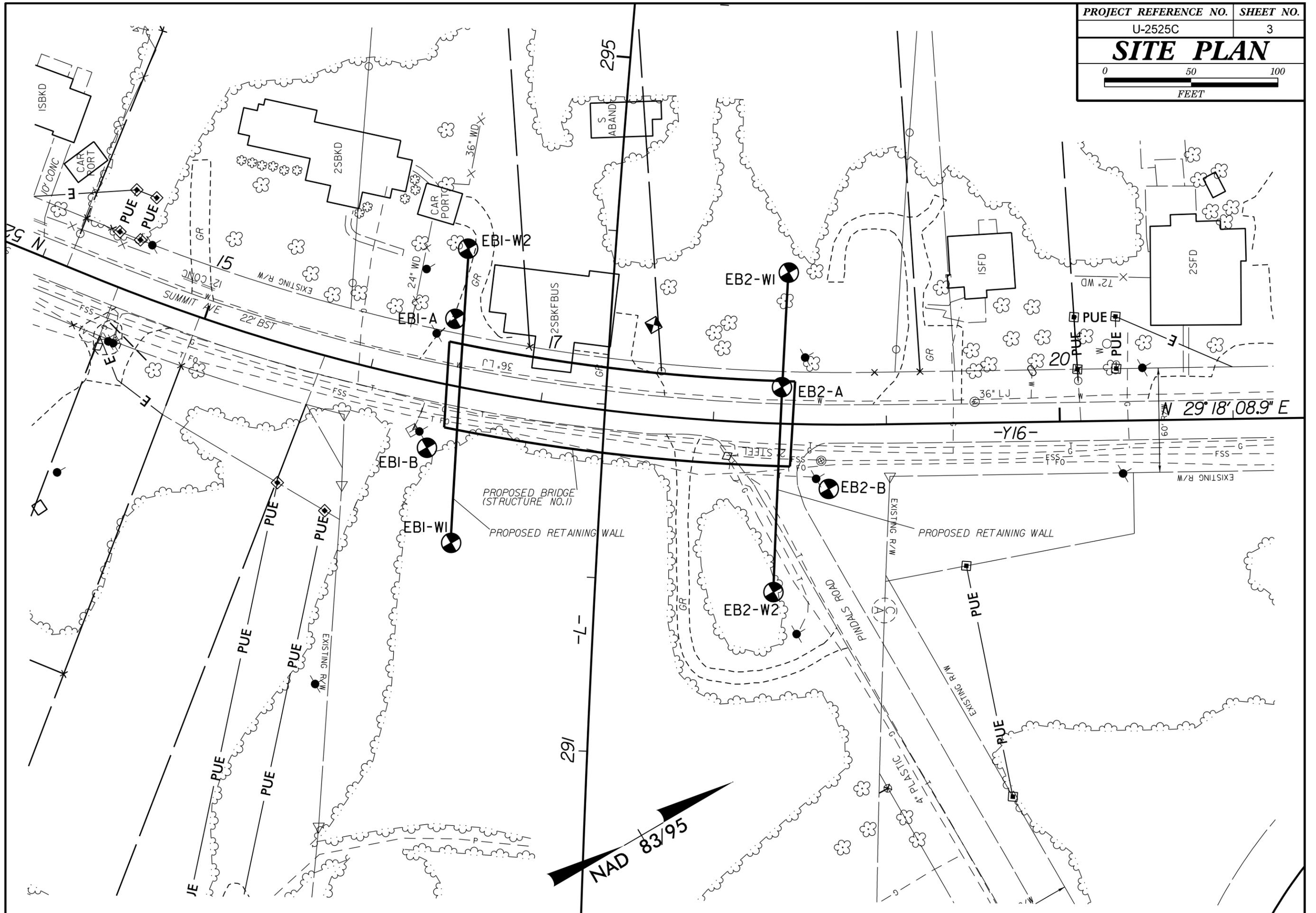
EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

**TERMS AND DEFINITIONS**

**ALLUVIUM (ALLUV.)** - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.  
**AQUIFER** - A WATER BEARING FORMATION OR STRATA.  
**ARENACEOUS** - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.  
**ARGILLACEOUS** - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.  
**ARTESIAN** - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.  
**CALCAREOUS (CALC.)** - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.  
**COLLUVIUM** - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.  
**CORE RECOVERY (REC.)** - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.  
**DIKE** - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.  
**DIP** - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.  
**DIP DIRECTION (DIP AZIMUTH)** - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.  
**FAULT** - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.  
**FISSILE** - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  
**FLOAT** - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOADED FROM PARENT MATERIAL.  
**FLOOD PLAIN (FP)** - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.  
**FORMATION (FM)** - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.  
**JOINT** - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.  
**LEDGE** - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.  
**LENS** - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.  
**MOTTLED (MOT.)** - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.  
**PERCHED WATER** - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.  
**RESIDUAL (RES.) SOIL** - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.  
**ROCK QUALITY DESIGNATION (ROD)** - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.  
**SAPROLITE (SAP.)** - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.  
**SILL** - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.  
**SLICKENSIDE** - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.  
**STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)** - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.  
**STRATA CORE RECOVERY (SREC.)** - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.  
**STRATA ROCK QUALITY DESIGNATION (SROD)** - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.  
**TOPSOIL (TS.)** - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

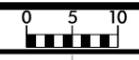
ELEVATION: 860.80 FEET

**NOTES:**



6/23/16

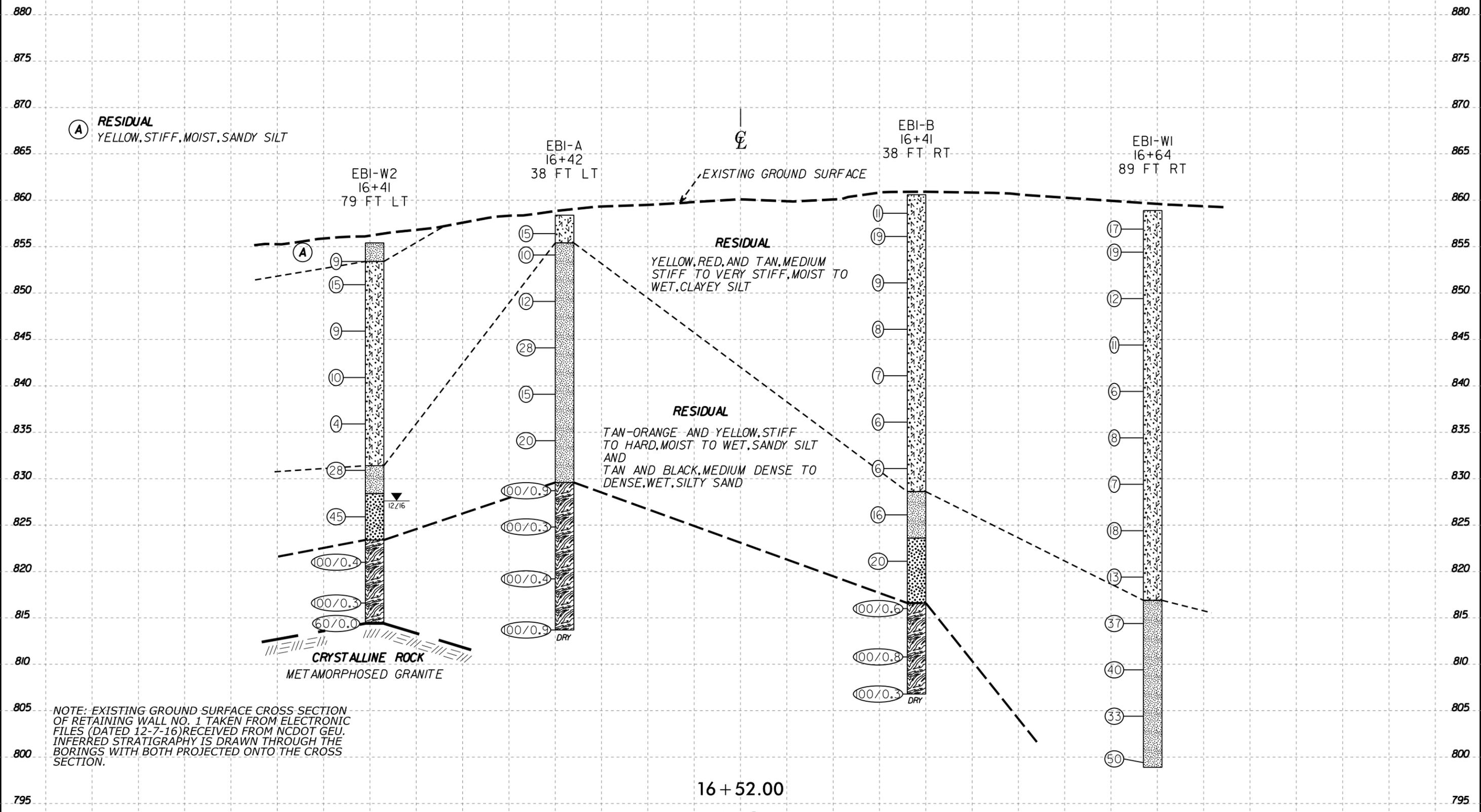
VE = 2:1



|                     |           |
|---------------------|-----------|
| PROJ. REFERENCE NO. | SHEET NO. |
| U-2525C             | 4         |

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

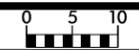
### CROSS SECTION ALONG RETAINING WALL AT END BENT NO. 1



NOTE: EXISTING GROUND SURFACE CROSS SECTION OF RETAINING WALL NO. 1 TAKEN FROM ELECTRONIC FILES (DATED 12-7-16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.

6/23/16

VE = 2:1



|                     |           |
|---------------------|-----------|
| PROJ. REFERENCE NO. | SHEET NO. |
| U-2525C             | 5         |

150 140 130 120 110 100 90 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150

### CROSS SECTION ALONG RETAINING WALL AT END BENT NO. 2

NOTE: EXISTING GROUND SURFACE CROSS SECTION OF RETAINING WALL NO. 2 TAKEN FROM ELECTRONIC FILES (DATED 12-7-16) RECEIVED FROM NCDOT GEU. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE CROSS SECTION.

(A) BROWN, VERY STIFF TO HARD, MOIST, CLAYEY SILT

EB2-W1  
18+41  
87 FT LT

EB2-A  
18+39  
21 FT LT

EB2-B  
18+67  
37 FT RT

EB2-W2  
18+38  
97 FT RT

EXISTING GROUND SURFACE

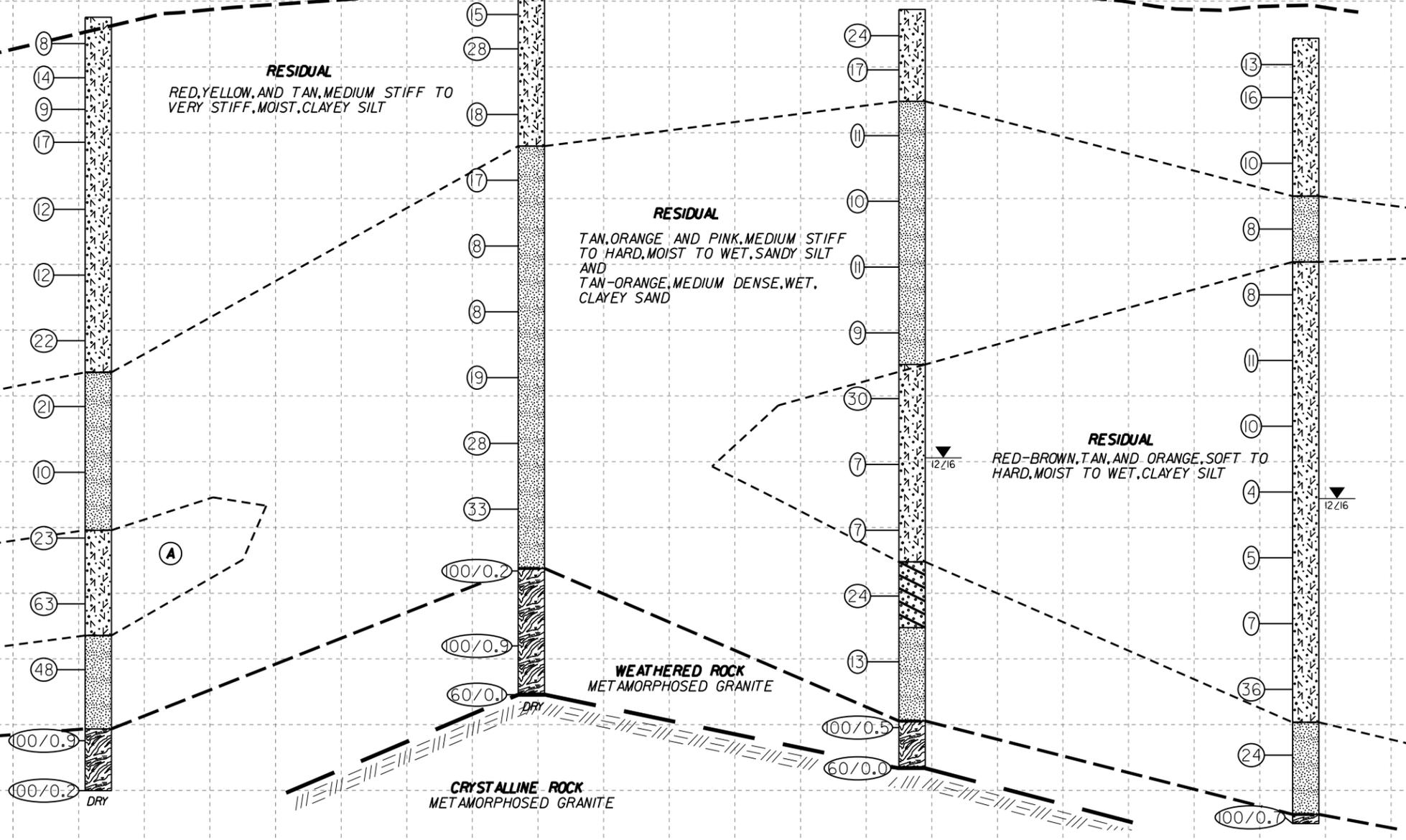
**RESIDUAL**  
RED, YELLOW, AND TAN, MEDIUM STIFF TO VERY STIFF, MOIST, CLAYEY SILT

**RESIDUAL**  
TAN, ORANGE, AND PINK, MEDIUM STIFF TO HARD, MOIST TO WET, SANDY SILT AND TAN-ORANGE, MEDIUM DENSE, WET, CLAYEY SAND

**RESIDUAL**  
RED-BROWN, TAN, AND ORANGE, SOFT TO HARD, MOIST TO WET, CLAYEY SILT

**WEATHERED ROCK**  
METAMORPHOSED GRANITE

**CRYSTALLINE ROCK**  
METAMORPHOSED GRANITE



18 + 39.00





# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |        | GEOLOGIST C.T. Tang, EI |                 |    |    |     |           |     |                           |       |  |
|---|-----------------|---------------------|-------------------------|---------------------|--------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|-------|--|
| SITE DESCRIPTION Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                 |                     |                         |                     |        |                         | GROUND WTR (ft) |    |    |     |           |     |                           |       |  |
| BORING NO. EB2-A  |                 | STATION 18+39       |                         | OFFSET 21 ft LT     |        | ALIGNMENT -Y16-         |                 |    |    |     |           |     |                           |       |  |
| COLLAR ELEV. 861.0 ft   |                 | TOTAL DEPTH 53.7 ft |                         | NORTHING 873,012    |        | EASTING 1,780,750       |                 |    |    |     |           |     |                           |       |  |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |                 |                     | DRILL METHOD Mud Rotary |                     |        | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |       |  |
| DRILLER J. Anderson   |                 | START DATE 12/13/16 |                         | COMP. DATE 12/13/16 |        | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |       |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |        | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |       |  |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft  | 0                       | 25              | 50 | 75 | 100 |           |     |                           |       |  |
| 865   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
| 860   | 860.0           | 1.0                 | 2                       | 7                   | 8      |                         |                 |    |    |     |           |     |                           | 861.0 | GROUND SURFACE   |
|   | 857.4           | 3.6                 | 5                       | 9                   | 19     |                         |                 |    |    |     |           |     |                           |       | <b>RESIDUAL</b><br>Yellow and Red, Clayey Silt, with Trace Roots |
| 855   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 852.4           | 8.6                 | 3                       | 7                   | 11     |                         |                 |    |    |     |           |     |                           |       |  |
| 850   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 847.4           | 13.6                | 5                       | 7                   | 10     |                         |                 |    |    |     |           |     |                           |       |  |
| 845   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 842.4           | 18.6                | 3                       | 3                   | 5      |                         |                 |    |    |     |           |     |                           |       |  |
| 840   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 837.4           | 23.6                | 2                       | 3                   | 5      |                         |                 |    |    |     |           |     |                           |       |  |
| 835   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 832.4           | 28.6                | 5                       | 8                   | 11     |                         |                 |    |    |     |           |     |                           |       |  |
| 830   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 827.4           | 33.6                | 9                       | 11                  | 17     |                         |                 |    |    |     |           |     |                           |       |  |
| 825   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 822.4           | 38.6                | 14                      | 17                  | 16     |                         |                 |    |    |     |           |     |                           |       |  |
| 820   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 817.4           | 43.6                | 62                      | 100/0.2             |        |                         |                 |    |    |     |           |     |                           |       |  |
| 815   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 812.4           | 48.6                | 24                      | 40                  | 60/0.4 |                         |                 |    |    |     |           |     |                           |       |  |
| 810   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   | 807.4           | 53.6                | 60/0.1                  |                     |        |                         |                 |    |    |     |           |     |                           |       |  |
|   |                 |                     |                         |                     |        |                         |                 |    |    |     |           |     |                           |       |  |

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |       | GEOLOGIST C.T. Tang, EI |                 |    |    |     |           |     |                           |  |       |
|---|-----------------|---------------------|-------------------------|---------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|--|-------|
| SITE DESCRIPTION Bridge No. 1240 on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |                 |                     |                         |                     |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |  |       |
| BORING NO. EB2-B  |                 | STATION 18+67       |                         | OFFSET 37 ft RT     |       | ALIGNMENT -Y16-         |                 |    |    |     |           |     |                           |  |       |
| COLLAR ELEV. 859.4 ft   |                 | TOTAL DEPTH 57.7 ft |                         | NORTHING 873,007    |       | EASTING 1,780,814       |                 |    |    |     |           |     |                           |  |       |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |                 |                     | DRILL METHOD Mud Rotary |                     |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |  |       |
| DRILLER J. Anderson   |                 | START DATE 12/14/16 |                         | COMP. DATE 12/14/16 |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |  |       |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |  |       |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     |                           |  |       |
| 860   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 858.4           | 1.0                 | 7                       | 10                  | 14    |                         |                 |    |    |     |           |     |                           |  | 859.4 |
| 855   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 855.8           | 3.6                 | 4                       | 7                   | 10    |                         |                 |    |    |     |           |     |                           |  |       |
| 850   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 850.8           | 8.6                 | 3                       | 5                   | 6     |                         |                 |    |    |     |           |     |                           |  |       |
| 845   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 845.8           | 13.6                | 3                       | 4                   | 6     |                         |                 |    |    |     |           |     |                           |  |       |
| 840   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 840.8           | 18.6                | 4                       | 4                   | 7     |                         |                 |    |    |     |           |     |                           |  |       |
| 835   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 835.8           | 23.6                | 3                       | 4                   | 5     |                         |                 |    |    |     |           |     |                           |  |       |
| 830   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 830.8           | 28.6                | 8                       | 13                  | 17    |                         |                 |    |    |     |           |     |                           |  |       |
| 825   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 825.8           | 33.6                | 3                       | 3                   | 4     |                         |                 |    |    |     |           |     |                           |  |       |
| 820   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 820.8           | 38.6                | 2                       | 3                   | 4     |                         |                 |    |    |     |           |     |                           |  |       |
| 815   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 815.8           | 43.6                | 5                       | 8                   | 16    |                         |                 |    |    |     |           |     |                           |  |       |
| 810   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 810.8           | 48.6                | 4                       | 5                   | 8     |                         |                 |    |    |     |           |     |                           |  |       |
| 805   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 805.8           | 53.6                | 39                      | 100                 |       |                         |                 |    |    |     |           |     |                           |  |       |
|   |                 |                     |                         |                     |       |                         |                 |    |    |     |           |     |                           |  |       |
|   | 801.7           | 57.7                | 60/0.0                  |                     |       |                         |                 |    |    |     |           |     |                           |  |       |

NCDOT BORE DOUBLE U2525C\_GEO\_RWAL\_EB1&EB2\_BH.GPJ\_NC\_DOT.GDT 10/3/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

|   |  |                     |                          |                     |  |                         |                 |
|---|--|---------------------|--------------------------|---------------------|--|-------------------------|-----------------|
| WBS 34821.1.1   |  | TIP U-2525C         |                          | COUNTY GUILFORD     |  | GEOLOGIST C.T. Tang, EI |                 |
| SITE DESCRIPTION End Bent No. 2 Retaining Wall on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |  |                     |                          |                     |  |                         | GROUND WTR (ft) |
| BORING NO. EB2-W1   |  | STATION 18+41       |                          | OFFSET 87 ft LT     |  | ALIGNMENT -Y16-         |                 |
| COLLAR ELEV. 858.8 ft   |  | TOTAL DEPTH 58.8 ft |                          | NORTHING 873,048    |  | EASTING 1,780,695       |                 |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |  |                     | DRILL METHOD H.S. Augers |                     |  | HAMMER TYPE Automatic   |                 |
| DRILLER J. Anderson   |  | START DATE 12/12/16 |                          | COMP. DATE 12/12/16 |  | SURFACE WATER DEPTH N/A |                 |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |        | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|-----------|-----------------|------------|------------|-------|--------|----------------|----|----|----|-----|-----------|-----|---------------------------|------------|---|------|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft  | 0              | 25 | 50 | 75 | 100 |           |     |                           |            |   |      |
| 860       |                 |            |            |       |        |                |    |    |    |     |           |     |                           | 858.8      | GROUND SURFACE  | 0.0  |
|           | 857.8           | 1.0        | 1          | 4     | 4      |                |    |    |    |     |           |     |                           |            | RESIDUAL<br>Brown and Red, Clayey Silt, with Trace to Some Mica                   |      |
| 855       | 855.2           | 3.6        | 3          | 6     | 8      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 852.8           | 6.0        | 4          | 4     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
| 850       | 850.3           | 8.5        | 5          | 8     | 9      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 848.7           | 8.5        | 3          | 4     | 6      |                |    |    |    |     |           |     |                           |            |   |      |
| 845       | 845.2           | 13.6       | 4          | 6     | 6      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 843.7           | 13.5       | 2          | 4     | 4      |                |    |    |    |     |           |     |                           |            |   |      |
| 840       | 840.2           | 18.6       | 3          | 6     | 6      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 838.7           | 18.5       | 2          | 3     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
| 835       | 835.2           | 23.6       | 3          | 8     | 14     |                |    |    |    |     |           |     |                           |            |   |      |
|           | 833.7           | 23.5       | 3          | 4     | 7      |                |    |    |    |     |           |     |                           |            |   |      |
| 830       | 830.2           | 28.6       | 6          | 10    | 11     |                |    |    |    |     |           |     |                           | 831.8      | Tan, Sandy Silt   | 27.0 |
|           | 828.7           | 28.5       | 3          | 5     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
| 825       | 825.2           | 33.6       | 2          | 4     | 6      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 823.7           | 33.5       | 1          | 2     | 2      |                |    |    |    |     |           |     |                           |            |   |      |
| 820       | 820.2           | 38.6       | 5          | 10    | 13     |                |    |    |    |     |           |     |                           | 819.8      | Brown, Clayey Silt  | 39.0 |
|           | 818.7           | 38.5       | 1          | 2     | 3      |                |    |    |    |     |           |     |                           |            |   |      |
| 815       | 815.2           | 43.6       | 12         | 21    | 42     |                |    |    |    |     |           |     |                           |            |   |      |
|           | 813.7           | 43.5       | 2          | 3     | 4      |                |    |    |    |     |           |     |                           |            |   |      |
| 810       | 810.2           | 48.6       | 9          | 19    | 29     |                |    |    |    |     |           |     |                           | 811.8      | Tan, Sandy Silt   | 47.0 |
|           | 808.7           | 48.5       | 8          | 15    | 21     |                |    |    |    |     |           |     |                           |            |   |      |
| 805       | 805.2           | 53.6       | 27         | 52    | 48/0.4 |                |    |    |    |     |           |     |                           | 804.7      | WEATHERED ROCK<br>(Metamorphosed Granite)   | 54.1 |
|           | 803.7           | 53.5       | 6          | 10    | 14     |                |    |    |    |     |           |     |                           |            |   |      |
| 800       | 800.2           | 58.6       |            |       |        |                |    |    |    |     |           |     |                           | 800.0      | Boring Terminated at Elevation 800.0 ft in Weathered Rock (Metamorphosed Granite) | 58.8 |
|           |                 | 100/0.2    |            |       |        |                |    |    |    |     |           |     |                           |            |   |      |

|   |  |                     |                          |                     |  |                         |                 |
|---|--|---------------------|--------------------------|---------------------|--|-------------------------|-----------------|
| WBS 34821.1.1   |  | TIP U-2525C         |                          | COUNTY GUILFORD     |  | GEOLOGIST C.T. Tang, EI |                 |
| SITE DESCRIPTION End Bent No. 2 Retaining Wall on SR2526 (Summit Ave.) over Greensboro Eastern Loop I-85 Bypass |  |                     |                          |                     |  |                         | GROUND WTR (ft) |
| BORING NO. EB2-W2   |  | STATION 18+38       |                          | OFFSET 97 ft RT     |  | ALIGNMENT -Y16-         |                 |
| COLLAR ELEV. 857.2 ft   |  | TOTAL DEPTH 59.7 ft |                          | NORTHING 872,949    |  | EASTING 1,780,849       |                 |
| DRILL RIG/HAMMER EFF./DATE BRI8284 45 Track 89% 02/26/2016  |  |                     | DRILL METHOD H.S. Augers |                     |  | HAMMER TYPE Automatic   |                 |
| DRILLER J. Anderson   |  | START DATE 12/12/16 |                          | COMP. DATE 12/12/16 |  | SURFACE WATER DEPTH N/A |                 |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |        | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|-----------|-----------------|------------|------------|-------|--------|----------------|----|----|----|-----|-----------|-----|---------------------------|------------|---|------|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft  | 0              | 25 | 50 | 75 | 100 |           |     |                           |            |   |      |
| 860       |                 |            |            |       |        |                |    |    |    |     |           |     |                           | 857.2      | GROUND SURFACE  | 0.0  |
|           | 856.2           | 1.0        | 3          | 6     | 7      |                |    |    |    |     |           |     |                           |            | RESIDUAL<br>Red, Clayey Silt  |      |
| 855       | 853.7           | 3.5        | 4          | 8     | 8      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 848.7           | 8.5        | 3          | 4     | 6      |                |    |    |    |     |           |     |                           |            |   |      |
| 850       |                 |            |            |       |        |                |    |    |    |     |           |     |                           |            |   |      |
|           | 845.2           | 12.0       |            |       |        |                |    |    |    |     |           |     |                           |            |   |      |
| 845       | 843.7           | 13.5       | 2          | 4     | 4      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 840.2           | 17.0       |            |       |        |                |    |    |    |     |           |     |                           |            |   |      |
| 840       | 838.7           | 18.5       | 2          | 3     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 833.7           | 23.5       | 3          | 4     | 7      |                |    |    |    |     |           |     |                           |            |   |      |
| 835       | 833.7           | 23.5       | 3          | 4     | 7      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 828.7           | 28.5       | 3          | 5     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
| 830       | 828.7           | 28.5       | 3          | 5     | 5      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 823.7           | 33.5       | 1          | 2     | 2      |                |    |    |    |     |           |     |                           |            |   |      |
| 825       | 823.7           | 33.5       | 1          | 2     | 2      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 818.7           | 38.5       | 1          | 2     | 3      |                |    |    |    |     |           |     |                           |            |   |      |
| 820       | 818.7           | 38.5       | 1          | 2     | 3      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 813.7           | 43.5       | 2          | 3     | 4      |                |    |    |    |     |           |     |                           |            |   |      |
| 815       | 813.7           | 43.5       | 2          | 3     | 4      |                |    |    |    |     |           |     |                           |            |   |      |
|           | 808.7           | 48.5       | 8          | 15    | 21     |                |    |    |    |     |           |     |                           |            |   |      |
| 810       | 808.7           | 48.5       | 8          | 15    | 21     |                |    |    |    |     |           |     |                           |            |   |      |
|           | 805.2           | 52.0       |            |       |        |                |    |    |    |     |           |     |                           |            |   |      |
| 805       | 803.7           | 53.5       | 6          | 10    | 14     |                |    |    |    |     |           |     |                           |            |   |      |
|           | 800.7           | 58.5       | 19         | 49    | 51/0.2 |                |    |    |    |     |           |     |                           |            |   |      |
| 800       | 798.7           | 58.5       | 19         | 49    | 51/0.2 |                |    |    |    |     |           |     |                           | 798.2      | WEATHERED ROCK<br>(Metamorphosed Granite)   | 59.0 |
|           |                 | 100/0.7    |            |       |        |                |    |    |    |     |           |     |                           | 797.5      | Boring Terminated at Elevation 797.5 ft in Weathered Rock (Metamorphosed Granite) | 59.7 |

NCDOT BORE DOUBLE U2525C\_GEO\_RWAL\_EB1&EB2\_BH.GPJ\_NC\_DOT.GDT 10/3/17

REFERENCE: U-2525C

PROJECT: 3482I

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

**STRUCTURE  
SUBSURFACE INVESTIGATION**

COUNTY GUILFORD  
PROJECT DESCRIPTION GREENSBORO EASTERN LOOP  
FROM US 29 NORTH OF GREENSBORO TO SR  
2303 (LAWNDALE DRIVE)  
SITE DESCRIPTION SITE #2 (STRUCTURE #2 AND #3)  
BRIDGE NO. 1241 AND 1242 ON I-85 BYPASS (-L-)  
OVER LEES CHAPEL ROAD (-Y1-)

**CONTENTS**

| SHEET NO. | DESCRIPTION          |
|-----------|----------------------|
| 1         | TITLE SHEET          |
| 2         | LEGEND (SOIL & ROCK) |
| 3         | SITE PLAN            |
| 4-5       | CROSS SECTIONS       |
| 6-10      | BORE LOGS            |
| 11        | LABORATORY RESULTS   |
| 12        | SITE PHOTOGRAPHS     |

| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
|-------|-----------------------------|-----------|--------------|
| N.C.  | U-2525C                     | 1         | 12           |

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PERSONNEL

D. KUBINSKI

R. TOOTHMAN

W. ALLEN

B. JOHNSON

INVESTIGATED BY D. KUBINSKI

DRAWN BY B. JOHNSON

CHECKED BY X. BARRETT

SUBMITTED BY KLEINFELDER, INC.

DATE SEPTEMBER 2017

Prepared in the Office of:



**KLEINFELDER**  
Bright People. Right Solutions.  
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GREENSBORO, NC 2740  
ENGINEERING FIRM LICENSE NO. F-132



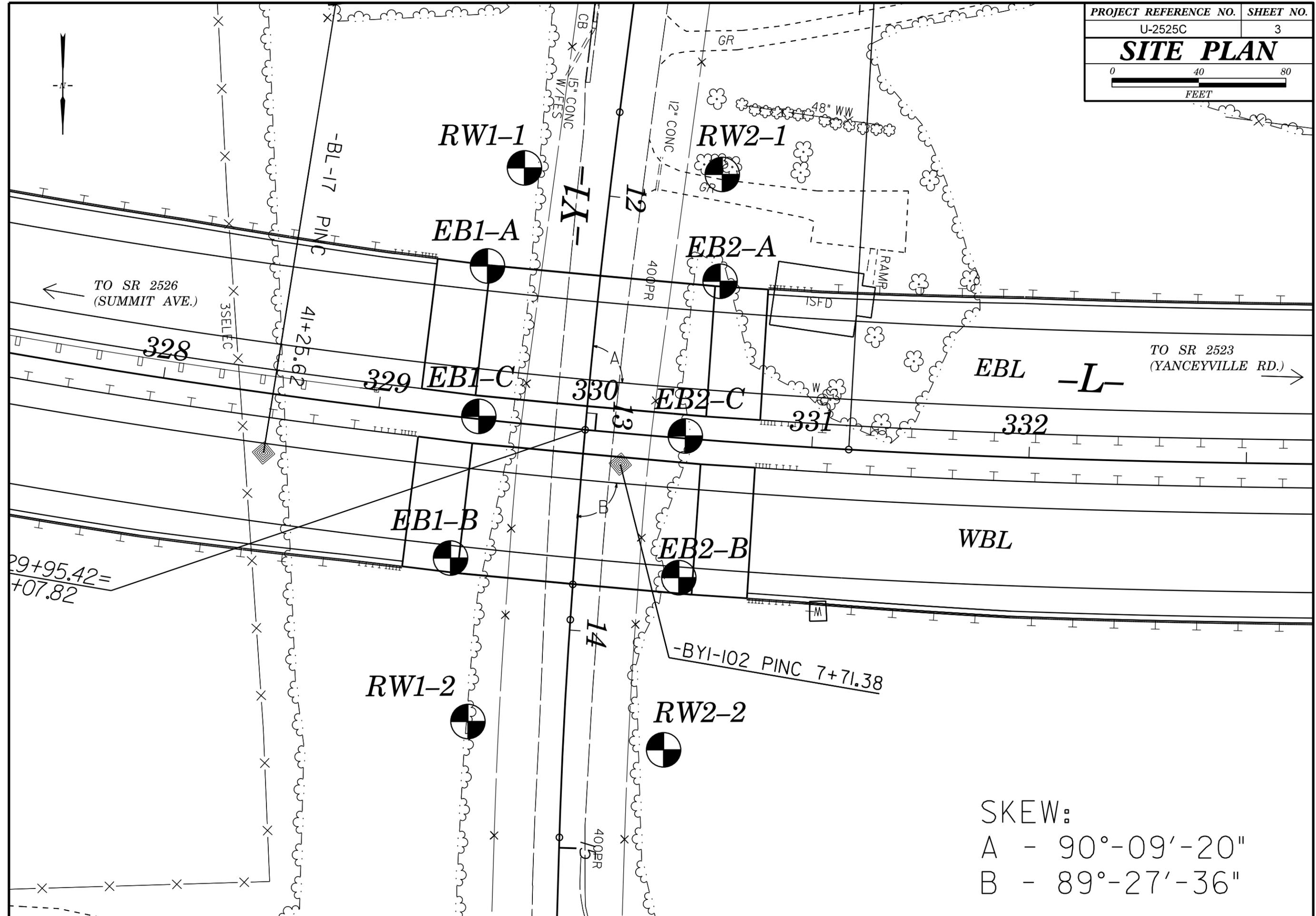
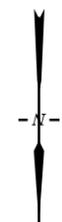
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Xavier C. Barrett 10/9/2017

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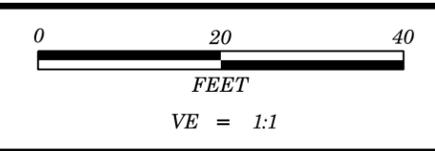
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**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**  
**SUBSURFACE INVESTIGATION**  
**SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

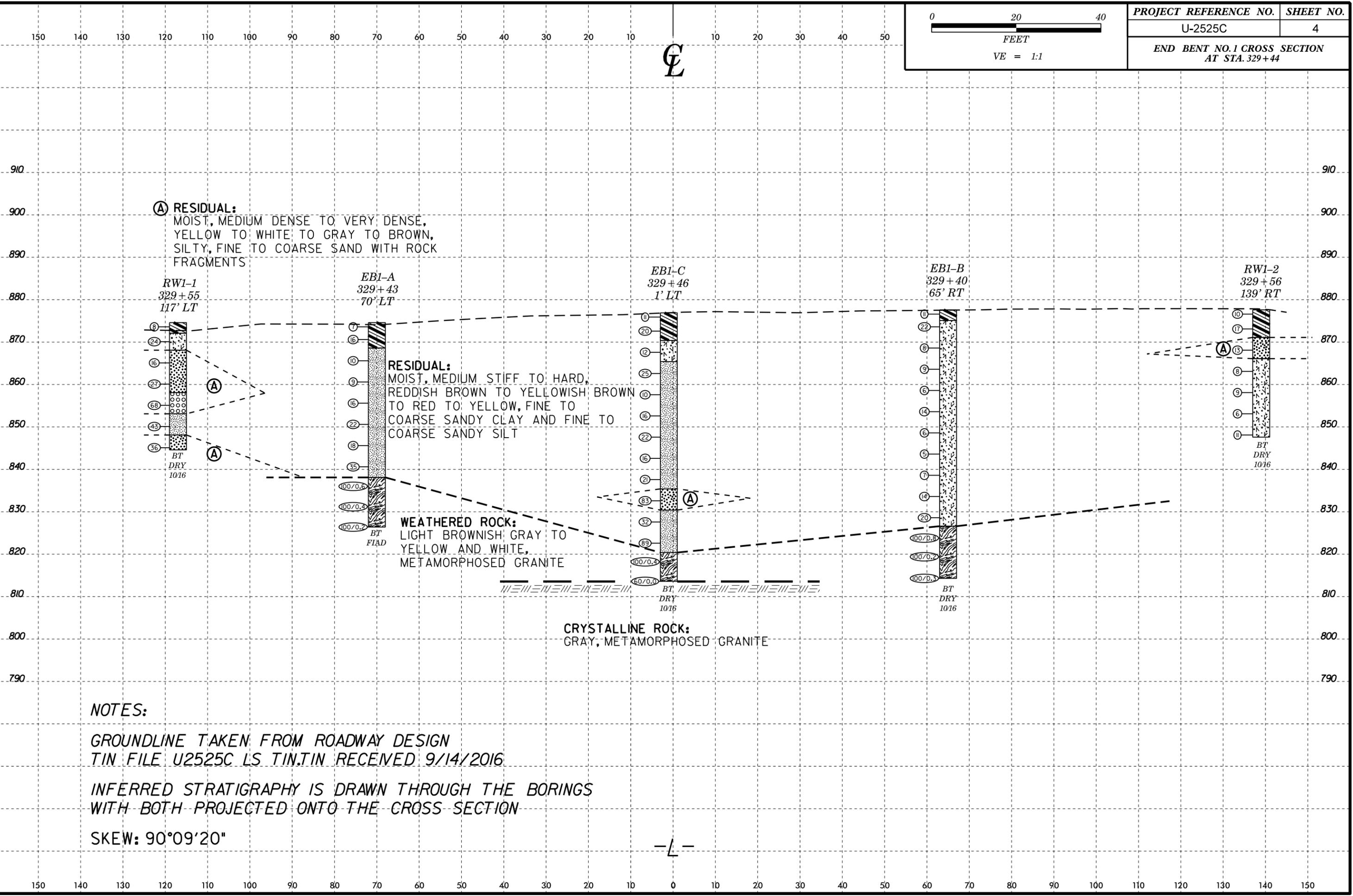
| SOIL DESCRIPTION  |   |   |  |                   |                   |  |                   |             |             | GRADATION  |   |  |  |  |   |  |             |   |  | ROCK DESCRIPTION   |  |   |             |  |  |               |                         |                    |                  | TERMS AND DEFINITIONS  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
|---|---|---|--|-------------------|-------------------|--|-------------------|-------------|-------------|--|---|--|--|--|---|--|-------------|---|--|--|--|---|-------------|--|--|---------------|-------------------------|--------------------|------------------|--|-------------------|------------------|--------------|-----|-----|-----|-----|------------|-----|----------|----------|-----------|-------------------|------|--------------|------------------|-------------|-------|----------------|------------|---------------------|--|--|---|--|--|--|------------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------|-------------|-------------|-------------|----------------|-----------------|------------|--|----------------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--------------------------------|---|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-------------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|------------------|----------------|-------------------|----------------|-------------------------|--------|--------|---------------|-----------------------|--------|---------|-----------------|--------------------|---------|----------|---------------|----------------|-------|-------|----------------------|
| <p>SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i></p>  |   |   |  |                   |                   |  |                   |             |             | <p><b>WELL GRADED</b> - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.<br/> <b>UNIFORMLY GRADED</b> - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.<br/> <b>GAP-GRADED</b> - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.</p>  |   |  |  |  |   |  |             |   |  | <p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p> |  |   |             |  |  |               |                         |                    |                  | <p><b>ALLUVIUM (ALLUV.)</b> - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.<br/> <b>AQUIFER</b> - A WATER BEARING FORMATION OR STRATA.<br/> <b>ARENACEOUS</b> - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.<br/> <b>ARGILLACEOUS</b> - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.<br/> <b>ARTESIAN</b> - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.<br/> <b>CALCAREOUS (CALC.)</b> - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.<br/> <b>COLLUVIUM</b> - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.<br/> <b>CORE RECOVERY (REC.)</b> - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/> <b>DIKE</b> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.<br/> <b>DIP</b> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.<br/> <b>DIP DIRECTION (DIP AZIMUTH)</b> - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.<br/> <b>FAULT</b> - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.<br/> <b>FISSILE</b> - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.<br/> <b>FLOAT</b> - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL.<br/> <b>FLOOD PLAIN (FP)</b> - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.<br/> <b>FORMATION (FM)</b> - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.<br/> <b>JOINT</b> - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.<br/> <b>LEDGE</b> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.<br/> <b>LENS</b> - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.<br/> <b>MOTTLED (MOT.)</b> - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS, MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.<br/> <b>PERCHED WATER</b> - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.<br/> <b>RESIDUAL (RES.) SOIL</b> - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.<br/> <b>ROCK QUALITY DESIGNATION (RQD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/> <b>SAPROLITE (SAP.)</b> - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.<br/> <b>SILL</b> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.<br/> <b>SLICKENSIDE</b> - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.<br/> <b>STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)</b> - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.<br/> <b>STRATA CORE RECOVERY (SREC.)</b> - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.<br/> <b>STRATA ROCK QUALITY DESIGNATION (SROD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.<br/> <b>TOPSOIL (TS.)</b> - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p> |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>SOIL LEGEND AND AASHTO CLASSIFICATION</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>GENERAL CLASS.</th> <th colspan="5">GRANULAR MATERIALS (≤ 35% PASSING #200)</th> <th colspan="5">SILT-CLAY MATERIALS (&gt; 35% PASSING #200)</th> <th colspan="5">ORGANIC MATERIALS</th> </tr> <tr> <th>GROUP CLASS.</th> <th>A-1</th> <th>A-3</th> <th>A-2</th> <th>A-2-4</th> <th>A-2-5</th> <th>A-2-6</th> <th>A-2-7</th> <th>A-4</th> <th>A-5</th> <th>A-6</th> <th>A-7</th> <th>A-1, A-2</th> <th>A-3</th> <th>A-4, A-5</th> <th>A-6, A-7</th> </tr> <tr> <th>SYMBOL</th> <td></td> </tr> <tr> <th>% PASSING #10 #40 #200</th> <td>50 MX 30 MX 15 MX</td> <td>50 MX 25 MX 10 MX</td> <td>51 MN 35 MX 35 MX</td> <td>40 MX 41 MN 10 MX</td> <td>40 MX 41 MN 11 MN</td> <td>40 MX 41 MN 11 MN</td> <td>40 MX 41 MN 11 MN</td> <td>36 MN 36 MN</td> <td>36 MN 36 MN</td> <td>36 MN 36 MN</td> <td>36 MN 36 MN</td> <td>GRANULAR SOILS</td> <td>SILT-CLAY SOILS</td> <td>MUCK, PEAT</td> <td></td> </tr> <tr> <th>MATERIAL PASSING #40 LL PI</th> <td colspan="15"> <p>SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER</p> <p>HIGHLY ORGANIC SOILS</p> </td> </tr> <tr> <th>GROUP INDEX</th> <td colspan="15"> <p>0 0 0 4 MX 8 MX 12 MX 16 MX NO MX</p> </td> </tr> <tr> <th>USUAL TYPES OF MAJOR MATERIALS</th> <td colspan="15"> <p>STONE FRAGS. GRAVEL, AND SAND FINE SAND SILTY OR CLAYEY GRAVEL AND SAND SILTY SOILS CLAYEY SOILS</p> </td> </tr> <tr> <th>GEN. RATING AS SUBGRADE</th> <td colspan="15"> <p>EXCELLENT TO GOOD FAIR TO POOR FAIR TO POOR POOR UNSUITABLE</p> </td> </tr> </table> |   |   |  |                   |                   |  |                   |             |             | GENERAL CLASS.   | GRANULAR MATERIALS (≤ 35% PASSING #200) |  |  |  |   | SILT-CLAY MATERIALS (> 35% PASSING #200)       |             |   |  |  | ORGANIC MATERIALS  |   |             |  |  | GROUP CLASS.  | A-1                     | A-3                | A-2              | A-2-4  | A-2-5             | A-2-6            | A-2-7        | A-4 | A-5 | A-6 | A-7 | A-1, A-2   | A-3 | A-4, A-5 | A-6, A-7 | SYMBOL    |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  | % PASSING #10 #40 #200 | 50 MX 30 MX 15 MX | 50 MX 25 MX 10 MX | 51 MN 35 MX 35 MX | 40 MX 41 MN 10 MX | 40 MX 41 MN 11 MN | 40 MX 41 MN 11 MN | 40 MX 41 MN 11 MN | 36 MN 36 MN | GRANULAR SOILS | SILT-CLAY SOILS | MUCK, PEAT |  | MATERIAL PASSING #40 LL PI | <p>SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER</p> <p>HIGHLY ORGANIC SOILS</p> |  |  |  |  |  |  |  |  |  |  |  |  |  |  | GROUP INDEX | <p>0 0 0 4 MX 8 MX 12 MX 16 MX NO MX</p> |  |  |  |  |  |  |  |  |  |  |  |  |  |  | USUAL TYPES OF MAJOR MATERIALS | <p>STONE FRAGS. GRAVEL, AND SAND FINE SAND SILTY OR CLAYEY GRAVEL AND SAND SILTY SOILS CLAYEY SOILS</p> |  |  |  |  |  |  |  |  |  |  |  |  |  |  | GEN. RATING AS SUBGRADE | <p>EXCELLENT TO GOOD FAIR TO POOR FAIR TO POOR POOR UNSUITABLE</p> |  |  |  |  |  |  |  |  |  |  |  |  |  |  | <p style="text-align: center;"><b>MINERALOGICAL COMPOSITION</b></p> <p>MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.</p> |  |  |  |  |  |  |  |  |  | <p style="text-align: center;"><b>WEATHERING</b></p> <p>FRESH ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.</p> <p>VERY SLIGHT (V SL.) ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.</p> <p>SLIGHT (SL.) ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.</p> <p>MODERATE (MOD.) SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.</p> <p>MODERATELY SEVERE (MOD. SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i></p> <p>SEVERE (SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &gt; 100 BPF</i></p> <p>VERY SEVERE (V SEV.) ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</i></p> <p>COMPLETE ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. FABRIC MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.</p> |  |  |  |  |  |  |  |  |  | <p style="text-align: center;"><b>PERCENTAGE OF MATERIAL</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>ORGANIC MATERIAL</th> <th>GRANULAR SOILS</th> <th>SILT - CLAY SOILS</th> <th>OTHER MATERIAL</th> </tr> <tr> <td>TRACE OF ORGANIC MATTER</td> <td>2 - 3%</td> <td>3 - 5%</td> <td>TRACE 1 - 10%</td> </tr> <tr> <td>LITTLE ORGANIC MATTER</td> <td>3 - 5%</td> <td>5 - 12%</td> <td>LITTLE 10 - 20%</td> </tr> <tr> <td>MODERATELY ORGANIC</td> <td>5 - 10%</td> <td>12 - 20%</td> <td>SOME 20 - 35%</td> </tr> <tr> <td>HIGHLY ORGANIC</td> <td>&gt; 10%</td> <td>&gt; 20%</td> <td>HIGHLY 35% AND ABOVE</td> </tr> </table> |  |  |  |  |  |  |  |  |  | ORGANIC MATERIAL | GRANULAR SOILS | SILT - CLAY SOILS | OTHER MATERIAL | TRACE OF ORGANIC MATTER | 2 - 3% | 3 - 5% | TRACE 1 - 10% | LITTLE ORGANIC MATTER | 3 - 5% | 5 - 12% | LITTLE 10 - 20% | MODERATELY ORGANIC | 5 - 10% | 12 - 20% | SOME 20 - 35% | HIGHLY ORGANIC | > 10% | > 20% | HIGHLY 35% AND ABOVE |
| GENERAL CLASS.  | GRANULAR MATERIALS (≤ 35% PASSING #200)   |   |  |                   |                   | SILT-CLAY MATERIALS (> 35% PASSING #200) |                   |             |             |  | ORGANIC MATERIALS                       |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GROUP CLASS.  | A-1   | A-3   | A-2  | A-2-4             | A-2-5             | A-2-6                                    | A-2-7             | A-4         | A-5         | A-6  | A-7                                     | A-1, A-2   | A-3  | A-4, A-5                                   | A-6, A-7  |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| SYMBOL  |   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| % PASSING #10 #40 #200  | 50 MX 30 MX 15 MX   | 50 MX 25 MX 10 MX   | 51 MN 35 MX 35 MX  | 40 MX 41 MN 10 MX | 40 MX 41 MN 11 MN | 40 MX 41 MN 11 MN                        | 40 MX 41 MN 11 MN | 36 MN 36 MN | 36 MN 36 MN | 36 MN 36 MN  | 36 MN 36 MN                             | GRANULAR SOILS                                     | SILT-CLAY SOILS  | MUCK, PEAT                                 |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| MATERIAL PASSING #40 LL PI  | <p>SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER</p> <p>HIGHLY ORGANIC SOILS</p>              |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GROUP INDEX   | <p>0 0 0 4 MX 8 MX 12 MX 16 MX NO MX</p>  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| USUAL TYPES OF MAJOR MATERIALS  | <p>STONE FRAGS. GRAVEL, AND SAND FINE SAND SILTY OR CLAYEY GRAVEL AND SAND SILTY SOILS CLAYEY SOILS</p> |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GEN. RATING AS SUBGRADE   | <p>EXCELLENT TO GOOD FAIR TO POOR FAIR TO POOR POOR UNSUITABLE</p>                                      |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| ORGANIC MATERIAL  | GRANULAR SOILS  | SILT - CLAY SOILS   | OTHER MATERIAL   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| TRACE OF ORGANIC MATTER   | 2 - 3%  | 3 - 5%  | TRACE 1 - 10%  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| LITTLE ORGANIC MATTER   | 3 - 5%  | 5 - 12%   | LITTLE 10 - 20%  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| MODERATELY ORGANIC  | 5 - 10%   | 12 - 20%  | SOME 20 - 35%  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| HIGHLY ORGANIC  | > 10%   | > 20%   | HIGHLY 35% AND ABOVE   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>GROUND WATER</b></p> <p> WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING</p> <p> STATIC WATER LEVEL AFTER 24 HOURS</p> <p> PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA</p> <p> SPRING OR SEEP</p>  |   |   |  |                   |                   |  |                   |             |             | <p style="text-align: center;"><b>MISCELLANEOUS SYMBOLS</b></p> <p> ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION</p> <p> SOIL SYMBOL</p> <p> ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT</p> <p> INFERRED SOIL BOUNDARY</p> <p> INFERRED ROCK LINE</p> <p> ALLUVIAL SOIL BOUNDARY</p> <p> DIP &amp; DIP DIRECTION OF ROCK STRUCTURES</p> <p> SPT TEST BORING</p> <p> AUGER BORING</p> <p> CORE BORING</p> <p> MONITORING WELL</p> <p> PIEZOMETER INSTALLATION</p> <p> SLOPE INDICATOR INSTALLATION</p> <p> CONE PENETROMETER TEST</p> <p> SOUNDING ROD</p> <p> TEST BORING WITH CORE</p> <p> SPT N-VALUE</p> |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>CONSISTENCY OR DENSENESS</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>PRIMARY SOIL TYPE</th> <th>COMPACTNESS OR CONSISTENCY</th> <th>RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)</th> <th>RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT<sup>2</sup>)</th> </tr> <tr> <td>GENERALLY GRANULAR MATERIAL (NON-COHESIVE)</td> <td>VERY LOOSE<br/>LOOSE<br/>MEDIUM DENSE<br/>DENSE<br/>VERY DENSE</td> <td>&lt; 4<br/>4 TO 10<br/>10 TO 30<br/>30 TO 50<br/>&gt; 50</td> <td>N/A</td> </tr> <tr> <td>GENERALLY SILT-CLAY MATERIAL (COHESIVE)</td> <td>VERY SOFT<br/>SOFT<br/>MEDIUM STIFF<br/>STIFF<br/>VERY STIFF<br/>HARD</td> <td>&lt; 2<br/>2 TO 4<br/>4 TO 8<br/>8 TO 15<br/>15 TO 30<br/>&gt; 30</td> <td>&lt; 0.25<br/>0.25 TO 0.5<br/>0.5 TO 1.0<br/>1 TO 2<br/>2 TO 4<br/>&gt; 4</td> </tr> </table>   |   |   |  |                   |                   |  |                   |             |             | PRIMARY SOIL TYPE  | COMPACTNESS OR CONSISTENCY              | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE) | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) | GENERALLY GRANULAR MATERIAL (NON-COHESIVE) | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE          | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50 | N/A         | GENERALLY SILT-CLAY MATERIAL (COHESIVE)               | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30   | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4 | <p style="text-align: center;"><b>RECOMMENDATION SYMBOLS</b></p> <p> UNDERCUT</p> <p> SHALLOW UNDERCUT</p> <p> UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE</p> <p> UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK</p> <p> UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL</p> |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| PRIMARY SOIL TYPE   | COMPACTNESS OR CONSISTENCY  | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)                  | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GENERALLY GRANULAR MATERIAL (NON-COHESIVE)  | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE  | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50                      | N/A  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GENERALLY SILT-CLAY MATERIAL (COHESIVE)   | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD  | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30              | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>TEXTURE OR GRAIN SIZE</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>U.S. STD. SIEVE SIZE OPENING (MM)</th> <td>4</td> <td>10</td> <td>40</td> <td>60</td> <td>200</td> <td>270</td> </tr> <tr> <td></td> <td>4.76</td> <td>2.00</td> <td>0.42</td> <td>0.25</td> <td>0.075</td> <td>0.053</td> </tr> <tr> <th>BOULDER (BLDR.)</th> <th>COBBLE (COB.)</th> <th>GRAVEL (GR.)</th> <th>COARSE SAND (CS.E. SD.)</th> <th>FINE SAND (F SD.)</th> <th>SILT (SL.)</th> <th>CLAY (CL.)</th> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <th>GRAIN SIZE</th> <th>MM</th> <th>305</th> <th>75</th> <th>2.0</th> <th>0.25</th> <th>0.05</th> <th>0.005</th> </tr> <tr> <td></td> <td>IN.</td> <td>12</td> <td>3</td> <td></td> <td></td> <td></td> <td></td> </tr> </table>  |   |   |  |                   |                   |  |                   |             |             | U.S. STD. SIEVE SIZE OPENING (MM)  | 4                                       | 10   | 40   | 60   | 200   | 270  |             | 4.76  | 2.00   | 0.42   | 0.25   | 0.075   | 0.053       | BOULDER (BLDR.)                                      | COBBLE (COB.)  | GRAVEL (GR.)  | COARSE SAND (CS.E. SD.) | FINE SAND (F SD.)  | SILT (SL.)       | CLAY (CL.)   |                   |                  |              |     |     |     |     | GRAIN SIZE | MM  | 305      | 75       | 2.0       | 0.25              | 0.05 | 0.005        |                  | IN.         | 12    | 3              |            |                     |  |  | <p style="text-align: center;"><b>ABBREVIATIONS</b></p> <p>AR - AUGER REFUSAL<br/> BT - BORING TERMINATED<br/> CL. - CLAY<br/> CPT - COANE PENETRATION TEST<br/> CSE. - COARSE<br/> DMT - DILATOMETER TEST<br/> DPT - DYNAMIC PENETRATION TEST<br/> e - VOID RATIO<br/> F - FINE<br/> FOSS. - FOSSILIFEROUS<br/> FRAC. - FRACTURED, FRACTURES<br/> FRAGS. - FRAGMENTS<br/> HI. - HIGHLY</p> <p>MED. - MEDIUM<br/> MICA. - MICACEOUS<br/> MOD. - MODERATELY<br/> NP - NON PLASTIC<br/> ORG. - ORGANIC<br/> PMT - PRESSUREMETER TEST<br/> SAP. - SAPROLITIC<br/> SD. - SAND, SANDY<br/> SL. - SILT, SILTY<br/> SLI. - SLIGHTLY<br/> TCR - TRICONE REFUSAL<br/> w - MOISTURE CONTENT<br/> V - VERY</p> <p>VST - VANE SHEAR TEST<br/> WEA. - WEATHERED<br/> W - UNIT WEIGHT<br/> W<sub>d</sub> - DRY UNIT WEIGHT</p> <p><b>SAMPLE ABBREVIATIONS</b></p> <p>S - BULK<br/> SS - SPLIT SPOON<br/> ST - SHELBY TUBE<br/> RS - ROCK<br/> RT - RECOMPACTED TRIAXIAL<br/> CBR - CALIFORNIA BEARING RATIO</p> |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| U.S. STD. SIEVE SIZE OPENING (MM)   | 4   | 10  | 40   | 60                | 200               | 270                                      |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
|   | 4.76  | 2.00  | 0.42   | 0.25              | 0.075             | 0.053                                    |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| BOULDER (BLDR.)   | COBBLE (COB.)   | GRAVEL (GR.)  | COARSE SAND (CS.E. SD.)  | FINE SAND (F SD.) | SILT (SL.)        | CLAY (CL.)                               |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
|   |   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| GRAIN SIZE  | MM  | 305   | 75   | 2.0               | 0.25              | 0.05                                     | 0.005             |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
|   | IN.   | 12  | 3  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>SOIL MOISTURE - CORRELATION OF TERMS</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>SOIL MOISTURE SCALE (ATTERBERG LIMITS)</th> <th>FIELD MOISTURE DESCRIPTION</th> <th>GUIDE FOR FIELD MOISTURE DESCRIPTION</th> </tr> <tr> <td>LL - LIQUID LIMIT</td> <td>- SATURATED - (SAT.)</td> <td>USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE</td> </tr> <tr> <td>PLASTIC RANGE (PI)</td> <td>- WET - (W)</td> <td>SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE</td> </tr> <tr> <td>OM - OPTIMUM MOISTURE</td> <td>- MOIST - (M)</td> <td>SOLID; AT OR NEAR OPTIMUM MOISTURE</td> </tr> <tr> <td>SL - SHRINKAGE LIMIT</td> <td>- DRY - (D)</td> <td>REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE</td> </tr> </table>  |   |   |  |                   |                   |  |                   |             |             | SOIL MOISTURE SCALE (ATTERBERG LIMITS)   | FIELD MOISTURE DESCRIPTION              | GUIDE FOR FIELD MOISTURE DESCRIPTION               | LL - LIQUID LIMIT  | - SATURATED - (SAT.)                       | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE | PLASTIC RANGE (PI)                             | - WET - (W) | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE | OM - OPTIMUM MOISTURE  | - MOIST - (M)  | SOLID; AT OR NEAR OPTIMUM MOISTURE                             | SL - SHRINKAGE LIMIT  | - DRY - (D) | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE | <p style="text-align: center;"><b>EQUIPMENT USED ON SUBJECT PROJECT</b></p> <p>DRILL UNITS:</p> <p><input type="checkbox"/> CME-45C</p> <p><input checked="" type="checkbox"/> CME-55</p> <p><input type="checkbox"/> CME-550</p> <p><input type="checkbox"/> VANE SHEAR TEST</p> <p><input type="checkbox"/> PORTABLE HOIST</p> <p>ADVANCING TOOLS:</p> <p><input type="checkbox"/> CLAY BITS</p> <p><input checked="" type="checkbox"/> 6" CONTINUOUS FLIGHT AUGER</p> <p><input type="checkbox"/> 8" HOLLOW AUGERS</p> <p><input type="checkbox"/> HARD FACED FINGER BITS</p> <p><input type="checkbox"/> TUNG-CARBIDE INSERTS</p> <p><input type="checkbox"/> CASING <input type="checkbox"/> W/ ADVANCER</p> <p><input checked="" type="checkbox"/> TRICONE 2-15/16" STEEL TEETH</p> <p><input type="checkbox"/> TRICONE " TUNG-CARB.</p> <p><input type="checkbox"/> CORE BIT</p> <p>HAMMER TYPE:</p> <p><input checked="" type="checkbox"/> AUTOMATIC <input type="checkbox"/> MANUAL</p> <p>CORE SIZE:</p> <p><input type="checkbox"/> -B <input type="checkbox"/> -H</p> <p><input type="checkbox"/> -N</p> <p>HAND TOOLS:</p> <p><input type="checkbox"/> POST HOLE DIGGER</p> <p><input type="checkbox"/> HAND AUGER</p> <p><input type="checkbox"/> SOUNDING ROD</p> <p><input type="checkbox"/> VANE SHEAR TEST</p> |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| SOIL MOISTURE SCALE (ATTERBERG LIMITS)  | FIELD MOISTURE DESCRIPTION  | GUIDE FOR FIELD MOISTURE DESCRIPTION                                |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| LL - LIQUID LIMIT   | - SATURATED - (SAT.)  | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| PLASTIC RANGE (PI)  | - WET - (W)   | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE               |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| OM - OPTIMUM MOISTURE   | - MOIST - (M)   | SOLID; AT OR NEAR OPTIMUM MOISTURE                                  |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| SL - SHRINKAGE LIMIT  | - DRY - (D)   | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE                |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>PLASTICITY</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>NON PLASTIC</th> <th colspan="2">PLASTICITY INDEX (PI)</th> <th>DRY STRENGTH</th> </tr> <tr> <td>SLIGHTLY PLASTIC</td> <td>0-5</td> <td></td> <td>VERY LOW</td> </tr> <tr> <td>MODERATELY PLASTIC</td> <td>6-15</td> <td></td> <td>SLIGHT</td> </tr> <tr> <td>HIGHLY PLASTIC</td> <td>16-25</td> <td></td> <td>MEDIUM</td> </tr> <tr> <td></td> <td>26 OR MORE</td> <td></td> <td>HIGH</td> </tr> </table>   |   |   |  |                   |                   |  |                   |             |             | NON PLASTIC  | PLASTICITY INDEX (PI)                   |  | DRY STRENGTH   | SLIGHTLY PLASTIC                           | 0-5   |  | VERY LOW    | MODERATELY PLASTIC                                    | 6-15   |  | SLIGHT   | HIGHLY PLASTIC  | 16-25       |  | MEDIUM   |               | 26 OR MORE              |                    | HIGH             | <p style="text-align: center;"><b>FRACATURE SPACING</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>TERM</th> <th>SPACING</th> </tr> <tr> <td>VERY WIDE</td> <td>MORE THAN 10 FEET</td> </tr> <tr> <td>WIDE</td> <td>3 TO 10 FEET</td> </tr> <tr> <td>MODERATELY CLOSE</td> <td>1 TO 3 FEET</td> </tr> <tr> <td>CLOSE</td> <td>0.16 TO 1 FOOT</td> </tr> <tr> <td>VERY CLOSE</td> <td>LESS THAN 0.16 FEET</td> </tr> </table>  |                   |                  |              |     |     |     |     |            |     | TERM     | SPACING  | VERY WIDE | MORE THAN 10 FEET | WIDE | 3 TO 10 FEET | MODERATELY CLOSE | 1 TO 3 FEET | CLOSE | 0.16 TO 1 FOOT | VERY CLOSE | LESS THAN 0.16 FEET |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| NON PLASTIC   | PLASTICITY INDEX (PI)   |   | DRY STRENGTH   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| SLIGHTLY PLASTIC  | 0-5   |   | VERY LOW   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| MODERATELY PLASTIC  | 6-15  |   | SLIGHT   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| HIGHLY PLASTIC  | 16-25   |   | MEDIUM   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
|   | 26 OR MORE  |   | HIGH   |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| TERM  | SPACING   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| VERY WIDE   | MORE THAN 10 FEET   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| WIDE  | 3 TO 10 FEET  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| MODERATELY CLOSE  | 1 TO 3 FEET   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| CLOSE   | 0.16 TO 1 FOOT  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| VERY CLOSE  | LESS THAN 0.16 FEET   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>COLOR</b></p> <p>DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-BROWN). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.</p>  |   |   |  |                   |                   |  |                   |             |             | <p style="text-align: center;"><b>BEDDING</b></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th>TERM</th> <th>THICKNESS</th> </tr> <tr> <td>VERY THICKLY BEDDED</td> <td>4 FEET</td> </tr> <tr> <td>THICKLY BEDDED</td> <td>1.5 - 4 FEET</td> </tr> <tr> <td>THINLY BEDDED</td> <td>0.16 - 1.5 FEET</td> </tr> <tr> <td>VERY THINLY BEDDED</td> <td>0.03 - 0.16 FEET</td> </tr> <tr> <td>THICKLY LAMINATED</td> <td>0.008 - 0.03 FEET</td> </tr> <tr> <td>THINLY LAMINATED</td> <td>&lt; 0.008 FEET</td> </tr> </table>  |   |  |  |  |   |  |             |   |  | TERM   | THICKNESS  | VERY THICKLY BEDDED   | 4 FEET      | THICKLY BEDDED                                       | 1.5 - 4 FEET   | THINLY BEDDED | 0.16 - 1.5 FEET         | VERY THINLY BEDDED | 0.03 - 0.16 FEET | THICKLY LAMINATED  | 0.008 - 0.03 FEET | THINLY LAMINATED | < 0.008 FEET |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| TERM  | THICKNESS   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| VERY THICKLY BEDDED   | 4 FEET  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| THICKLY BEDDED  | 1.5 - 4 FEET  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| THINLY BEDDED   | 0.16 - 1.5 FEET   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| VERY THINLY BEDDED  | 0.03 - 0.16 FEET  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| THICKLY LAMINATED   | 0.008 - 0.03 FEET   |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| THINLY LAMINATED  | < 0.008 FEET  |   |  |                   |                   |  |                   |             |             |  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>INDURATION</b></p> <p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p>FRIABLE RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.</p> <p>MODERATELY INDURATED GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.</p> <p>INDURATED GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.</p> <p>EXTREMELY INDURATED SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.</p>  |   |   |  |                   |                   |  |                   |             |             | <p style="text-align: center;"><b>NOTES:</b></p> <p>FIAD: FILLED IMMEDIATELY AFTER DRILLING</p>  |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |
| <p style="text-align: center;"><b>BENCH MARK: BYI-102; -YI- STA. 7+71.38, (874,678 FT. N, 1,777,494 FT. E)</b></p>  |   |   |  |                   |                   |  |                   |             |             | <p style="text-align: center;"><b>ELEVATION: 874.57 FEET</b></p>   |   |  |  |  |   |  |             |   |  |  |  |   |             |  |  |               |                         |                    |                  |  |                   |                  |              |     |     |     |     |            |     |          |          |           |                   |      |              |                  |             |       |                |            |                     |  |  |   |  |  |  |                        |                   |                   |                   |                   |                   |                   |                   |             |             |             |             |                |                 |            |  |                            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                         |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                  |                |                   |                |                         |        |        |               |                       |        |         |                 |                    |         |          |               |                |       |       |                      |



SKEW:  
 A - 90°-09'-20"  
 B - 89°-27'-36"



|  |                  |
|--|------------------|
| <b>PROJECT REFERENCE NO.</b>                           | <b>SHEET NO.</b> |
| U-2525C  | 4                |
| <b>END BENT NO. 1 CROSS SECTION<br/>AT STA. 329+44</b> |                  |



**(A) RESIDUAL:**  
MOIST, MEDIUM DENSE TO VERY DENSE,  
YELLOW TO WHITE TO GRAY TO BROWN,  
SILTY, FINE TO COARSE SAND WITH ROCK  
FRAGMENTS

**RWI-1**  
329+55  
117' LT  
BT  
DRY  
10/16

**EBI-A**  
329+43  
70' LT

**RESIDUAL:**  
MOIST, MEDIUM STIFF TO HARD,  
REDDISH BROWN TO YELLOWISH BROWN  
TO RED TO YELLOW, FINE TO  
COARSE SANDY CLAY AND FINE TO  
COARSE SANDY SILT

**WEATHERED ROCK:**  
LIGHT BROWNISH GRAY TO  
YELLOW AND WHITE,  
METAMORPHOSED GRANITE

**CRYSTALLINE ROCK:**  
GRAY, METAMORPHOSED GRANITE

**EBI-C**  
329+46  
1' LT

**EBI-B**  
329+40  
65' RT

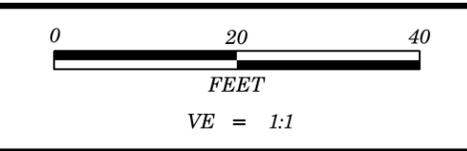
BT  
DRY  
10/16

**RWI-2**  
329+56  
139' RT  
BT  
DRY  
10/16

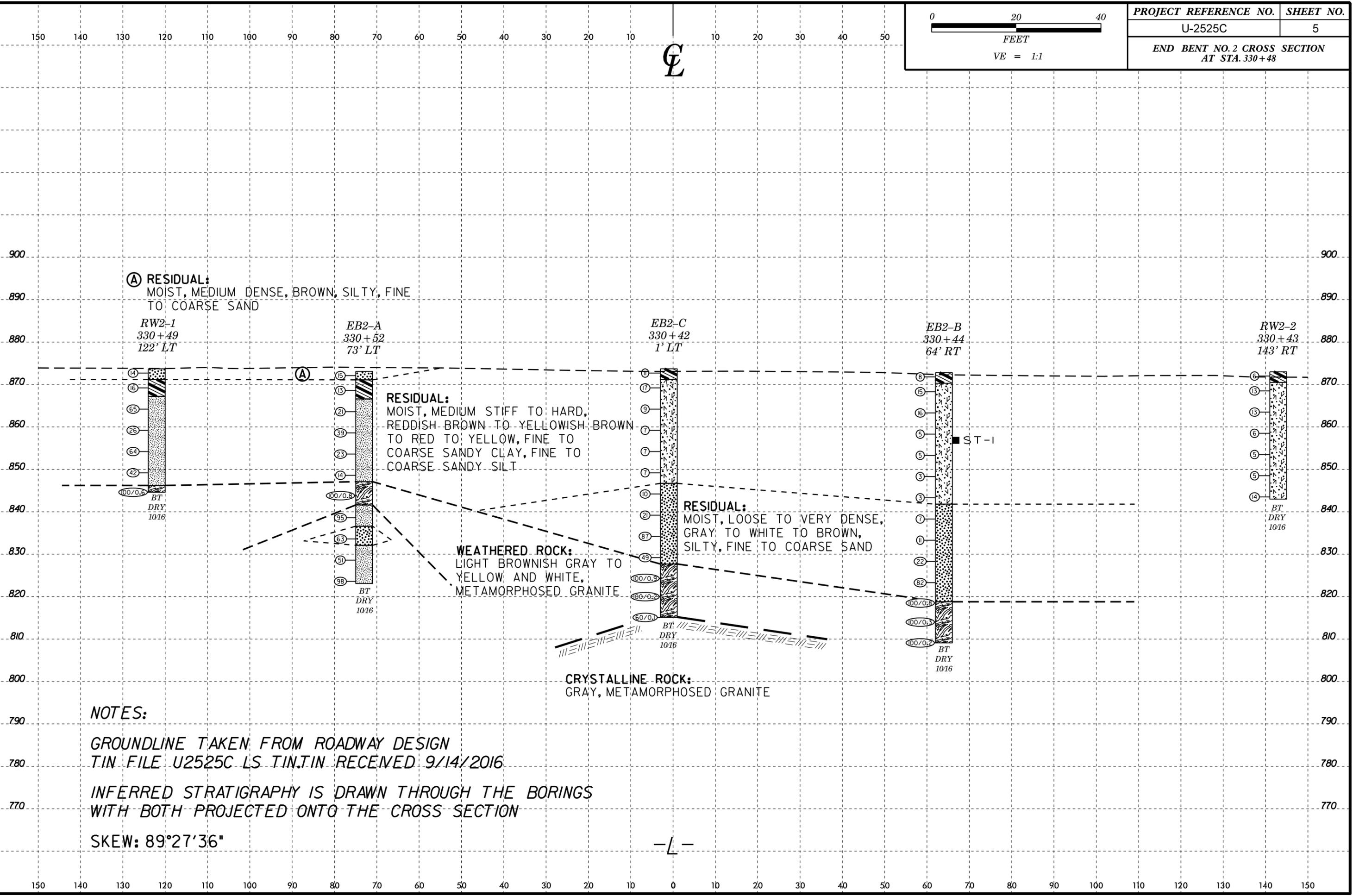
**NOTES:**  
GROUNDLINE TAKEN FROM ROADWAY DESIGN  
TIN FILE U2525C LS TIN.TIN RECEIVED 9/14/2016  
INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
WITH BOTH PROJECTED ONTO THE CROSS SECTION  
SKEW: 90°09'20"

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22-NOV-2016 04:20  
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 Wells At KA20215



|  |                  |
|--|------------------|
| <b>PROJECT REFERENCE NO.</b>                           | <b>SHEET NO.</b> |
| U-2525C  | 5                |
| <b>END BENT NO. 2 CROSS SECTION<br/>AT STA. 330+48</b> |                  |



**NOTES:**  
 GROUNDLINE TAKEN FROM ROADWAY DESIGN  
 TIN FILE U2525C\_LS\_TIN.TIN RECEIVED 9/14/2016  
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
 WITH BOTH PROJECTED ONTO THE CROSS SECTION  
 SKEW: 89°27'36"

# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |            |   |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|------------|---|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |            |   |
| BORING NO. EB1-A  |                 | STATION 329+43      |            | OFFSET 70 ft LT         |       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |            |   |
| COLLAR ELEV. 874.6 ft   |                 | TOTAL DEPTH 48.2 ft |            | NORTHING 874,587        |       | EASTING 1,777,555       |                 |    |    |     |           |     |                           |            |            |   |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |            |   |
| DRILLER Toothman, R.  |                 | START DATE 10/10/16 |            | COMP. DATE 10/10/16     |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |            |   |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |            |   |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     |                           | ELEV. (ft) | DEPTH (ft) |   |
| 875   | 874.6           | 0.0                 | 2          | 2                       | 5     |                         |                 |    |    |     |           |     |                           | 874.6      | 0.0        | GROUND SURFACE  |
| 870   | 871.6           | 3.0                 | 7          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            |            | RESIDUAL<br>Brown and Yellowish Brown to Red, Fine Sandy CLAY   |
|   | 866.6           | 8.0                 | 4          | 5                       | 5     |                         |                 |    |    |     |           |     |                           | 868.6      | 6.0        | Yellowish Brown and Yellow to Gray to Olive Yellow, Fine to Coarse Sandy SILT                                   |
| 860   | 861.6           | 13.0                | 3          | 4                       | 5     |                         |                 |    |    |     |           |     |                           |            |            |   |
|   | 856.6           | 18.0                | 5          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            |            |   |
| 850   | 851.6           | 23.0                | 5          | 10                      | 12    |                         |                 |    |    |     |           |     |                           |            |            |   |
|   | 846.6           | 28.0                | 5          | 8                       | 10    |                         |                 |    |    |     |           |     |                           |            |            |   |
| 840   | 841.6           | 33.0                | 12         | 15                      | 20    |                         |                 |    |    |     |           |     |                           |            |            |   |
|   | 836.6           | 38.0                | 84         | 16/0.1                  |       |                         |                 |    |    |     |           |     |                           | 838.1      | 36.5       | WEATHERED ROCK<br>Light Brownish Gray, METAMORPHOSED GRANITE  |
| 830   | 831.6           | 43.0                | 100/0.4    |                         |       |                         |                 |    |    |     |           |     |                           |            |            |   |
|   | 826.6           | 48.0                | 100/0.2    |                         |       |                         |                 |    |    |     |           |     |                           | 826.4      | 48.2       | Boring Terminated at Elevation 826.4 ft in WEATHERED ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.4 foot |

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |            |  |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|------------|--|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |            |  |
| BORING NO. EB1-C  |                 | STATION 329+46      |            | OFFSET 1 ft LT          |       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |            |  |
| COLLAR ELEV. 876.9 ft   |                 | TOTAL DEPTH 63.3 ft |            | NORTHING 874,656        |       | EASTING 1,777,559       |                 |    |    |     |           |     |                           |            |            |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |            |  |
| DRILLER Toothman, R.  |                 | START DATE 10/06/16 |            | COMP. DATE 10/06/16     |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |            |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |            |  |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     |                           | ELEV. (ft) | DEPTH (ft) |  |
| 880   |                 |                     |            |                         |       |                         |                 |    |    |     |           |     |                           |            |            |  |
| 875   | 876.9           | 0.0                 | 5          | 6                       | 5     |                         |                 |    |    |     |           |     |                           | 876.9      | 0.0        | GROUND SURFACE   |
|   | 873.6           | 3.3                 | 6          | 9                       | 11    |                         |                 |    |    |     |           |     |                           |            |            | RESIDUAL<br>Red, Fine Sandy CLAY with Trace Mica   |
| 870   | 868.6           | 8.3                 | 5          | 5                       | 7     |                         |                 |    |    |     |           |     |                           | 870.4      | 6.5        | Red, Fine Sandy SILT with Trace Mica   |
|   | 863.6           | 13.3                | 8          | 11                      | 14    |                         |                 |    |    |     |           |     |                           | 865.4      | 11.5       | Red to Olive and Yellow to Light Brownish Gray, Fine Sandy SILT with Trace Mica  |
| 860   | 858.6           | 18.3                | 5          | 4                       | 6     |                         |                 |    |    |     |           |     |                           |            |            |  |
|   | 853.6           | 23.3                | 4          | 6                       | 10    |                         |                 |    |    |     |           |     |                           |            |            |  |
| 850   | 848.6           | 28.3                | 7          | 10                      | 12    |                         |                 |    |    |     |           |     |                           |            |            |  |
|   | 843.6           | 33.3                | 8          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            |            |  |
| 840   | 838.6           | 38.3                | 6          | 9                       | 12    |                         |                 |    |    |     |           |     |                           |            |            |  |
|   | 833.6           | 43.3                | 21         | 32                      | 51    |                         |                 |    |    |     |           |     |                           |            |            |  |
| 830   | 828.6           | 48.3                | 13         | 14                      | 18    |                         |                 |    |    |     |           |     |                           |            |            |  |
|   | 823.6           | 53.3                | 17         | 31                      | 58    |                         |                 |    |    |     |           |     |                           |            |            |  |
| 820   | 818.6           | 58.3                | 100/0.4    |                         |       |                         |                 |    |    |     |           |     |                           |            |            |  |
|   | 813.6           | 63.3                | 60/0.0     |                         |       |                         |                 |    |    |     |           |     |                           | 813.6      | 63.3       | Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 813.6 ft on CRYSTALLINE ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.4 foot |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_5\_6.GPJ\_NC\_DOT.GDT 9/29/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C             |            | COUNTY GUILFORD       |       | GEOLOGIST Kubinski, D.  |    |    |    |     |           |     |                           |            |  |     |
|---|-----------------|-------------------------|------------|-----------------------|-------|-------------------------|----|----|----|-----|-----------|-----|---------------------------|------------|--|-----|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                         |            |                       |       | GROUND WTR (ft)         |    |    |    |     |           |     |                           |            |  |     |
| BORING NO. EB1-B  |                 | STATION 329+40          |            | OFFSET 65 ft RT       |       | ALIGNMENT -L-           |    |    |    |     |           |     |                           |            |  |     |
| COLLAR ELEV. 877.6 ft   |                 | TOTAL DEPTH 63.3 ft     |            | NORTHING 874,721      |       | EASTING 1,777,572       |    |    |    |     |           |     |                           |            |  |     |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 | DRILL METHOD Mud Rotary |            | HAMMER TYPE Automatic |       |                         |    |    |    |     |           |     |                           |            |  |     |
| DRILLER Toothman, R.  |                 | START DATE 10/06/16     |            | COMP. DATE 10/06/16   |       | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |                           |            |  |     |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)              | BLOW COUNT |                       |       | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |  |     |
|   |                 |                         | 0.5ft      | 0.5ft                 | 0.5ft | 0                       | 25 | 50 | 75 | 100 |           |     |                           |            |  |     |
| 880   | 877.6           | 0.0                     |            |                       |       |                         |    |    |    |     |           |     |                           | 877.6      | GROUND SURFACE   | 0.0 |
| 875   | 874.6           | 3.0                     | 5          | 5                     | 6     | 11                      |    |    |    |     |           |     | M                         | 875.1      | RESIDUAL<br>Reddish Brown, Fine Sandy CLAY   | 2.5 |
| 870   | 869.6           | 8.0                     | 6          | 10                    | 12    | 22                      |    |    |    |     |           |     | M                         |            | Reddish Brown to Gray and Yellow to Light Brownish Gray, Fine to Coarse Sandy SILT with Trace Mica |     |
| 865   | 864.6           | 13.0                    | 3          | 4                     | 4     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 860   | 859.6           | 18.0                    | 3          | 4                     | 5     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 855   | 854.6           | 23.0                    | 3          | 2                     | 4     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 850   | 849.6           | 28.0                    | 5          | 6                     | 8     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 845   | 844.6           | 33.0                    | 2          | 3                     | 3     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 840   | 839.6           | 38.0                    | 2          | 2                     | 3     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 835   | 834.6           | 43.0                    | 3          | 3                     | 4     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 830   | 829.6           | 48.0                    | 3          | 6                     | 8     |                         |    |    |    |     |           |     | M                         |            |  |     |
| 825   | 824.6           | 53.0                    | 3          | 7                     | 13    |                         |    |    |    |     |           |     | M                         |            |  |     |
| 820   | 819.6           | 58.0                    | 40         | 60/0.3                |       |                         |    |    |    |     |           |     |                           |            |  |     |
| 815   | 814.6           | 63.0                    | 100/0.2    |                       |       |                         |    |    |    |     |           |     |                           |            |  |     |
|   |                 |                         | 100/0.3    |                       |       |                         |    |    |    |     |           |     |                           |            |  |     |
|   |                 |                         |            |                       |       |                         |    |    |    |     |           |     |                           |            |  |     |

| WBS 34821.1.5   |                 | TIP U-2525C             |            | COUNTY GUILFORD       |       | GEOLOGIST Kubinski, D.  |    |    |    |     |           |     |                           |            |   |      |
|---|-----------------|-------------------------|------------|-----------------------|-------|-------------------------|----|----|----|-----|-----------|-----|---------------------------|------------|---|------|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                         |            |                       |       | GROUND WTR (ft)         |    |    |    |     |           |     |                           |            |   |      |
| BORING NO. EB2-A  |                 | STATION 330+52          |            | OFFSET 73 ft LT       |       | ALIGNMENT -L-           |    |    |    |     |           |     |                           |            |   |      |
| COLLAR ELEV. 873.1 ft   |                 | TOTAL DEPTH 50.0 ft     |            | NORTHING 874,594      |       | EASTING 1,777,448       |    |    |    |     |           |     |                           |            |   |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 | DRILL METHOD Mud Rotary |            | HAMMER TYPE Automatic |       |                         |    |    |    |     |           |     |                           |            |   |      |
| DRILLER Toothman, R.  |                 | START DATE 10/03/16     |            | COMP. DATE 10/03/16   |       | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |                           |            |   |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)              | BLOW COUNT |                       |       | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|   |                 |                         | 0.5ft      | 0.5ft                 | 0.5ft | 0                       | 25 | 50 | 75 | 100 |           |     |                           |            |   |      |
| 875   | 873.1           | 0.0                     |            |                       |       |                         |    |    |    |     |           |     |                           | 873.1      | GROUND SURFACE  | 0.0  |
| 870   | 869.6           | 3.5                     | 4          | 6                     | 9     | 15                      |    |    |    |     |           |     | M                         | 871.1      | RESIDUAL<br>Brown to Tan, Silty, Fine SAND with Trace of Organic Matter | 2.0  |
| 865   | 864.6           | 8.5                     | 6          | 7                     | 6     | 13                      |    |    |    |     |           |     | M                         |            | Tan, Fine Sandy CLAY  |      |
| 860   | 859.6           | 13.5                    | 8          | 11                    | 10    | 21                      |    |    |    |     |           |     | W                         | 866.6      | Tan, Fine to Coarse Sandy SILT  | 6.5  |
| 855   | 854.6           | 18.5                    | 17         | 19                    | 20    | 39                      |    |    |    |     |           |     | W                         |            |   |      |
| 850   | 849.6           | 23.5                    | 6          | 8                     | 15    | 23                      |    |    |    |     |           |     | W                         |            |   |      |
| 845   | 844.6           | 28.5                    | 3          | 6                     | 8     | 14                      |    |    |    |     |           |     | W                         | 847.1      | WEATHERED ROCK<br>Tan, METAMORPHOSED GRANITE                            | 26.0 |
| 840   | 839.6           | 33.5                    | 53         | 47/0.3                |       |                         |    |    |    |     |           |     | W                         | 841.6      | RESIDUAL<br>Brown and Tan, Fine Sandy SILT with Trace Mica              | 31.5 |
| 835   | 834.6           | 38.5                    | 20         | 33                    | 62    |                         |    |    |    |     |           |     | W                         | 836.6      | Tan, Silty, Fine to Coarse SAND   | 36.5 |
| 830   | 829.6           | 43.5                    | 35         | 27                    | 36    |                         |    |    |    |     |           |     | W                         | 832.1      | Brown, Fine Sandy SILT with Trace Mica                                  | 41.0 |
| 825   | 824.6           | 48.5                    | 14         | 20                    | 31    |                         |    |    |    |     |           |     | W                         |            |   |      |
|   |                 |                         | 23         | 32                    | 66    |                         |    |    |    |     |           |     | W                         | 823.1      | Boring Terminated at Elevation 823.1 ft in RESIDUAL: Sandy SILT         | 50.0 |
|   |                 |                         |            |                       |       |                         |    |    |    |     |           |     |                           |            | Topsoil 0.0 to 0.3 foot   |      |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_5.6.GPJ\_NC\_DOT.GDT 9/29/17





# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C         |                          | COUNTY GUILFORD     |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |      |  |
|---|-----------------|---------------------|--------------------------|---------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|------|--|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |                          |                     |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |      |  |
| BORING NO. RW2-1  |                 | STATION 330+49      |                          | OFFSET 122 ft LT    |       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |      |  |
| COLLAR ELEV. 873.7 ft   |                 | TOTAL DEPTH 29.1 ft |                          | NORTHING 874,545    |       | EASTING 1,777,447       |                 |    |    |     |           |     |                           |            |      |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     | DRILL METHOD H.S. Augers |                     |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |      |  |
| DRILLER Toothman, R.  |                 | START DATE 10/05/16 |                          | COMP. DATE 10/05/16 |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |      |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT               |                     |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |      |  |
|   |                 |                     | 0.5ft                    | 0.5ft               | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     | ELEV. (ft)                | DEPTH (ft) |      |  |
| 875   | 873.7           | 0.0                 | 2                        | 5                   | 9     |                         |                 |    |    |     |           |     |                           | 873.7      | 0.0  | GROUND SURFACE   |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           | 871.2      | 2.5  | RESIDUAL<br>Brown, Silty, Fine SAND  |
| 870   | 870.2           | 3.5                 | 8                        | 8                   | 8     |                         |                 |    |    |     |           |     |                           | 867.2      | 6.5  | Yellowish Brown, Fine Sandy CLAY   |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |      | White and Yellow to Olive, Fine Sandy SILT with Trace Mica                       |
| 865   | 865.2           | 8.5                 | 31                       | 28                  | 37    |                         |                 |    |    |     |           |     |                           |            |      |  |
| 860   | 860.2           | 13.5                | 10                       | 10                  | 16    |                         |                 |    |    |     |           |     |                           |            |      |  |
| 855   | 855.2           | 18.5                | 11                       | 20                  | 44    |                         |                 |    |    |     |           |     |                           |            |      |  |
| 850   | 850.2           | 23.5                | 10                       | 15                  | 27    |                         |                 |    |    |     |           |     |                           |            |      |  |
| 845   | 845.2           | 28.5                | 88                       | 12/0.1              |       |                         |                 |    |    |     |           |     |                           | 846.2      | 27.5 | WEATHERED ROCK   |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           | 844.6      | 29.1 | Gray, METAMORPHOSED GRANITE  |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |      | Boring Terminated at Elevation 844.6 ft in WEATHERED ROCK: METAMORPHOSED GRANITE |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |      | Topsoil 0.0 to 0.9 foot  |

| WBS 34821.1.5   |                 | TIP U-2525C         |                          | COUNTY GUILFORD     |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |     |  |
|---|-----------------|---------------------|--------------------------|---------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|-----|--|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |                          |                     |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |     |  |
| BORING NO. RW2-2  |                 | STATION 330+43      |                          | OFFSET 143 ft RT    |       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |     |  |
| COLLAR ELEV. 873.0 ft   |                 | TOTAL DEPTH 30.0 ft |                          | NORTHING 874,809    |       | EASTING 1,777,474       |                 |    |    |     |           |     |                           |            |     |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     | DRILL METHOD H.S. Augers |                     |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |     |  |
| DRILLER Toothman, R.  |                 | START DATE 10/05/16 |                          | COMP. DATE 10/05/16 |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |     |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT               |                     |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |     |  |
|   |                 |                     | 0.5ft                    | 0.5ft               | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     | ELEV. (ft)                | DEPTH (ft) |     |  |
| 875   | 873.0           | 0.0                 | 1                        | 2                   | 4     |                         |                 |    |    |     |           |     |                           | 873.0      | 0.0 | GROUND SURFACE   |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           | 870.5      | 2.5 | RESIDUAL<br>Reddish Brown, Fine Sandy SILT                       |
| 870   | 869.5           | 3.5                 | 4                        | 6                   | 7     |                         |                 |    |    |     |           |     |                           |            |     | Reddish Brown to Yellow and Red, Fine Sandy SILT with Trace Mica |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |     |  |
| 865   | 864.5           | 8.5                 | 5                        | 5                   | 8     |                         |                 |    |    |     |           |     |                           |            |     |  |
| 860   | 859.5           | 13.5                | 3                        | 2                   | 4     |                         |                 |    |    |     |           |     |                           |            |     |  |
| 855   | 854.5           | 18.5                | 2                        | 2                   | 3     |                         |                 |    |    |     |           |     |                           |            |     |  |
| 850   | 849.5           | 23.5                | 2                        | 2                   | 3     |                         |                 |    |    |     |           |     |                           |            |     |  |
| 845   | 844.5           | 28.5                | 4                        | 5                   | 9     |                         |                 |    |    |     |           |     |                           |            |     |  |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |     | Boring Terminated at Elevation 843.0 ft in RESIDUAL: Sandy SILT  |
|   |                 |                     |                          |                     |       |                         |                 |    |    |     |           |     |                           |            |     | Topsoil 0.0 to 0.4 foot  |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_5\_6.GPJ\_NC\_DOT.GDT 9/29/17

**SUMMARY OF LABORATORY TEST DATA**

**PROJECT NO. 34821.1.5 (U-2525C)**

**COUNTY: GUILFORD**

**SITE #2 (STRUCTURE #2 AND #3) – BRIDGE NO. 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)**

| Sample No. | Boring Number | Station | Offset | Alignment | Sample Depth (ft.) | AASHTO Class | Atterberg Limits |      |      | Gradation Results |          |           |               |             |           |          |          |
|------------|---------------|---------|--------|-----------|--------------------|--------------|------------------|------|------|-------------------|----------|-----------|---------------|-------------|-----------|----------|----------|
|            |               |         |        |           |                    |              | L.L.             | P.L. | P.I. | Pass #10          | Pass #40 | Pass #200 | Retained #270 | Coarse Sand | Fine Sand | Silt (%) | Clay (%) |
| ST-1 *     | EB2-B         | 330+44  | 64' RT | -L-       | 15.1-16.8          | A-5 (3)      | 45               | 38   | 7    | 99.71             | 77.34    | 52.28     | 53.6          | 29.89       | 23.71     | 37.21    | 9.19     |

SS = Split-Barrel Sample (ASTM-D-1586) ST = Shelby Tube (Undisturbed) Sample

S = Grab Sample

NP -- Non Plastic

NA-- Non Applicable

\* CONSOLIDATION TEST RESULTS CAN BE FOUND UNDER SEPARATE COVER

Page: 1 of 1

Lab Technician: NCDOT Certification No.: 129-01-0411 – Geotechnics, Raleigh, NC

*Michael P. Smith*

**SITE PHOTOGRAPHS**



Profile View Looking South along -Y1-



Cross-Section View Looking East from End Bent 2

REFERENCE: U-2525C

PROJECT: 34821

|       |                             |           |              |
|-------|-----------------------------|-----------|--------------|
| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
| N.C.  | U-2525C                     | 1         | 76           |

**STATE OF NORTH CAROLINA**  
**DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**

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**STRUCTURE**

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**SUBSURFACE INVESTIGATION**

COUNTY GUILFORD

PROJECT DESCRIPTION GREENSBORO EASTERN LOOP  
FROM US 29 NORTH OF GREENSBORO TO SR  
2303 (LAWNDALE DRIVE)

SITE DESCRIPTION SITE #2 (STRUCTURE #2 AND #3)  
BRIDGE NO. 1241 AND 1242 ON I-85 BYPASS (-L-)  
OVER LEES CHAPEL ROAD (-YI-) CPT AND DMT  
TESTING

**CONTENTS**

| <u>SHEET NO.</u> | <u>DESCRIPTION</u>   |
|------------------|----------------------|
| 1                | TITLE SHEET          |
| 2, 2A            | LEGEND (SOIL & ROCK) |
| 3                | SITE PLAN            |
| 4-75             | CPT AND DMT REPORT   |

PERSONNEL

C. CHILDREY

B. RAMSEYER

INVESTIGATED BY T. WELLS

DRAWN BY T. WELLS

CHECKED BY X. BARRETT

SUBMITTED BY KLEINFELDER, INC.

DATE OCTOBER 2017

**CAUTION NOTICE**

THE SUBSURFACE INFORMATION AND THE SUBSURFACE INVESTIGATION ON WHICH IT IS BASED WERE MADE FOR THE PURPOSE OF STUDY, PLANNING AND DESIGN, AND NOT FOR CONSTRUCTION OR PAY PURPOSES. THE VARIOUS FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA AVAILABLE MAY BE REVIEWED OR INSPECTED IN RALEIGH BY CONTACTING THE N. C. DEPARTMENT OF TRANSPORTATION, GEOTECHNICAL ENGINEERING UNIT AT (919) 707-6850. THE SUBSURFACE PLANS AND REPORTS, FIELD BORING LOGS, ROCK CORES AND SOIL TEST DATA ARE NOT PART OF THE CONTRACT.

GENERAL SOIL AND ROCK STRATA DESCRIPTIONS AND INDICATED BOUNDARIES ARE BASED ON A GEOTECHNICAL INTERPRETATION OF ALL AVAILABLE SUBSURFACE DATA AND MAY NOT NECESSARILY REFLECT THE ACTUAL SUBSURFACE CONDITIONS BETWEEN BORINGS OR BETWEEN SAMPLED STRATA WITHIN THE BOREHOLE. THE LABORATORY SAMPLE DATA AND THE IN SITU (IN-PLACE) TEST DATA CAN BE RELIED ON ONLY TO THE DEGREE OF RELIABILITY INHERENT IN THE STANDARD TEST METHOD. THE OBSERVED WATER LEVELS OR SOIL MOISTURE CONDITIONS INDICATED IN THE SUBSURFACE INVESTIGATIONS ARE AS RECORDED AT THE TIME OF THE INVESTIGATION. THESE WATER LEVELS OR SOIL MOISTURE CONDITIONS MAY VARY CONSIDERABLY WITH TIME ACCORDING TO CLIMATIC CONDITIONS INCLUDING TEMPERATURES, PRECIPITATION AND WIND, AS WELL AS OTHER NON-CLIMATIC FACTORS.

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- BY HAVING REQUESTED THIS INFORMATION, THE CONTRACTOR SPECIFICALLY WAIVES ANY CLAIMS FOR INCREASED COMPENSATION OR EXTENSION OF TIME BASED ON DIFFERENCES BETWEEN THE CONDITIONS INDICATED HEREIN AND THE ACTUAL CONDITIONS AT THE PROJECT SITE.

Prepared in the Office of:



**KLEINFELDER**  
 Bright People. Right Solutions.  
 7343 WEST FRIENDLY AVE, SUITE B  
 GREENSBORO, NC 27410  
 ENGINEERING FIRM LICENSE NO. F-1143



DocuSigned by:  
Thomas R. Wells 10/23/2017  
 7DA5D2D0518F4B0  
 SIGNATURE DATE

**DOCUMENT NOT CONSIDERED FINAL  
 UNLESS ALL SIGNATURES COMPLETED**

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

**SUBSURFACE INVESTIGATION**

SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS  
(PAGE 1 OF 2)

| SOIL DESCRIPTION   |  |  |  |  |  |  |  |  |  | GRADATION  |  |  |  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6 |  |  |  |  |  |  |  |  |  | WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.<br>UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.<br>GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.  |  |  |  |  |  |  |  |  |  |
| SOIL LEGEND AND AASHTO CLASSIFICATION  |  |  |  |  |  |  |  |  |  | ANGULARITY OF GRAINS   |  |  |  |  |  |  |  |  |  |
| GENERAL CLASS. GRANULAR MATERIALS (<= 35% PASSING #200) SILT-CLAY MATERIALS (> 35% PASSING #200) ORGANIC MATERIALS   |  |  |  |  |  |  |  |  |  | MINERALOGICAL COMPOSITION  |  |  |  |  |  |  |  |  |  |
| GROUP CLASS. A-1, A-3, A-2, A-4, A-5, A-6, A-7, A-1-A2, A-3, A-4, A-5, A-6, A-7  |  |  |  |  |  |  |  |  |  | MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.  |  |  |  |  |  |  |  |  |  |
| SYMBOL   |  |  |  |  |  |  |  |  |  | COMPRESSIBILITY  |  |  |  |  |  |  |  |  |  |
| % PASSING #10, #40, #200   |  |  |  |  |  |  |  |  |  | SLIGHTLY COMPRESSIBLE LL < 31<br>MODERATELY COMPRESSIBLE LL = 31 - 50<br>HIGHLY COMPRESSIBLE LL > 50   |  |  |  |  |  |  |  |  |  |
| MATERIAL PASSING #40 LL, PI  |  |  |  |  |  |  |  |  |  | PERCENTAGE OF MATERIAL   |  |  |  |  |  |  |  |  |  |
| GROUP INDEX  |  |  |  |  |  |  |  |  |  | ORGANIC MATERIAL GRANULAR SOILS SILT - CLAY SOILS OTHER MATERIAL   |  |  |  |  |  |  |  |  |  |
| USUAL TYPES OF MAJOR MATERIALS   |  |  |  |  |  |  |  |  |  | TRACE OF ORGANIC MATTER 2 - 3% 3 - 5% TRACE 1 - 10%<br>LITTLE ORGANIC MATTER 3 - 5% 5 - 12% LITTLE 10 - 20%<br>MODERATELY ORGANIC 5 - 10% 12 - 20% SOME 20 - 35%<br>HIGHLY ORGANIC > 10% > 20% HIGHLY 35% AND ABOVE  |  |  |  |  |  |  |  |  |  |
| GEN. RATING AS SUBGRADE  |  |  |  |  |  |  |  |  |  | GROUND WATER   |  |  |  |  |  |  |  |  |  |
| EXCELLENT TO GOOD FAIR TO POOR FAIR TO POOR POOR UNSUITABLE  |  |  |  |  |  |  |  |  |  | ▽ WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING<br>▽ STATIC WATER LEVEL AFTER 24 HOURS<br>▽PW PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA<br>○ SPRING OR SEEP   |  |  |  |  |  |  |  |  |  |
| CONSISTENCY OR DENSENESS   |  |  |  |  |  |  |  |  |  | MISCELLANEOUS SYMBOLS  |  |  |  |  |  |  |  |  |  |
| PRIMARY SOIL TYPE COMPACTNESS OR CONSISTENCY RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE) RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> )   |  |  |  |  |  |  |  |  |  | ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION 25/025 DIP & DIP DIRECTION OF ROCK STRUCTURES<br>SOIL SYMBOL SPT DMT VST PMT TEST BORING<br>ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT AUGER BORING CONE PENETROMETER TEST<br>INFERRED SOIL BOUNDARY CORE BORING SOUNDING ROD<br>INFERRED ROCK LINE MONITORING WELL TEST BORING WITH CORE<br>ALLUVIAL SOIL BOUNDARY PIEZOMETER INSTALLATION SPT N-VALUE  |  |  |  |  |  |  |  |  |  |
| TEXTURE OR GRAIN SIZE  |  |  |  |  |  |  |  |  |  | RECOMMENDATION SYMBOLS   |  |  |  |  |  |  |  |  |  |
| U.S. STD. SIEVE SIZE OPENING (MM) 4 10 40 60 200 270 4.76 2.00 0.42 0.25 0.075 0.053   |  |  |  |  |  |  |  |  |  | UNDERCUT UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL<br>SHALLOW UNDERCUT UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK  |  |  |  |  |  |  |  |  |  |
| GRAIN SIZE MM 305 75 2.0 0.25 0.05 0.005 IN. 12 3  |  |  |  |  |  |  |  |  |  | ABBREVIATIONS  |  |  |  |  |  |  |  |  |  |
| SOIL MOISTURE - CORRELATION OF TERMS   |  |  |  |  |  |  |  |  |  | AR - AUGER REFUSAL MED. - MEDIUM VST - VANE SHEAR TEST<br>BT - BORING TERMINATED MICA - MICACEOUS WEA. - WEATHERED<br>CL - CLAY MOD. - MODERATELY ? - UNIT WEIGHT<br>CPT - CONE PENETRATION TEST NP - NON PLASTIC 7/2 - DRY UNIT WEIGHT<br>CSE. - COARSE PMT - PRESSUREMETER TEST SAMPLE ABBREVIATIONS<br>DMT - DILATOMETER TEST DPT - DYNAMIC PENETRATION TEST S - BULK<br>e - VOID RATIO SD. - SAND, SANDY SD. - SAND, SANDY SS - SPLIT SPOON<br>F - FINE SL. - SILT, SILTY ST - SHELBY TUBE<br>FOSS. - FOSSILIFEROUS SLI. - SLIGHTLY RS - ROCK<br>FRAC. - FRACTURED, FRACTURES TCR - TRICONE REFUSAL RT - RECOMPACTED TRIAXIAL<br>FRAGS. - FRAGMENTS w - MOISTURE CONTENT CBR - CALIFORNIA BEARING RATIO<br>HI. - HIGHLY v - VERY |  |  |  |  |  |  |  |  |  |
| PLASTICITY   |  |  |  |  |  |  |  |  |  | EQUIPMENT USED ON SUBJECT PROJECT  |  |  |  |  |  |  |  |  |  |
| PLASTICITY INDEX (PI) DRY STRENGTH   |  |  |  |  |  |  |  |  |  | DRILL UNITS: CME-45C ADVANCING TOOLS: CLAY BITS HAMMER TYPE: AUTOMATIC MANUAL<br>CME-55 6' CONTINUOUS FLIGHT AUGER CORE SIZE: B H<br>CME-550 8' HOLLOW AUGERS N<br>VANE SHEAR TEST HARD FACED FINGER BITS<br>PORTABLE HOIST TUNG-CARBIDE INSERTS CASING W/ ADVANCER<br>CONETEC 15 TON TRICONE STEEL TEETH TRICONE TUNG-CARB. CORE BIT<br>CORE BIT  |  |  |  |  |  |  |  |  |  |
| DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.   |  |  |  |  |  |  |  |  |  | HAND TOOLS: POST HOLE DIGGER HAND AUGER SOUNDING ROD VANE SHEAR TEST   |  |  |  |  |  |  |  |  |  |

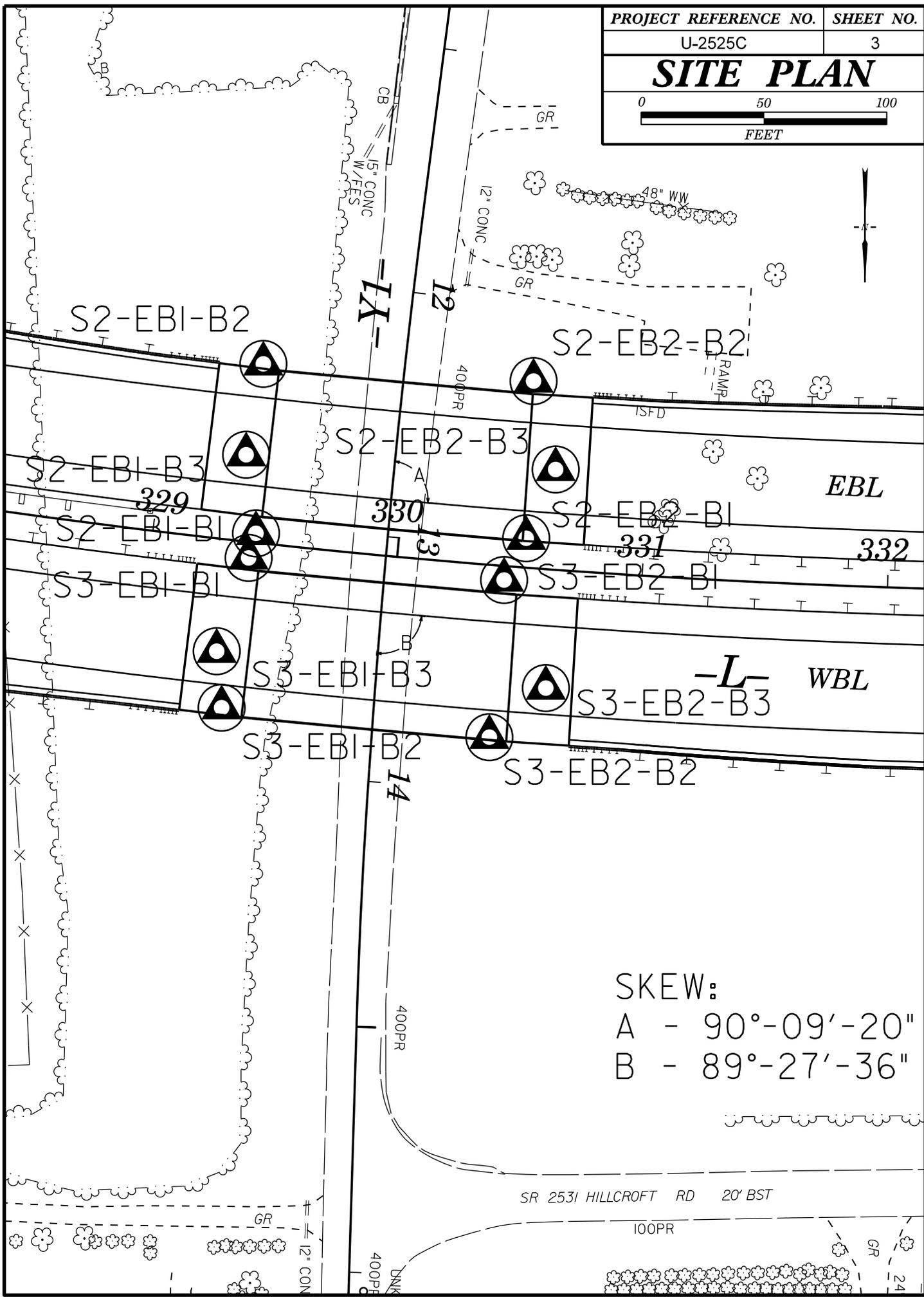
**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT**

# SUBSURFACE INVESTIGATION

## SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS (PAGE 2 OF 2)

| ROCK DESCRIPTION   |   | TERMS AND DEFINITIONS   |                   |
|--|---|---|-------------------|
| <p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED. AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p> |   | <p><b>ALLUVIUM (ALLUV.)</b> - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.<br/> <b>AQUIFER</b> - A WATER BEARING FORMATION OR STRATA.<br/> <b>ARENACEOUS</b> - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.<br/> <b>ARGILLACEOUS</b> - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.<br/> <b>ARTESIAN</b> - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.<br/> <b>CALCAREOUS (CALC.)</b> - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.<br/> <b>COLLUVIUM</b> - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.<br/> <b>CORE RECOVERY (REC.)</b> - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/> <b>DIKE</b> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.<br/> <b>DIP</b> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.<br/> <b>DIP DIRECTION (DIP AZIMUTH)</b> - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.<br/> <b>FAULT</b> - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.<br/> <b>FISSILE</b> - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.<br/> <b>FLOAT</b> - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.<br/> <b>FLOOD PLAIN (FP)</b> - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.<br/> <b>FORMATION (FM.)</b> - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.<br/> <b>JOINT</b> - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.<br/> <b>LEDGE</b> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.<br/> <b>LENS</b> - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.<br/> <b>MOTTLED (MOT.)</b> - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.<br/> <b>PERCHED WATER</b> - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.<br/> <b>RESIDUAL (RES.) SOIL</b> - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.<br/> <b>ROCK QUALITY DESIGNATION (RQD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/> <b>SAPROLITE (SAP.)</b> - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.<br/> <b>SILL</b> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRODUCED ROCKS.<br/> <b>SLICKENSIDE</b> - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.<br/> <b>STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)</b> - NUMBER OF BLOWS IN OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.<br/> <b>STRATA CORE RECOVERY (SREC.)</b> - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.<br/> <b>STRATA ROCK QUALITY DESIGNATION (SRQD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.<br/> <b>TOPSOIL (TS.)</b> - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p> |                   |
|  | <b>WEATHERING</b>   |   |                   |
| FRESH  | ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.   |   |                   |
| VERY SLIGHT (V SL.)  | ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.   |   |                   |
| SLIGHT (SL.)   | ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.   |   |                   |
| MODERATE (MOD.)  | SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.  |   |                   |
| MODERATELY SEVERE (MOD. SEV.)  | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK.<br><i>IF TESTED, WOULD YIELD SPT REFUSAL</i>  |   |                   |
| SEVERE (SEV.)  | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN.<br><i>IF TESTED, WOULD YIELD SPT N VALUES &gt; 100 BPF</i>  |   |                   |
| VERY SEVERE (V SEV.)   | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</i> |   |                   |
| COMPLETE   | ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.  |   |                   |
| <b>ROCK HARDNESS</b>   |   |   |                   |
| VERY HARD  | CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.   |   |                   |
| HARD   | CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.   |   |                   |
| MODERATELY HARD  | CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.   |   |                   |
| MEDIUM HARD  | CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.  |   |                   |
| SOFT   | CAN BE GROOVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.   |   |                   |
| VERY SOFT  | CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGERNAIL.   |   |                   |
| <b>FRACTURE SPACING</b>  |   | <b>BEDDING</b>  |                   |
| <b>TERM</b>  | <b>SPACING</b>  | <b>TERM</b>   | <b>THICKNESS</b>  |
| VERY WIDE  | MORE THAN 10 FEET   | VERY THICKLY BEDDED   | 4 FEET            |
| WIDE   | 3 TO 10 FEET  | THICKLY BEDDED  | 1.5 - 4 FEET      |
| MODERATELY CLOSE   | 1 TO 3 FEET   | THINLY BEDDED   | 0.16 - 1.5 FEET   |
| CLOSE  | 0.16 TO 1 FOOT  | VERY THINLY BEDDED  | 0.03 - 0.16 FEET  |
| VERY CLOSE   | LESS THAN 0.16 FEET   | THICKLY LAMINATED   | 0.008 - 0.03 FEET |
|  |   | THINLY LAMINATED  | < 0.008 FEET      |
| <b>INDURATION</b>  |   |   |                   |
| FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.  |   |   |                   |
| FRIABLE  | RUBBING WITH FINGER FREES NUMEROUS GRAINS;<br>GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.   |   |                   |
| MODERATELY INDURATED   | GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE;<br>BREAKS EASILY WHEN HIT WITH HAMMER.  |   |                   |
| INDURATED  | GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE;<br>DIFFICULT TO BREAK WITH HAMMER.   |   |                   |
| EXTREMELY INDURATED  | SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE;<br>SAMPLE BREAKS ACROSS GRAINS.  |   |                   |
|  |   | BENCH MARK: N/A   |                   |
|  |   | ELEVATION: N/A FEET   |                   |
| <b>NOTES:</b>  |   |   |                   |
| TOP OF CPT AND DMT ELEVATIONS OBTAINED FROM PROJECT TIN FILE (U2525C_LS_TIN.TIN) RECEIVED ON SEPTEMBER 14, 2016  |   |   |                   |
| DATE: 8-15-14  |   |   |                   |

|                       |           |
|-----------------------|-----------|
| PROJECT REFERENCE NO. | SHEET NO. |
| U-2525C               | 3         |
| <b>SITE PLAN</b>      |           |
|                       |           |



SKEW:  
A - 90°-09'-20"  
B - 89°-27'-36"

SR 2531 HILLCROFT RD 20' BST

100PR

## PRESENTATION OF SITE INVESTIGATION RESULTS

### SITE #2 (STRUCTURE #2 AND #3) – BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-) – Greensboro NC – Rev 04

*Prepared for:*

Kleinfelder

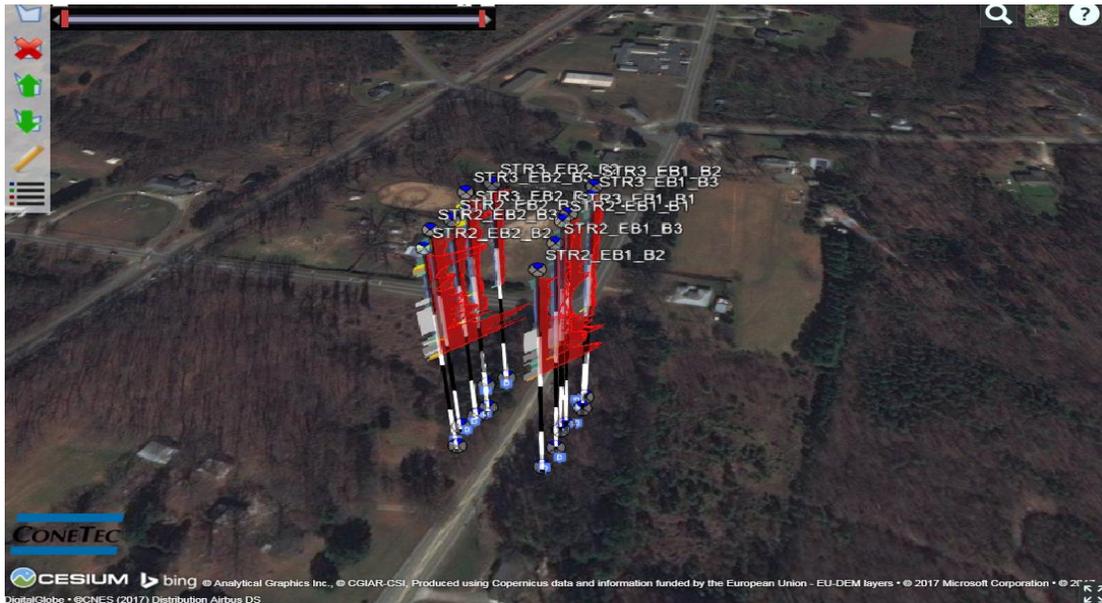
ConeTec Job No: 16-54112

Project Start Date: 19-DEC-2016

Project End Date: 21-DEC-2016

Report Date: 3-JAN-2017

Revision Date: 20-OCT-2017



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SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

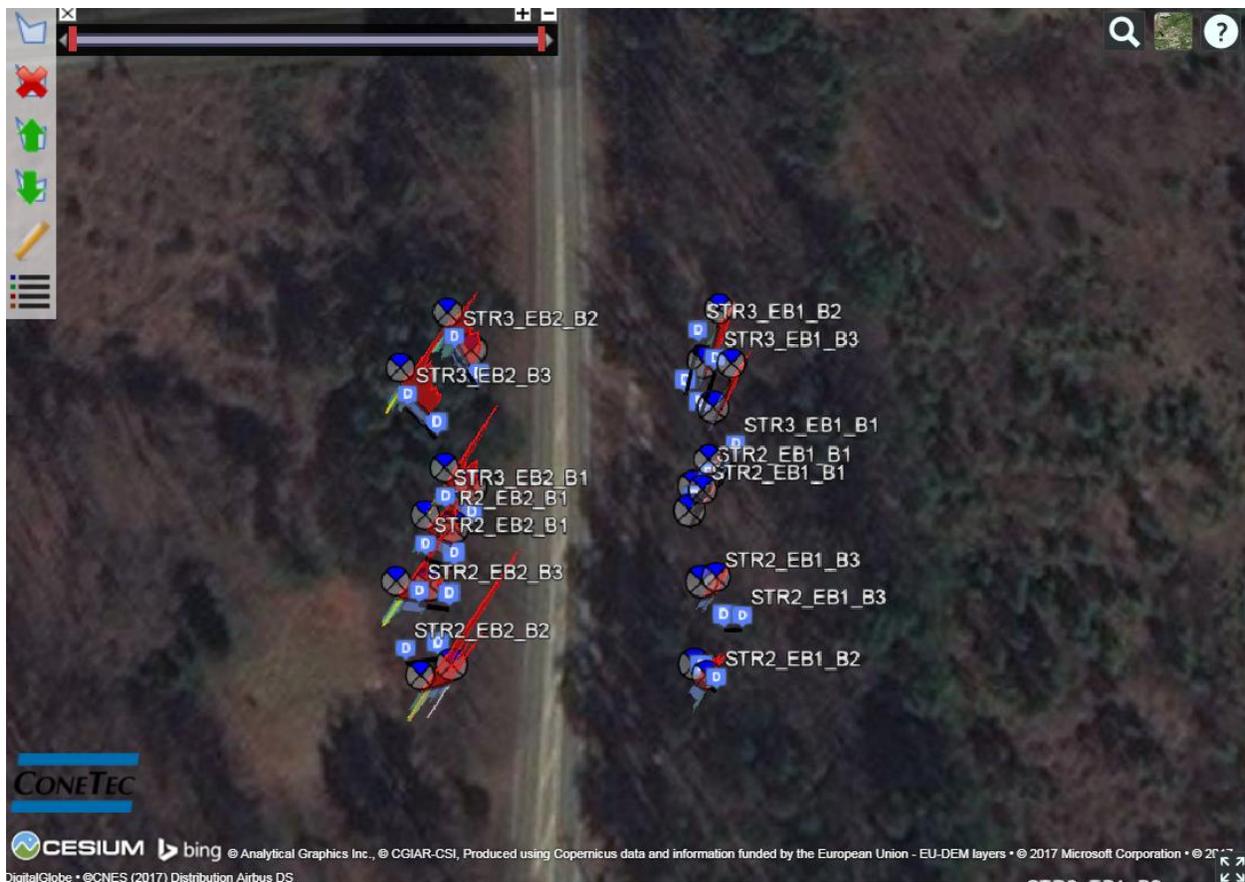
Introduction

The enclosed report presents the results of the site investigation program conducted by ConeTec Inc. for Kleinfelder at SITE #2 (STRUCTURE #2 AND #3) – BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-) in Greensboro, NC. The program consisted of 12 cone penetration tests (CPTu) and 12 flat plate dilatometer tests (DMT) at locations selected and labeled under the direction of Kleinfelder personnel. The purpose of the program was to evaluate existing site conditions.

Project Information

|                        |   |
|------------------------|---|
| Project                |   |
| Client                 | Kleinfelder   |
| Project                | SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-) |
| ConeTec project number | 16-54112  |

A map from Google Earth including the CPT and DMT test locations is presented below.



| Rig Description      | Deployment System     | Test Type |
|----------------------|-----------------------|-----------|
| 25 Ton CPT Truck Rig | Integrated CPT Ramset | CPTu, DMT |



SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

| Coordinates |                   |             |
|-------------|-------------------|-------------|
| Test Type   | Collection Method | EPSG Number |
| CPTu, DMT   | Handheld GPS      | 4326        |

| Cone Penetration Test (CPT) |   |
|-----------------------------|---|
| Depth reference             | Depths are referenced to the existing ground surface at the time of each test |
| Tip and sleeve data offset  | 0.1 meter<br>This has been accounted for in the CPT data files                |

| Cone Penetrometers Used for this Project |             |   |                                |                    |                       |                              |
|--|-------------|---|--------------------------------|--------------------|-----------------------|------------------------------|
| Cone Description                         | Cone Number | Cross Sectional Area (cm <sup>2</sup> ) | Sleeve Area (cm <sup>2</sup> ) | Tip Capacity (bar) | Sleeve Capacity (bar) | Pore Pressure Capacity (psi) |
| 367:T1500F15U500                         | AD367       | 15                                      | 225                            | 1500               | 15                    | 500                          |
| Cone 367 was used for all CPT soundings  |             |   |                                |                    |                       |                              |

| Interpretation Tables  |  |
|------------------------|--|
| Additional information | <p>The Soil Behaviour Type (SBT) classification chart (Robertson et al., 1986 presented by Lunne, Robertson and Powell, 1997) was used to classify the soil for this project. A detailed set of CPT interpretations were generated and are provided in Excel format files in the release folder. The CPT interpretations are based on values of corrected tip (<math>q_t</math>), sleeve friction (<math>f_s</math>) and pore pressure (<math>u_2</math>) averaged over a user specified interval of 20 cm.</p> <p>Soils were classified as either drained or undrained based on the Soil Behaviour Type (SBT) classification chart (Robertson et al., 1986 presented by Lunne, Robertson and Powell, 1997).</p> |

| Flat Plate Dilatometer Test (DMT) |   |
|-----------------------------------|---|
| Depth reference                   | Depths are referenced to the existing ground surface at the time of each test           |
| Phreatic surface determination    | The phreatic surface is assumed not to be encountered within sounding exploration depth |

### Limitations

This report has been prepared for the exclusive use of Kleinfelder (Client) for the project titled "SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)". The report's contents may not be relied upon by any other party without the express written permission of ConeTec Inc. (ConeTec). ConeTec has provided site investigation services, prepared the factual data reporting, and provided geotechnical parameter calculations consistent with current best practices. No other warranty, expressed or implied, is made.

The information presented in the report document and the accompanying data set pertain to the specific project, site conditions and objectives described to ConeTec by the Client. In order to properly understand the factual data, assumptions and calculations, reference must be made to the documents provided and their accompanying data sets, in their entirety.

The cone penetration tests (CPTu) are conducted using an integrated electronic piezocone penetrometer and data acquisition system manufactured by Adara Systems Ltd. of Richmond, British Columbia, Canada.

ConeTec's piezocone penetrometers are compression type designs in which the tip and friction sleeve load cells are independent and have separate load capacities. The piezocones use strain gauged load cells for tip and sleeve friction and a strain gauged diaphragm type transducer for recording pore pressure. The piezocones also have a platinum resistive temperature device (RTD) for monitoring the temperature of the sensors, an accelerometer type dual axis inclinometer and a geophone sensor for recording seismic signals. All signals are amplified down hole within the cone body and the analog signals are sent to the surface through a shielded cable.

ConeTec penetrometers are manufactured with various tip, friction and pore pressure capacities in both 10 cm<sup>2</sup> and 15 cm<sup>2</sup> tip base area configurations in order to maximize signal resolution for various soil conditions. The specific piezocone used for each test is described in the CPT summary table presented in the first Appendix. The 15 cm<sup>2</sup> penetrometers do not require friction reducers as they have a diameter larger than the deployment rods. The 10 cm<sup>2</sup> piezocones use a friction reducer consisting of a rod adapter extension behind the main cone body with an enlarged cross sectional area (typically 44 mm diameter over a length of 32 mm with tapered leading and trailing edges) located at a distance of 585 mm above the cone tip.

The penetrometers are designed with equal end area friction sleeves, a net end area ratio of 0.8 and cone tips with a 60 degree apex angle.

All ConeTec piezocones can record pore pressure at various locations. Unless otherwise noted, the pore pressure filter is located directly behind the cone tip in the "u<sub>2</sub>" position (ASTM Type 2). The filter is 6 mm thick, made of porous plastic (polyethylene) having an average pore size of 125 microns (90-160 microns). The function of the filter is to allow rapid movements of extremely small volumes of water needed to activate the pressure transducer while preventing soil ingress or blockage.

The piezocone penetrometers are manufactured with dimensions, tolerances and sensor characteristics that are in general accordance with the current ASTM D5778 standard. ConeTec's calibration criteria also meet or exceed those of the current ASTM D5778 standard. An illustration of the piezocone penetrometer is presented in Figure CPTu.

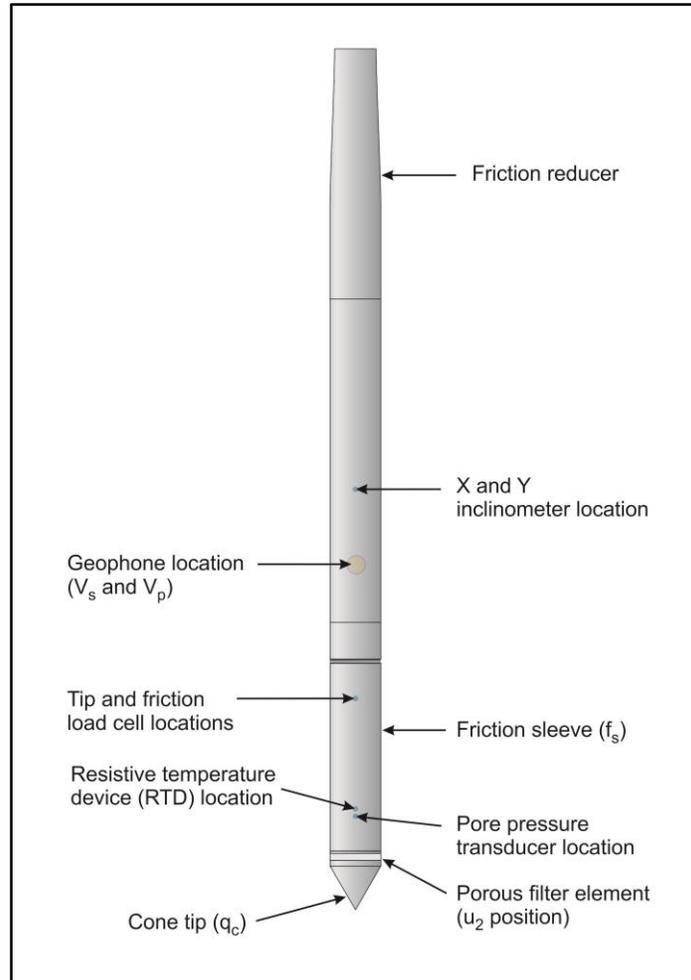


Figure CPTu. Piezocone Penetrometer (15 cm<sup>2</sup>)

The ConeTec data acquisition systems consist of a Windows based computer and a signal conditioner and power supply interface box with a 16 bit (or greater) analog to digital (A/D) converter. The data is recorded at fixed depth increments using a depth wheel attached to the push cylinders or by using a spring loaded rubber depth wheel that is held against the cone rods. The typical recording intervals are either 2.5 cm or 5.0 cm depending on project requirements; custom recording intervals are possible. The system displays the CPTu data in real time and records the following parameters to a storage media during penetration:

- Depth
- Uncorrected tip resistance ( $q_c$ )
- Sleeve friction ( $f_s$ )
- Dynamic pore pressure ( $u$ )
- Additional sensors such as resistivity, passive gamma, ultra violet induced fluorescence, if applicable

All testing is performed in accordance to ConeTec's CPT operating procedures which are in general accordance with the current ASTM D5778 standard.

Prior to the start of a CPTu sounding a suitable cone is selected, the cone and data acquisition system are powered on, the pore pressure system is saturated with either glycerin or silicone oil and the baseline readings are recorded with the cone hanging freely in a vertical position.

The CPTu is conducted at a steady rate of 2 cm/s, within acceptable tolerances. Typically one meter length rods with an outer diameter of 1.5 inches are added to advance the cone to the sounding termination depth. After cone retraction final baselines are recorded.

Additional information pertaining to ConeTec's cone penetration testing procedures:

- Each filter is saturated in silicone oil or glycerin under vacuum pressure prior to use
- Recorded baselines are checked with an independent multi-meter
- Baseline readings are compared to previous readings
- Soundings are terminated at the client's target depth or at a depth where an obstruction is encountered, excessive rod flex occurs, excessive inclination occurs, equipment damage is likely to take place, or a dangerous working environment arises
- Differences between initial and final baselines are calculated to ensure zero load offsets have not occurred and to ensure compliance with ASTM standards

The interpretation of piezocone data for this report is based on the corrected tip resistance ( $q_t$ ), sleeve friction ( $f_s$ ) and pore water pressure ( $u$ ). The interpretation of soil type is based on the correlations developed by Robertson (1990) and Robertson (2009). It should be noted that it is not always possible to accurately identify a soil type based on these parameters. In these situations, experience, judgment and an assessment of other parameters may be used to infer soil behavior type.

The recorded tip resistance ( $q_c$ ) is the total force acting on the piezocone tip divided by its base area. The tip resistance is corrected for pore pressure effects and termed corrected tip resistance ( $q_t$ ) according to the following expression presented in Robertson et al, 1986:

$$q_t = q_c + (1-a) \cdot u_2$$

where:  $q_t$  is the corrected tip resistance

$q_c$  is the recorded tip resistance

$u_2$  is the recorded dynamic pore pressure behind the tip ( $u_2$  position)

$a$  is the Net Area Ratio for the piezocone (0.8 for ConeTec probes)

The sleeve friction ( $f_s$ ) is the frictional force on the sleeve divided by its surface area. As all ConeTec piezocones have equal end area friction sleeves, pore pressure corrections to the sleeve data are not required.

The dynamic pore pressure ( $u$ ) is a measure of the pore pressures generated during cone penetration. To record equilibrium pore pressure, the penetration must be stopped to allow the dynamic pore pressures to stabilize. The rate at which this occurs is predominantly a function of the permeability of the soil and the diameter of the cone.

The friction ratio ( $R_f$ ) is a calculated parameter. It is defined as the ratio of sleeve friction to the tip resistance expressed as a percentage. Generally, saturated cohesive soils have low tip resistance, high

friction ratios and generate large excess pore water pressures. Cohesionless soils have higher tip resistances, lower friction ratios and do not generate significant excess pore water pressure.

A summary of the CPTu soundings along with test details and individual plots are provided in the appendices. A set of interpretation files were generated for each sounding based on published correlations and are provided in Excel format in the data release folder. Information regarding the interpretation methods used is also included in the data release folder.

For additional information on CPTu interpretations, refer to Robertson et al. (1986), Lunne et al. (1997), Robertson (2009), Mayne (2013, 2014) and Mayne and Peuchen (2012).

The cone penetration test is halted at specific depths to carry out pore pressure dissipation (PPD) tests, shown in Figure PPD-1. For each dissipation test the cone and rods are decoupled from the rig and the data acquisition system measures and records the variation of the pore pressure ( $u$ ) with time ( $t$ ).

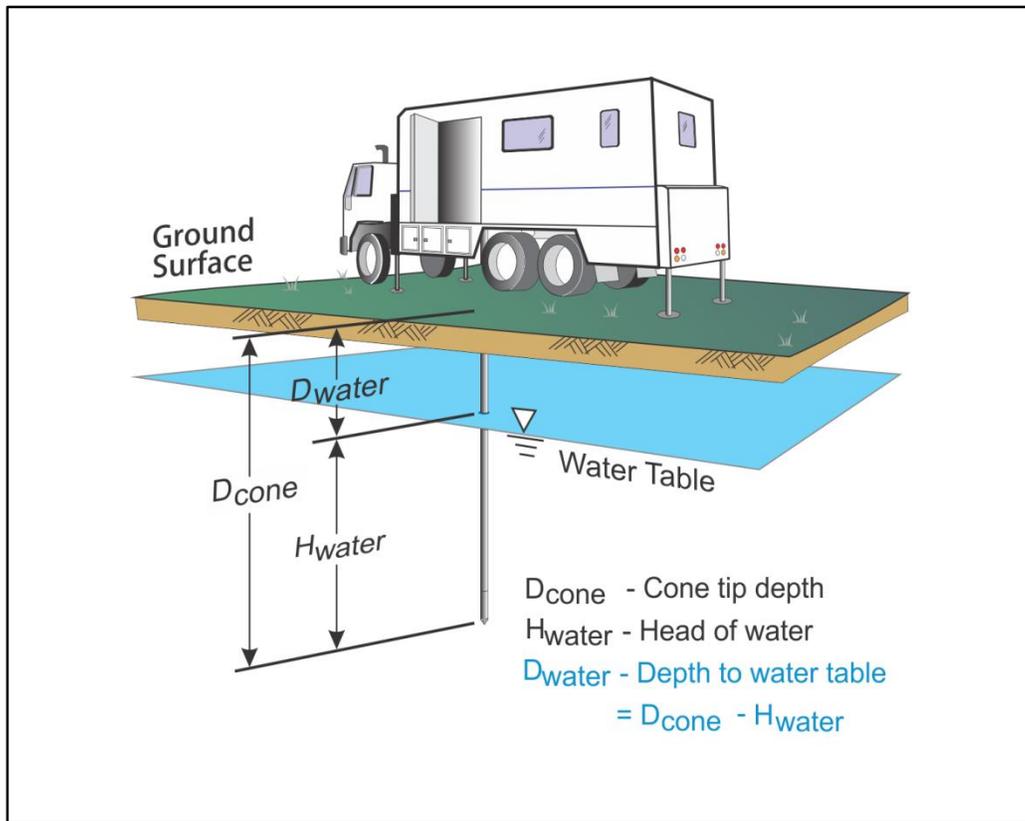


Figure PPD-1. Pore pressure dissipation test setup

Pore pressure dissipation data can be interpreted to provide estimates of ground water conditions, permeability, consolidation characteristics and soil behavior.

The typical shapes of dissipation curves shown in Figure PPD-2 are very useful in assessing soil type, drainage, in situ pore pressure and soil properties. A flat curve that stabilizes quickly is typical of a freely draining sand. Undrained soils such as clays will typically show positive excess pore pressure and have long dissipation times. Dilative soils will often exhibit dynamic pore pressures below equilibrium that then rise over time. Overconsolidated fine-grained soils will often exhibit an initial dilatatory response where there is an initial rise in pore pressure before reaching a peak and dissipating.

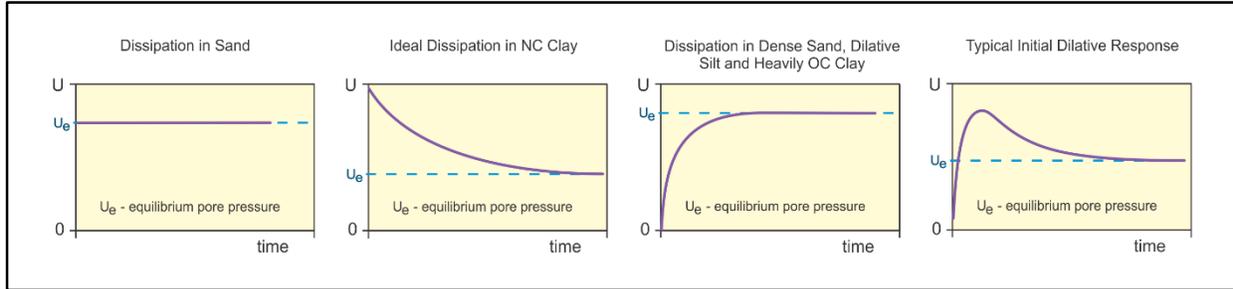


Figure PPD-2. Pore pressure dissipation curve examples

In order to interpret the equilibrium pore pressure ( $u_{eq}$ ) and the apparent phreatic surface, the pore pressure should be monitored until such time as there is no variation in pore pressure with time as shown for each curve of Figure PPD-2.

In fine grained deposits the point at which 100% of the excess pore pressure has dissipated is known as  $t_{100}$ . In some cases this can take an excessive amount of time and it may be impractical to take the dissipation to  $t_{100}$ . A theoretical analysis of pore pressure dissipations by Teh and Houlsby (1991) showed that a single curve relating degree of dissipation versus theoretical time factor ( $T^*$ ) may be used to calculate the coefficient of consolidation ( $c_h$ ) at various degrees of dissipation resulting in the expression for  $c_h$  shown below.

$$c_h = \frac{T^* \cdot a^2 \cdot \sqrt{I_r}}{t}$$

Where:

- $T^*$  is the dimensionless time factor (Table Time Factor)
- $a$  is the radius of the cone
- $I_r$  is the rigidity index
- $t$  is the time at the degree of consolidation

Table Time Factor.  $T^*$  versus degree of dissipation (Teh and Houlsby, 1991)

| Degree of Dissipation (%) | 20    | 30    | 40    | 50    | 60    | 70    | 80   |
|---------------------------|-------|-------|-------|-------|-------|-------|------|
| $T^* (u_2)$               | 0.038 | 0.078 | 0.142 | 0.245 | 0.439 | 0.804 | 1.60 |

The coefficient of consolidation is typically analyzed using the time ( $t_{50}$ ) corresponding to a degree of dissipation of 50% ( $u_{50}$ ). In order to determine  $t_{50}$ , dissipation tests must be taken to a pressure less than  $u_{50}$ . The  $u_{50}$  value is half way between the initial maximum pore pressure and the equilibrium pore pressure value, known as  $u_{100}$ . To estimate  $u_{50}$ , both the initial maximum pore pressure and  $u_{100}$  must be known or estimated. Other degrees of dissipations may be considered, particularly for extremely long dissipations.

At any specific degree of dissipation the equilibrium pore pressure ( $u$  at  $t_{100}$ ) must be estimated at the depth of interest. The equilibrium value may be determined from one or more sources such as measuring the value directly ( $u_{100}$ ), estimating it from other dissipations in the same profile, estimating the phreatic surface and assuming hydrostatic conditions, from nearby soundings, from client provided information, from site observations and/or past experience, or from other site instrumentation.

For calculations of  $c_h$  (Teh and Houlsby, 1991),  $t_{50}$  values are estimated from the corresponding pore pressure dissipation curve and a rigidity index ( $I_r$ ) is assumed. For curves having an initial dilatatory response in which an initial rise in pore pressure occurs before reaching a peak, the relative time from the peak value is used in determining  $t_{50}$ . In cases where the time to peak is excessive,  $t_{50}$  values are not calculated.

Due to possible inherent uncertainties in estimating  $I_r$ , the equilibrium pore pressure and the effect of an initial dilatatory response on calculating  $t_{50}$ , other methods should be applied to confirm the results for  $c_h$ .

Additional published methods for estimating the coefficient of consolidation from a piezocone test are described in Burns and Mayne (1998, 2002), Jones and Van Zyl (1981), Robertson et al. (1992) and Sully et al. (1999).

A summary of the pore pressure dissipation tests and dissipation plots are presented in the relevant appendix.

## REFERENCES

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Flat plate dilatometer tests (DMT) are conducted using a flat steel blade with a thin, expandable, circular membrane mounted on one surface, a control unit and a compressed gas (typically nitrogen) supply. A photo of the system is presented in Figure DMT-1.

The dilatometer blade is connected to the up-hole control box by a pneumatic tube with an inner conductor wire. The tube is threaded through a set of steel push rods. The control unit has pressure gauges, an audio-visual signal, a gas flow control and vent valve. A syringe is used to quantify the stiffness of the blade membrane.



Figure DMT-1. Flat plate dilatometer system  
(Marchetti, <http://www.marchetti-dmt.it/pagespictures/blade&case.htm>)

Prior to conducting a DMT profile, the blade membrane stiffness is recorded according to the current ASTM D6635 specifications and the system is assembled and tested for any leaks.

The dilatometer blade is pushed into the ground to the desired depth from surface or through a cased hole using a CPT rig or a drill rig. The blade is inflated using compressed gas and up to three pressure readings are recorded, the A reading at zero deflection (lift-off) and the B reading when a deflection of 1.1 mm has been achieved. An optional C reading representing the closing pressure can be recorded by slowly deflating the membrane soon after B is reached. The blade is advanced to subsequent depths

and the test procedures are repeated at each test depth, up to the sounding termination depth. After the blade is retracted membrane stiffness values are recorded.

The dilatometer operating procedures are performed in general accordance with the current ASTM D6635 standard.

The interpretation of the dilatometer data is based on the pressure related parameters  $p_0$  and  $p_1$  that are derived from the recorded A and B pressure values corrected for membrane stiffness and the gauge zero offset. Figure DMT-2 shows  $p_0$  and  $p_1$ .

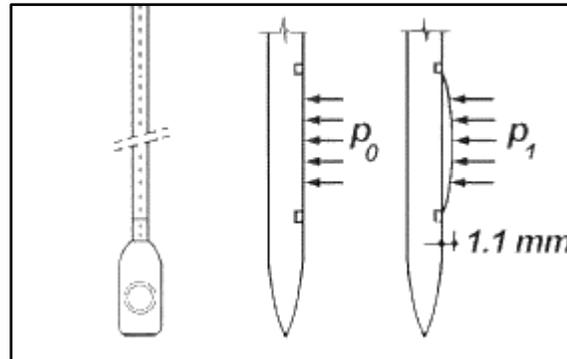


Figure DMT-2. Flat plate dilatometer  $p_0$  and  $p_1$   
(Marchetti, <http://www.marchetti-dmt.it/>)

The A reading is the pressure required to lift-off the membrane while the B reading is the pressure required to move the center of the membrane by 1.1 mm. The C pressure measurement is the pressure at which the membrane returns to the A position and is used to estimate equilibrium pore pressures in sand. The A and B pressure readings are corrected by the membrane stiffness values at the respective membrane deflections that are recorded before and after each test location.

The empirical correlations use the parameters  $p_0$ ,  $p_1$  and  $p_2$  derived from the A, B and C readings accounting for membrane stiffness and gauge offset. These parameters provide the basic values needed in the empirical correlations developed by Marchetti et al. (2001). The equations for these parameters are presented in the relevant appendix.

The  $p_0$ ,  $p_1$  and  $p_2$  parameters are used to calculate the DMT indices, material index ( $I_D$ ), horizontal stress index ( $K_D$ ), and dilatometer modulus ( $E_D$ ). Soil type is inferred from the material index. Clays generally have a material index of less than 0.6. The material index for silts is generally between 0.6 and 1.8, while sands generally exhibit a material index greater than 1.8. While  $K_D$  and  $E_D$  have limited direct use in geotechnical design, they are critical for determining parameters that are required for most design calculations such as earth pressure coefficient ( $K_0$ ), undrained shear strength ( $S_u$ ), and over consolidation ratio (OCR).

A summary of the tests including coordinates and estimated phreatic surface, along with plots and tabular results are provided in the relevant appendices. The calculated geotechnical parameters presented are based on published empirical correlations and are provided only as a first approximation. No warranty, expressed or implied, is made to the accuracy of these estimated geotechnical parameters.

References

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The appendices listed below are included in the report:

- Cone Penetration Test Summary and Standard Cone Penetration Test Plots
- Pore Pressure Dissipation Summary and Pore Pressure Dissipation Plots
- Flat Plate Dilatometer Test Summary, Plots and Tabular Results

Cone Penetration Test Summary and  
Standard Cone Penetration Test Plots

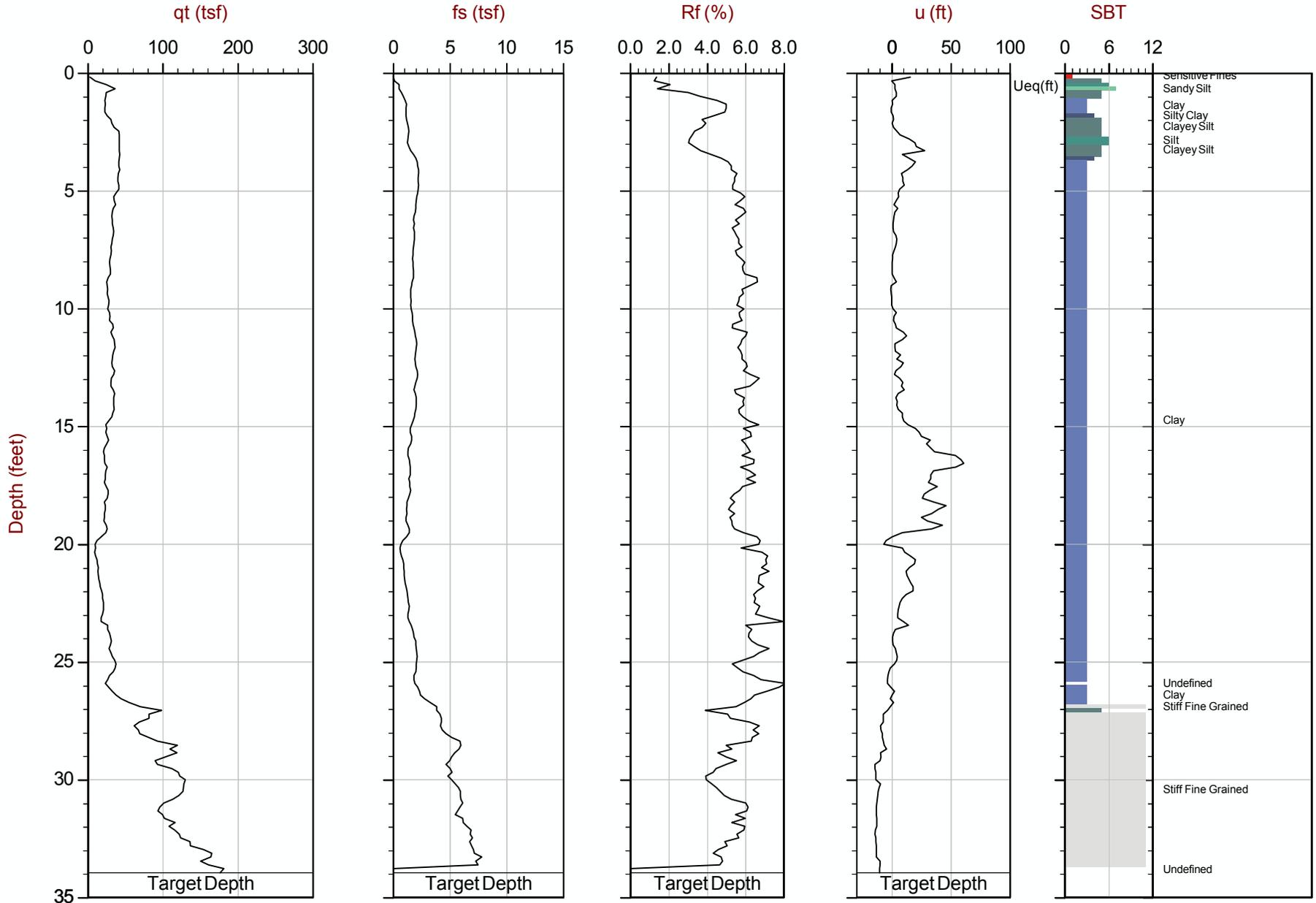


Job No: 16-54112  
Client: Kleinfelder  
Project: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Start Date: 19-Dec-2016  
End Date: 21-Dec-2016

### CONE PENETRATION TEST SUMMARY

| Sounding ID | File Name               | Date        | Cone             | Assumed Phreatic Surface <sup>1</sup> (ft) | Final Depth (ft) | Northing <sup>2</sup> (feet) | Easting (feet) | Refer to Notation Number |
|-------------|-------------------------|-------------|------------------|--|------------------|------------------------------|----------------|--------------------------|
| STR2_EB1_B1 | 16-54112_CP STR2_EB1_B1 | 19-Dec-2016 | 367:T1500F15U500 |  | 34.0             | 874653                       | 1777563        | 1                        |
| STR2_EB1_B2 | 16-54112_CP STR2_EB1_B2 | 19-Dec-2016 | 367:T1500F15U500 |  | 28.5             | 874584                       | 1777560        | 1                        |
| STR2_EB1_B3 | 16-54112_CP STR2_EB1_B3 | 19-Dec-2016 | 367:T1500F15U500 |  | 30.5             | 874621                       | 1777567        | 1                        |
| STR2_EB2_B1 | 16-54112_CP STR2_EB2_B1 | 19-Dec-2016 | 367:T1500F15U500 |  | 28.1             | 874655                       | 1777453        | 1                        |
| STR2_EB2_B2 | 16-54112_CP STR2_EB2_B2 | 19-Dec-2016 | 367:T1500F15U500 |  | 29.0             | 874591                       | 1777450        | 1                        |
| STR2_EB2_B3 | 16-54112_CP STR2_EB2_B3 | 19-Dec-2016 | 367:T1500F15U500 |  | 29.9             | 874627                       | 1777441        | 1                        |
| STR3_EB1_B1 | 16-54112_CP STR3_EB1_B1 | 19-Dec-2016 | 367:T1500F15U500 |  | 32.8             | 874663                       | 1777566        | 1                        |
| STR3_EB1_B2 | 16-54112_CP STR3_EB1_B2 | 19-Dec-2016 | 367:T1500F15U500 |  | 33.0             | 874724                       | 1777577        | 1                        |
| STR3_EB1_B3 | 16-54112_CP STR3_EB1_B3 | 19-Dec-2016 | 367:T1500F15U500 |  | 32.8             | 874701                       | 1777579        | 1                        |
| STR3_EB2_B1 | 16-54112_CP STR3_EB2_B1 | 19-Dec-2016 | 367:T1500F15U500 |  | 27.6             | 874672                       | 1777462        | 1                        |
| STR3_EB2_B2 | 16-54112_CP STR3_EB2_B2 | 19-Dec-2016 | 367:T1500F15U500 |  | 27.9             | 874736                       | 1777468        | 1                        |
| STR3_EB2_B3 | 16-54112_CP STR3_EB2_B3 | 19-Dec-2016 | 367:T1500F15U500 |  | 27.9             | 874716                       | 1777445        | 1                        |
| Totals      | 12 soundings            |             |                  |  | 361.9            |                              |                |                          |

1. Phreatic surface is assumed not to be encountered within exploration depth.
2. State Plane System 3200 - North Carolina. Coordinates were provided by client.

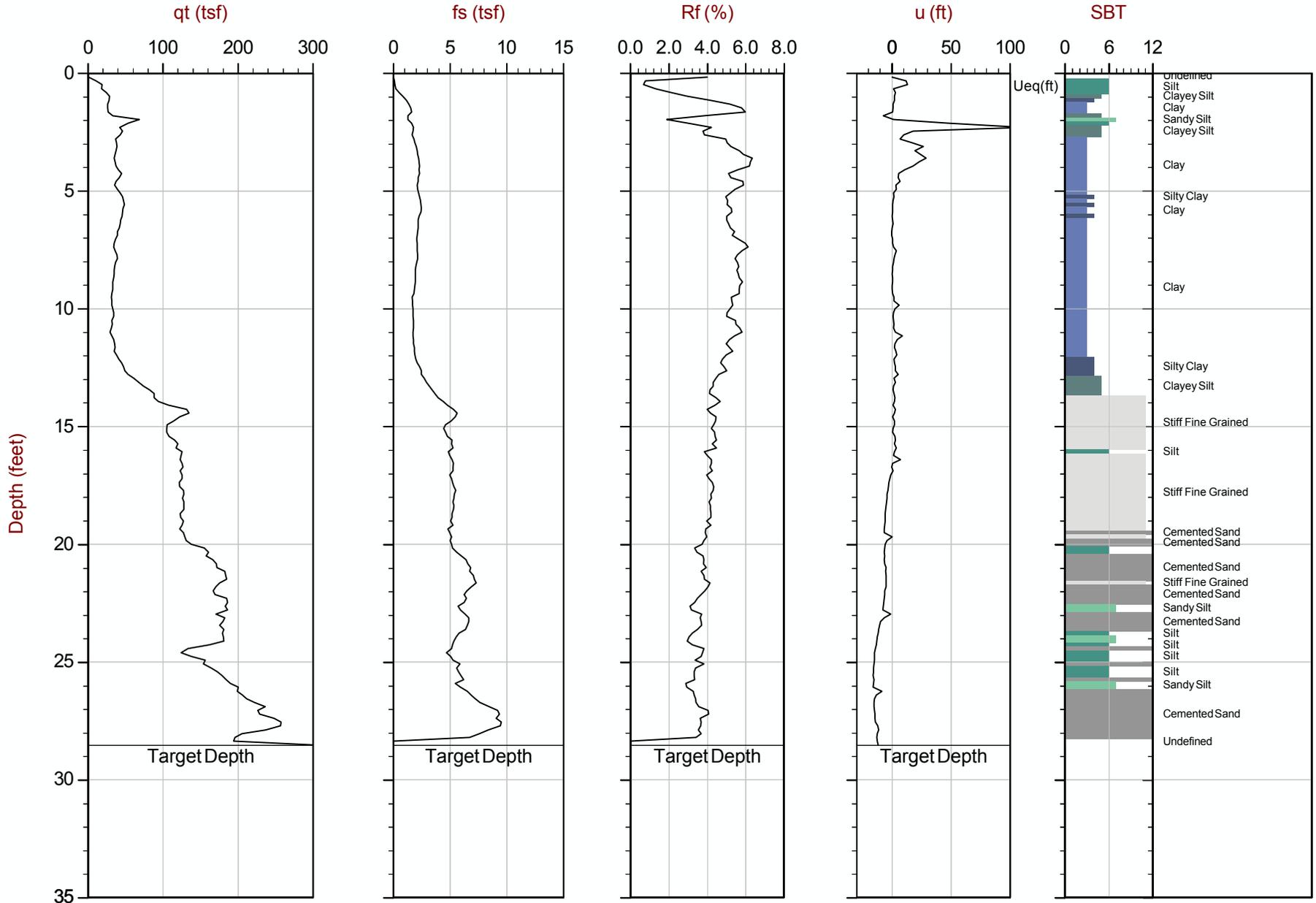


Max Depth: 10.350 m / 33.96 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB1\_B1.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874653 E: 177563 Elev: 876.9

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

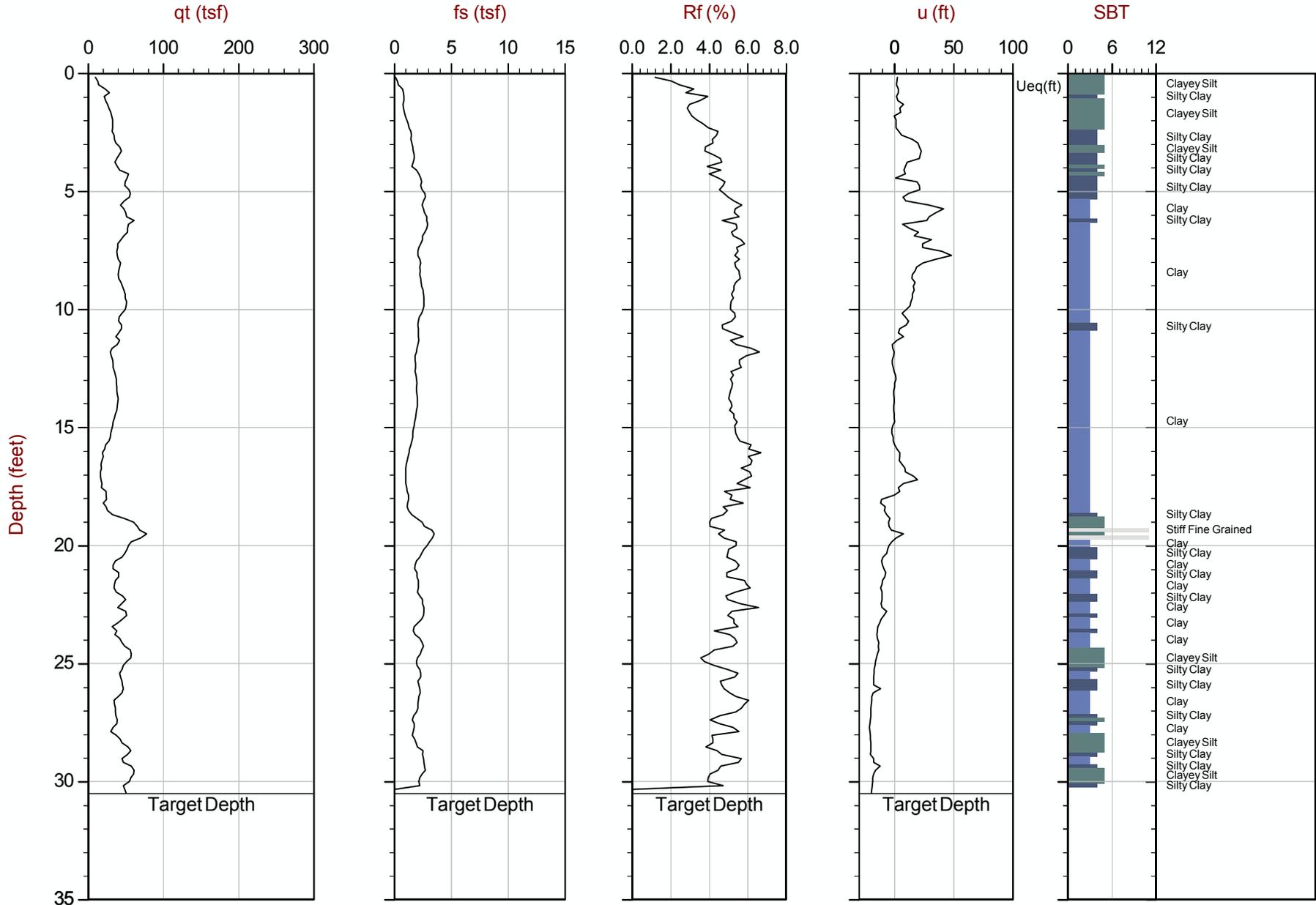


Max Depth: 8.700 m / 28.54 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB1\_B2.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874584 E: 1777560 Elev: 874.1

△ Dissipation with estimated Ueq value  
 △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

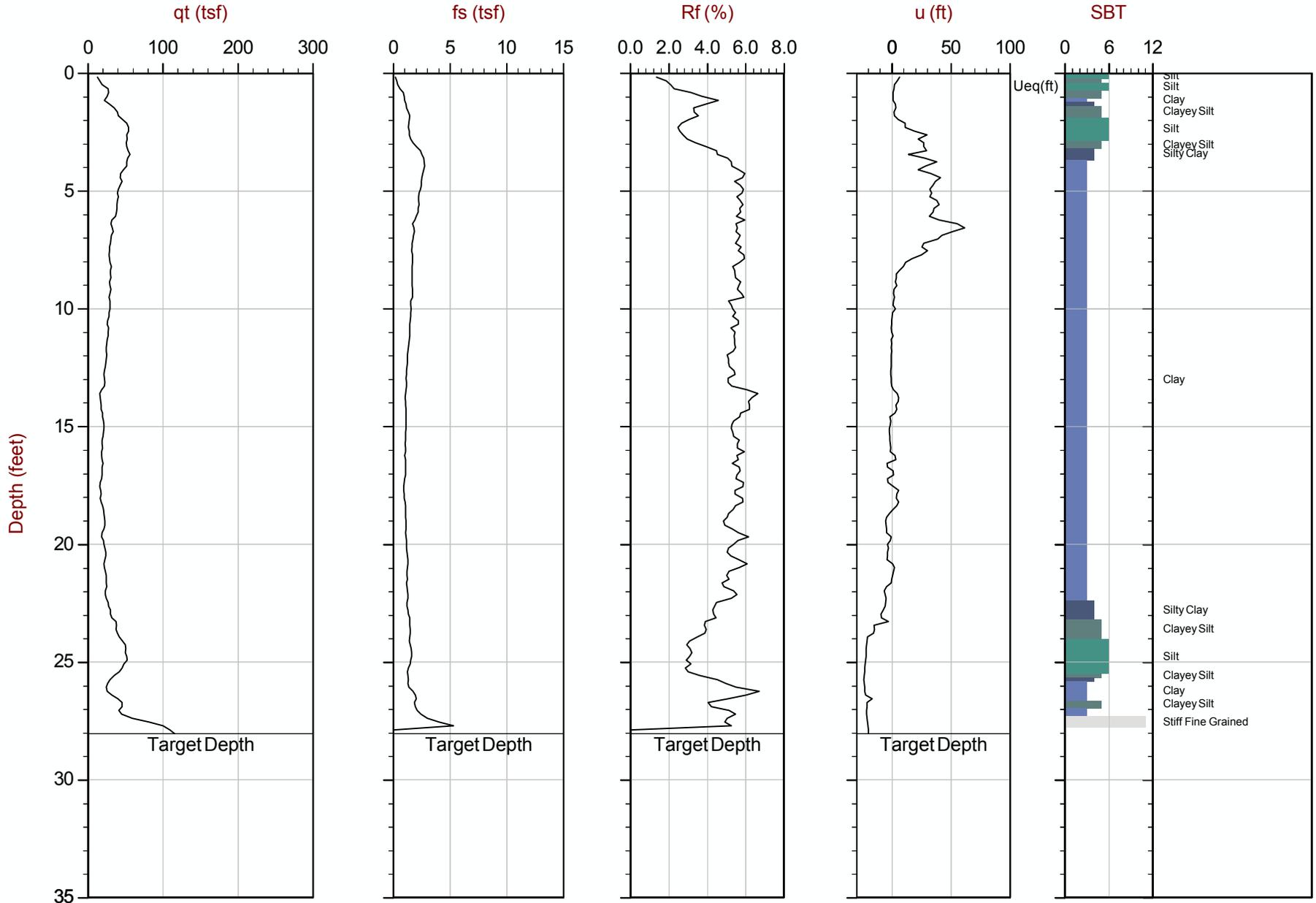


Max Depth: 9.300 m / 30.51 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB1\_B3.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874621 E: 1777567 Elev: 875.8

△ Dissipation with estimated Ueq value  
 △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

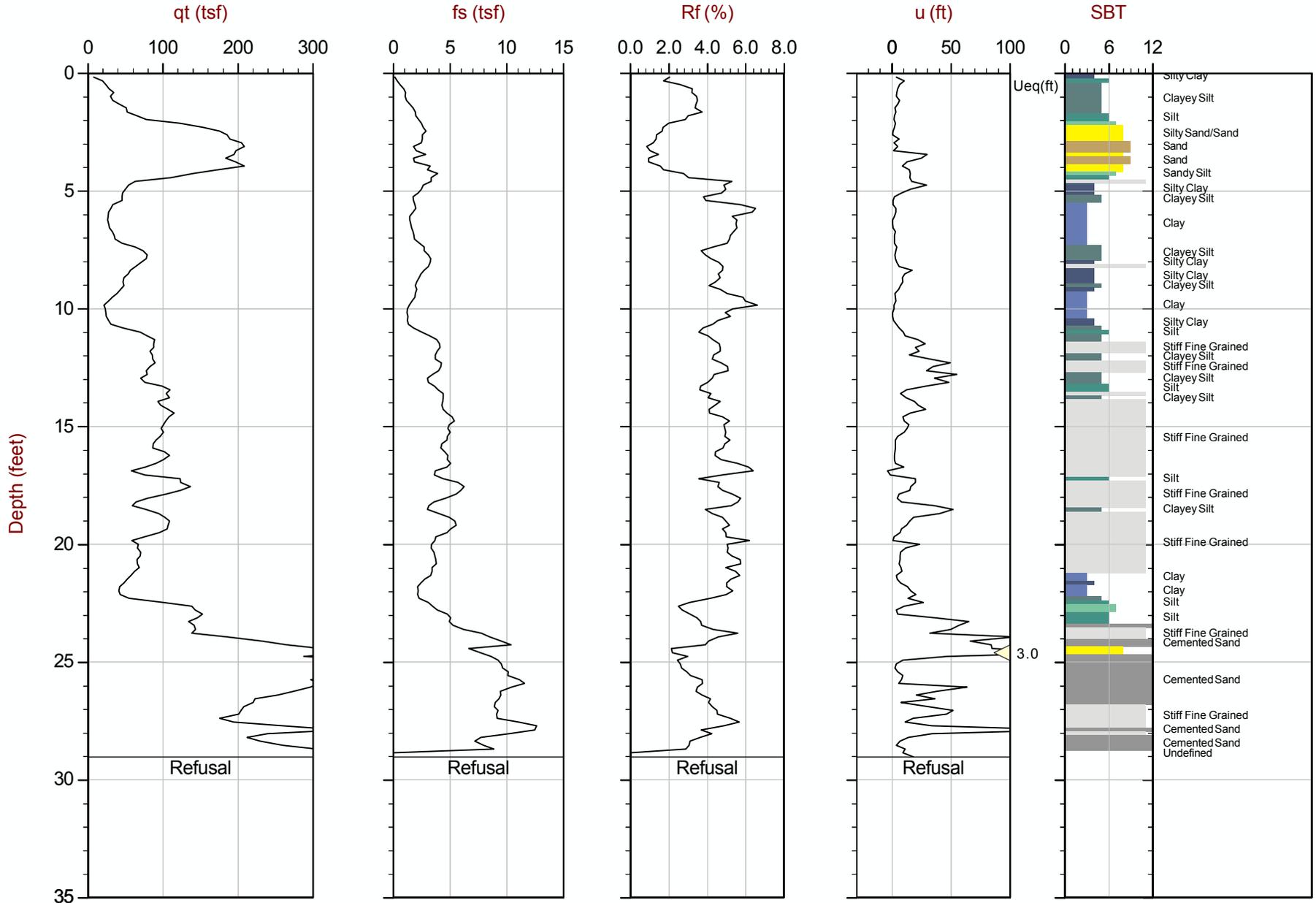


Max Depth: 8.550 m / 28.05 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB2\_B1.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874655 E: 1777453 Elev: 873.0

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

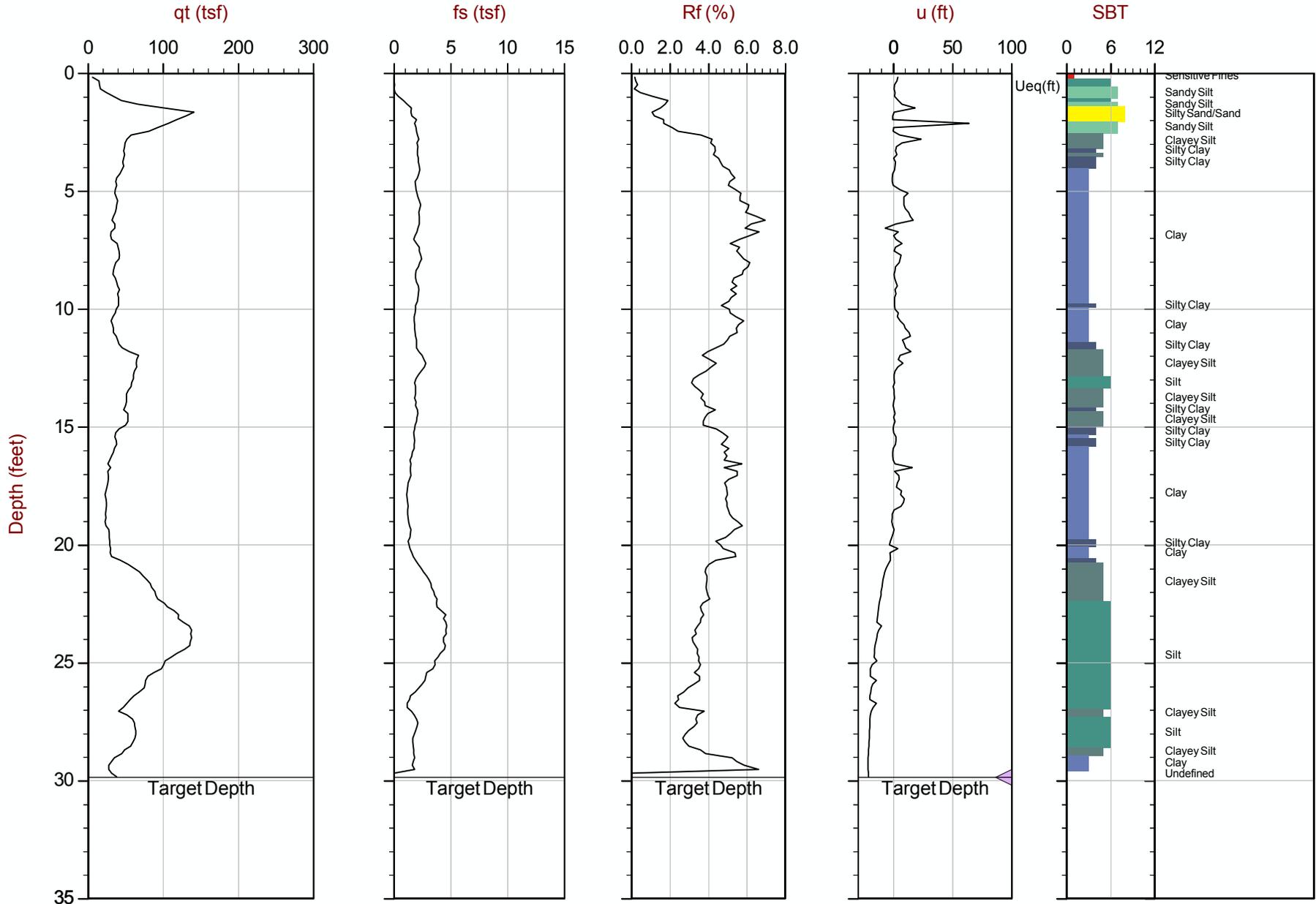


Max Depth: 8.850 m / 29.04 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB2\_B2.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874591 E: 1777450 Elev: 874.0

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

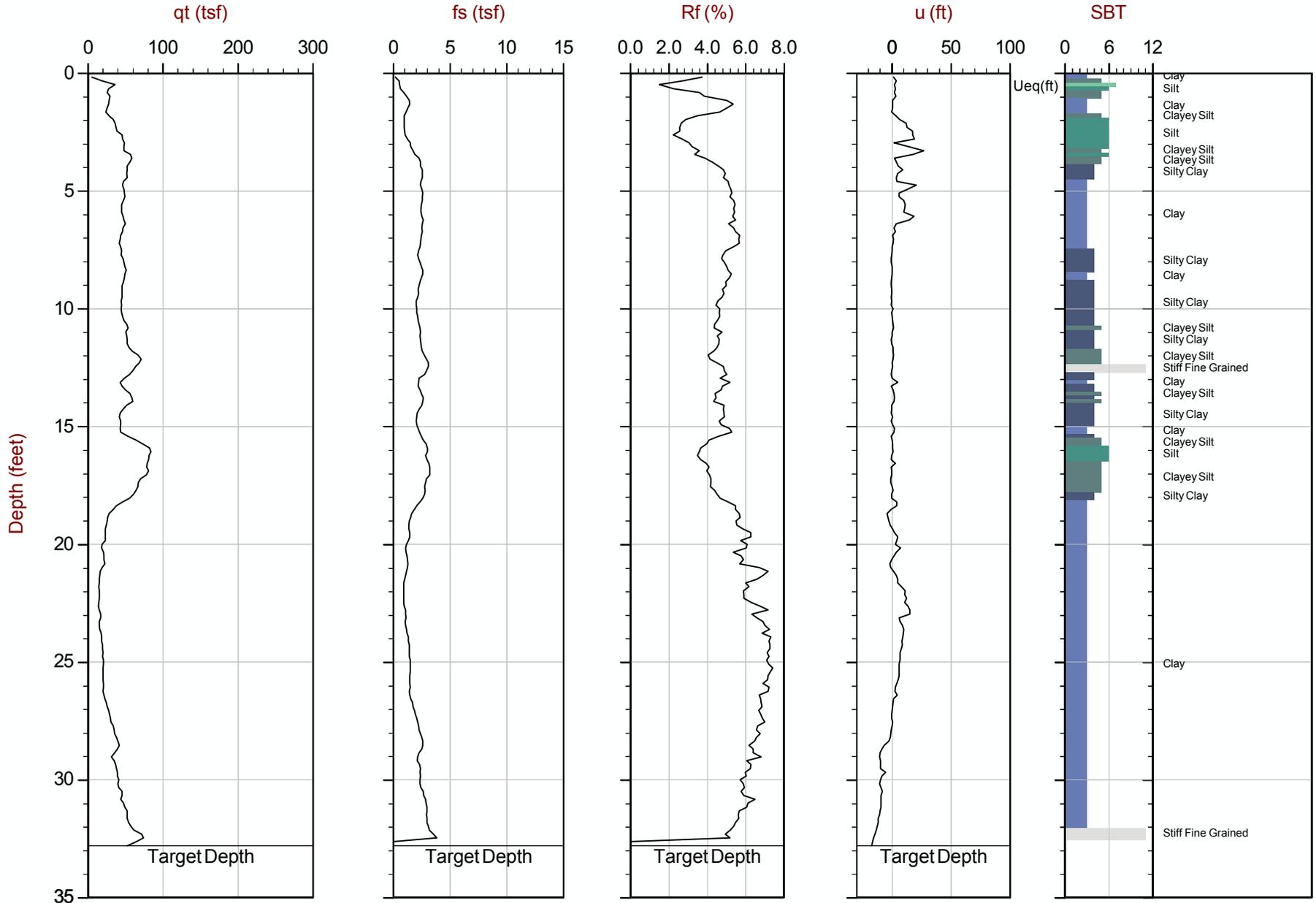


Max Depth: 9.100 m / 29.86 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR2\_EB2\_B3.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874627 E: 1777441 Elev: 873.4

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

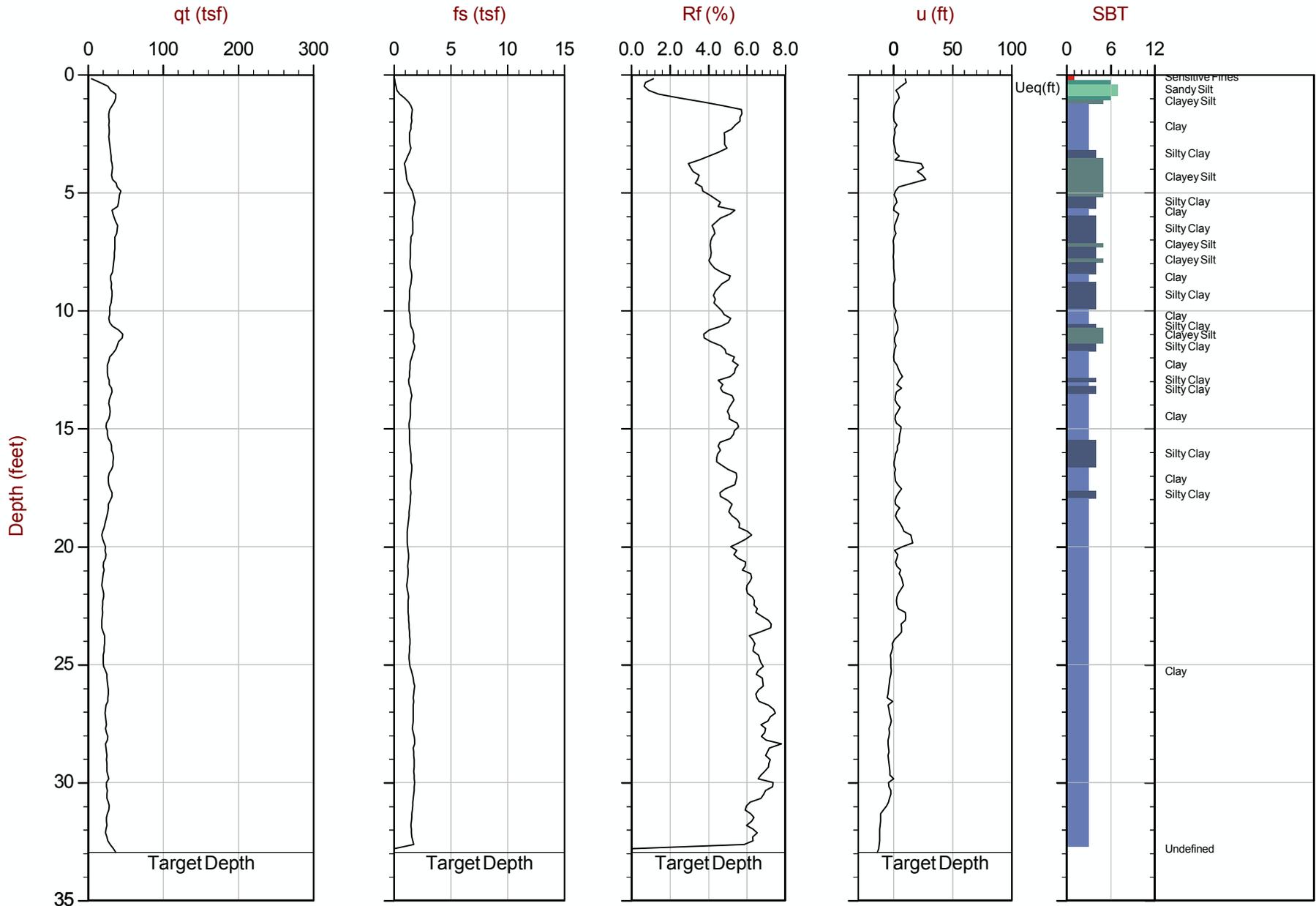


Max Depth: 10.000 m / 32.81 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB1\_B1.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874663 E: 1777566 Elev: 877.3

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

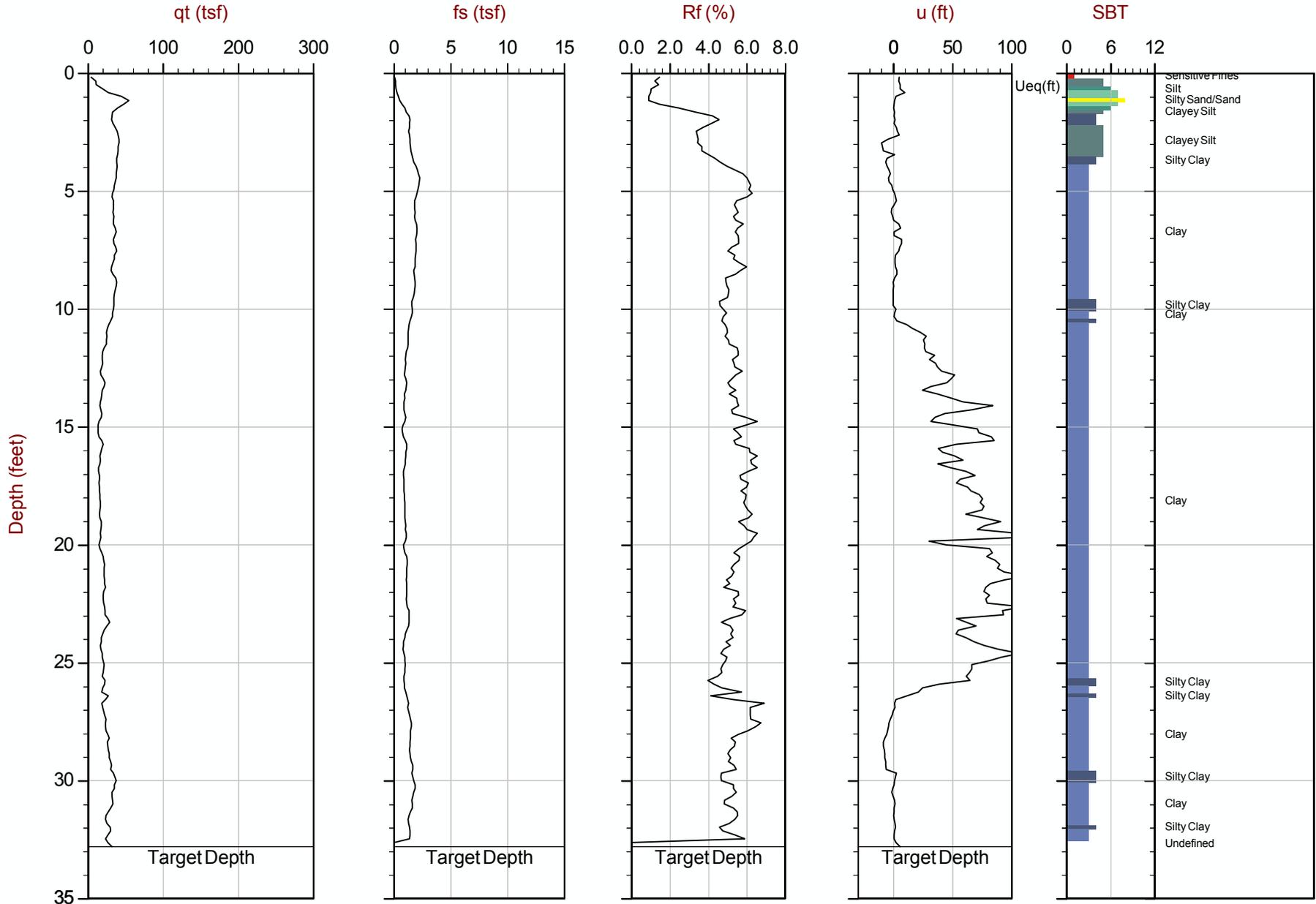


Max Depth: 10.050 m / 32.97 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB1\_B2.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874724 E: 1777577 Elev: 877.4

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

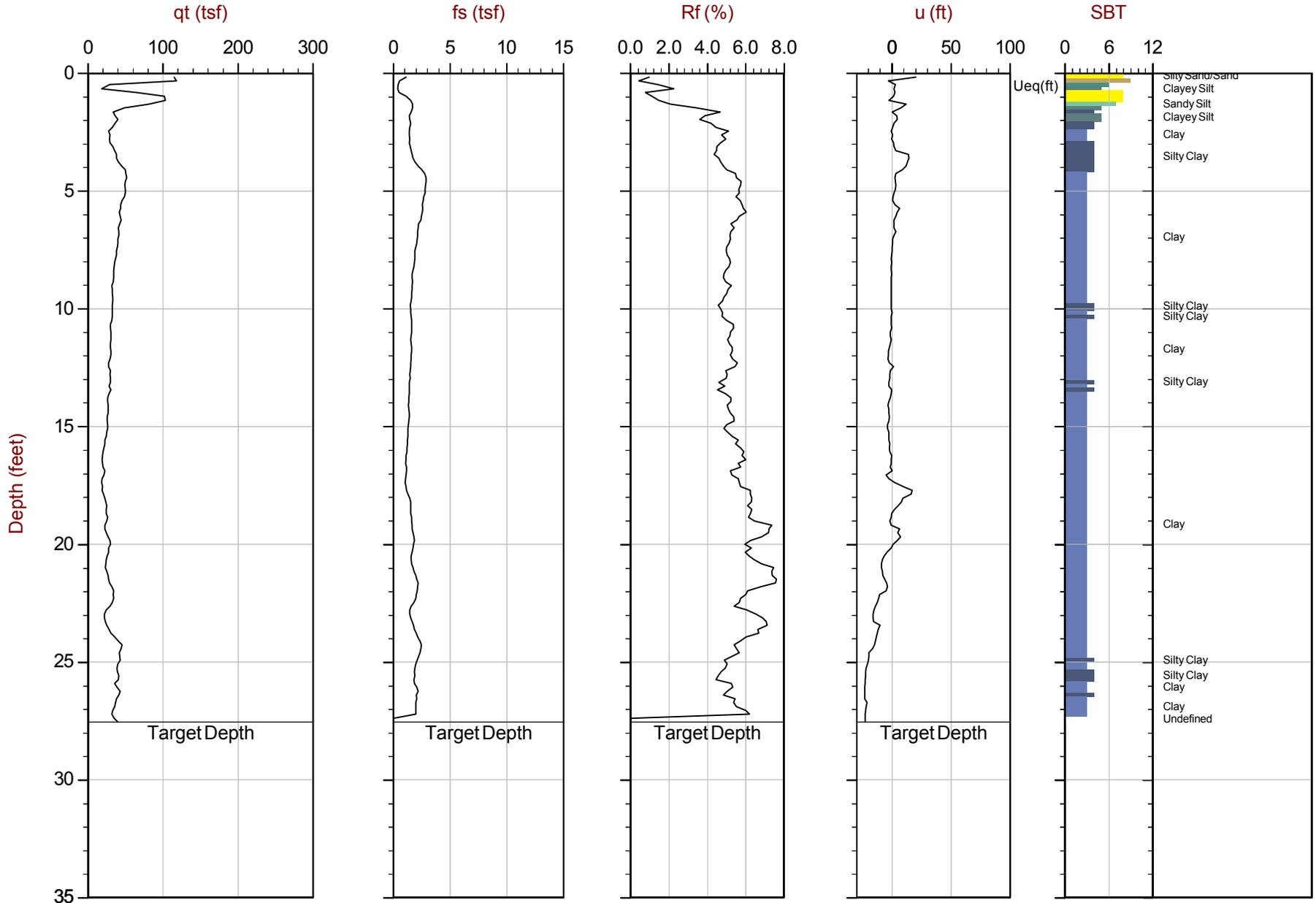


Max Depth: 10.000 m / 32.81 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB1\_B3.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874701 E: 1777579 Elev: 877.4

△ Dissipation with estimated Ueq value  
 △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

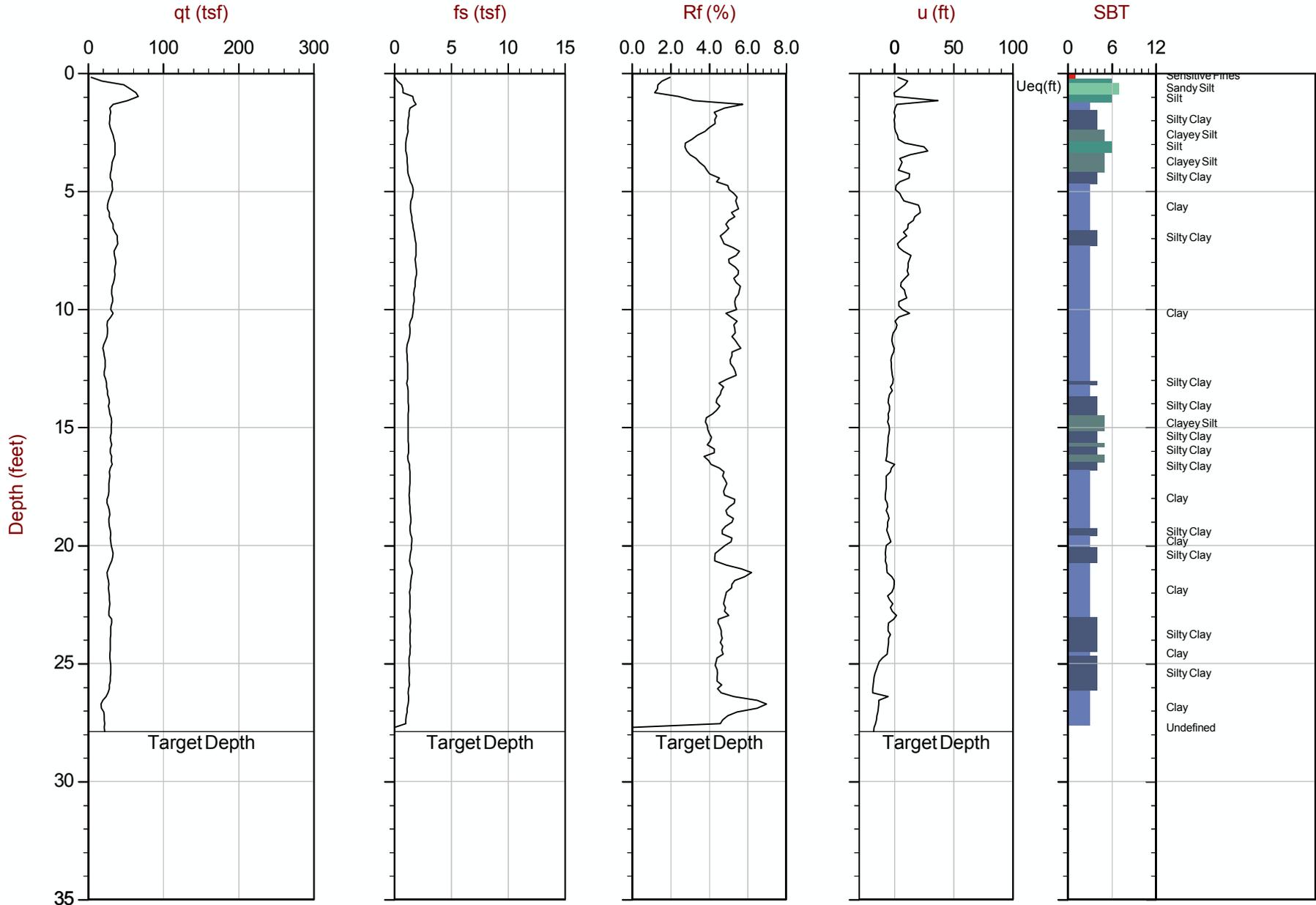


Max Depth: 8.400 m / 27.56 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB2\_B1.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874672 E: 1777462 Elev: 873.3

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

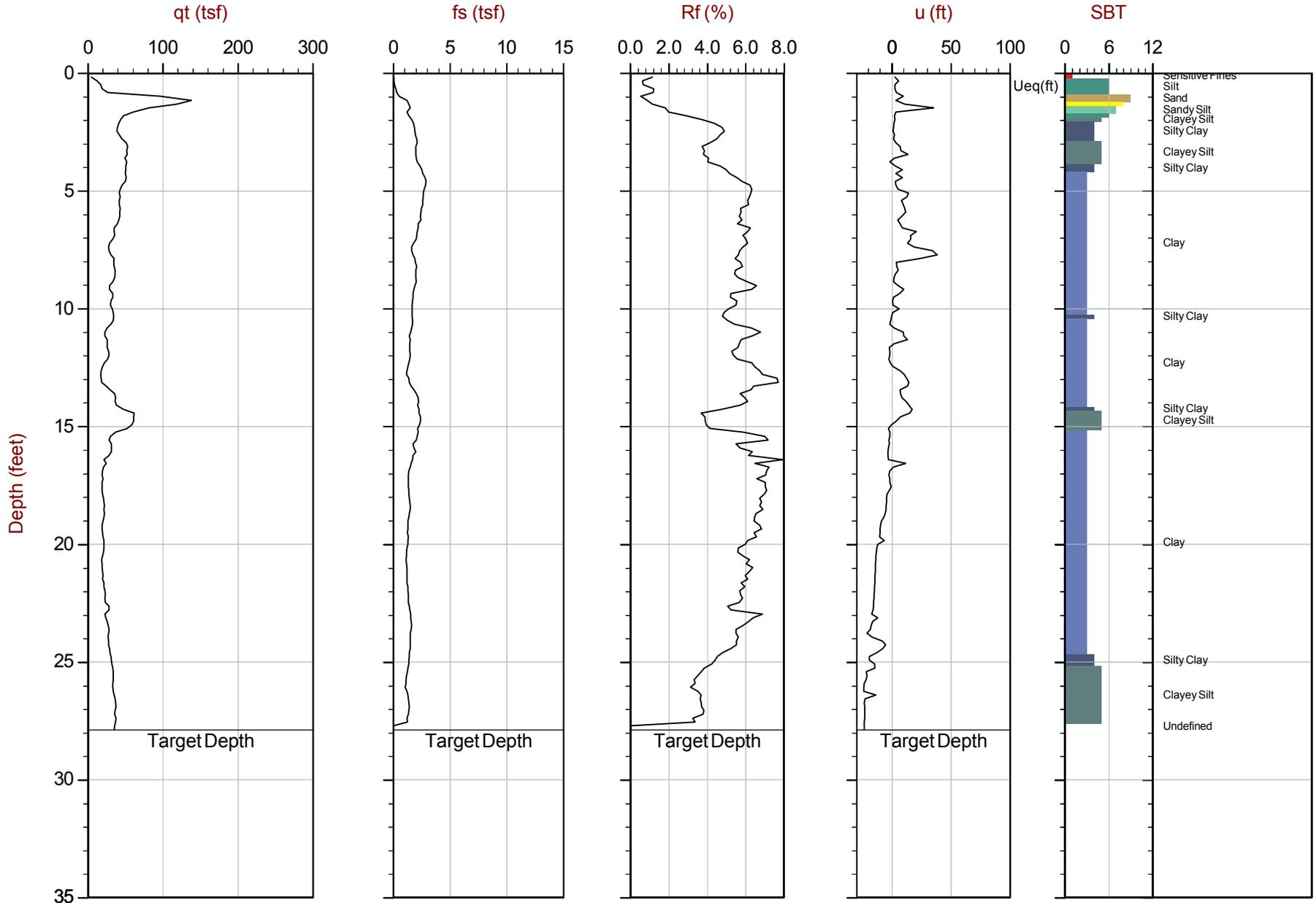


Max Depth: 8.500 m / 27.89 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB2\_B2.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874736 E: 1777468 Elev: 872.5

△ Dissipation with estimated Ueq value      △ Dissipation, equilibrium not achieved  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Max Depth: 8.500 m / 27.89 ft  
 Depth Inc: 0.050 m / 0.164 ft  
 Avg Int: Every Point

File: 16-54112\_CPSTR3\_EB2\_B3.COR  
 Unit Wt: SBT (R&C1986)

SBT: Robertson and Campanella, 1986  
 Coords: N: 874716 E: 1777445 Elev: 872.2

△ Dissipation with estimated Ueq value  
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

△ Dissipation, equilibrium not achieved

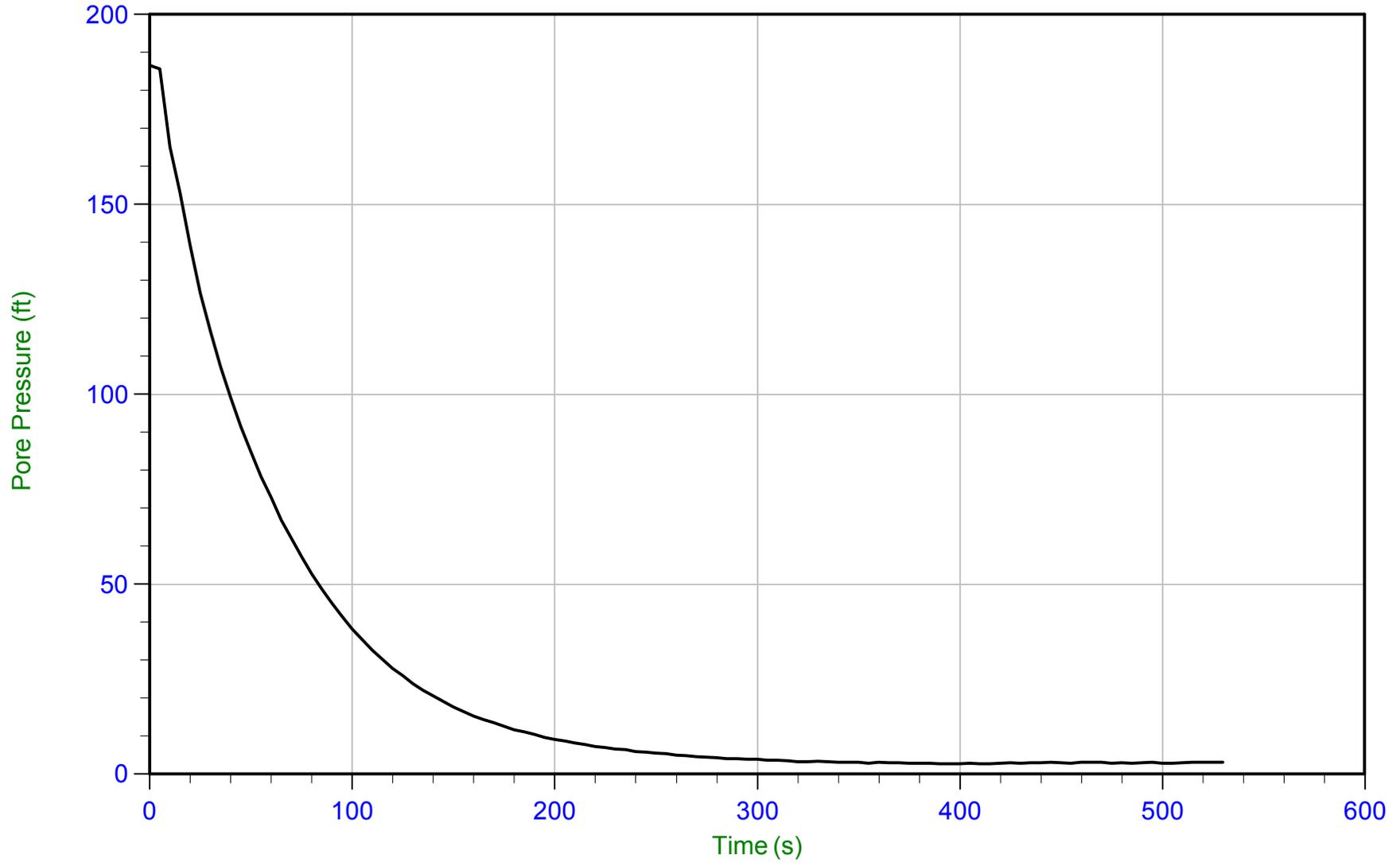
Pore Pressure Dissipation Summary and  
Pore Pressure Dissipation Plots



Job No: 16-54112  
Client: Kleinfelder  
Project: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85  
BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Start Date: 19-Dec-2016  
End Date: 21-Dec-2016

**CPT<sub>u</sub> PORE PRESSURE DISSIPATION SUMMARY**

| Sounding ID | File Name                   | Cone Area (cm <sup>2</sup> ) | Duration (s) | Test Depth (ft) | Estimated Equilibrium Pore Pressure U <sub>eq</sub> (ft) | Calculated Phreatic Surface (ft) |
|-------------|-----------------------------|------------------------------|--------------|-----------------|--|----------------------------------|
| STR2_EB2_B2 | 16-54112_CP STR2_EB2_B2.PPD | 15.0                         | 530          | 24.6            | 3.0  | 21.6                             |
| STR2_EB2_B3 | 16-54112_CP STR2_EB2_B3.PPD | 15.0                         | 865          | 29.9            |  |                                  |
| Totals      |                             |                              | 14.4 min     |                 |  |                                  |



Trace Summary:   
Filename: 16-54112\_CP\_STR2\_EB2\_B2.PPT Min: 2.7 ft WT: 6.591 m / 21.624 ft   
Depth: 7.500 m / 24.606 ft UMax: 186.5 ft Ueq: 3.0 ft   
Duration: 530.0 s



*Kleinfelder*

Job No: 16-54112

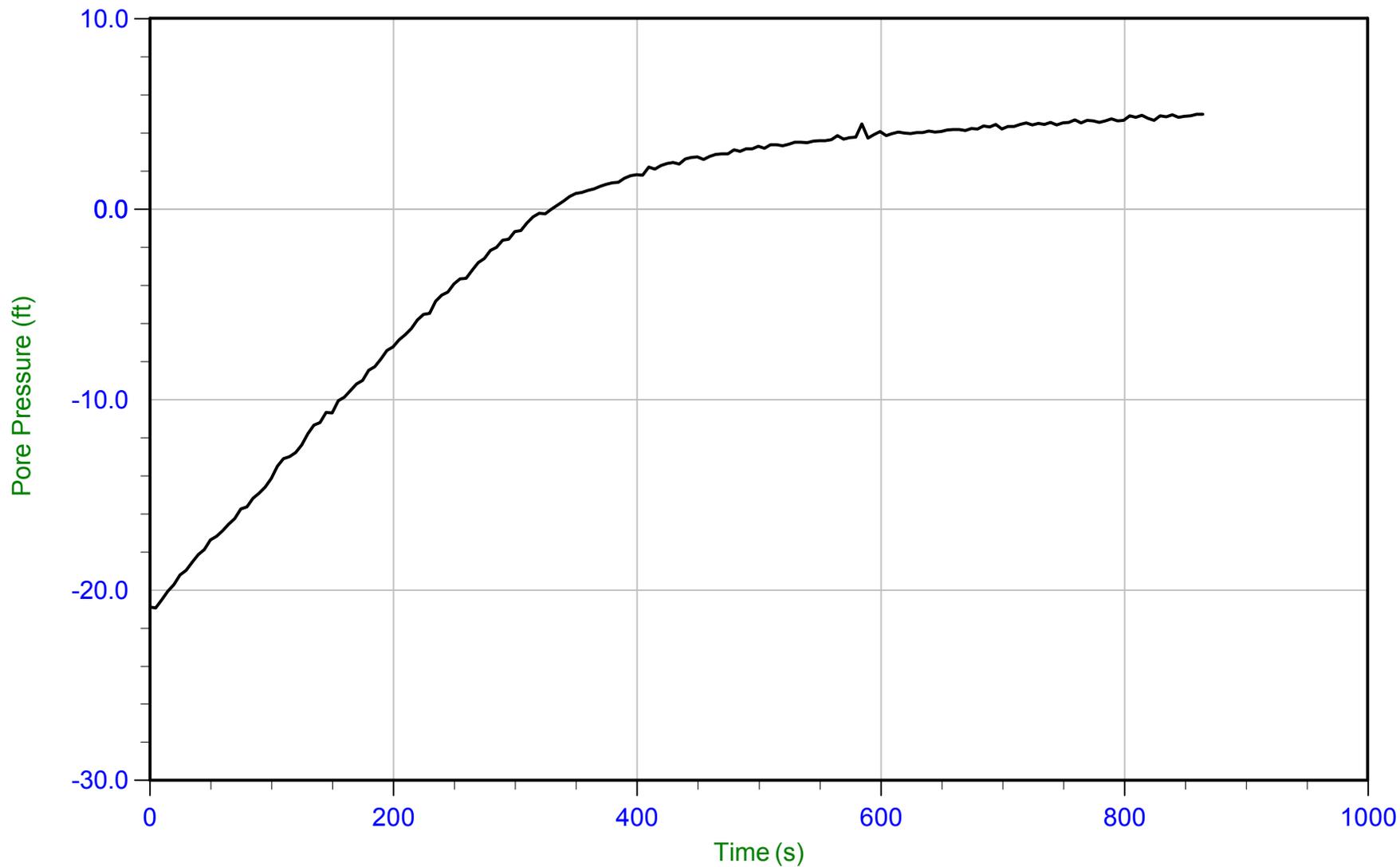
Date: 12/19/2016 09:49

Site: SITE #2 (STRUCTURE #2 AND #3)...

Sounding: STR2\_EB2\_B3

Cone: 367:T1500F15U500

Cone Area: 15 sq cm



Trace Summary: Filename: 16-54112\_CP\_STR2\_EB2\_B3.PPT  
Min: -20.9 ft  
Depth: 9.100 m / 29.855 ft  
U Max: 5.0 ft  
Duration: 865.0 s

## Flat Plate Dilatometer Test Summary, Plots and Tabular Results



Job No: 16-54112  
Client: Kleinfelder  
Project: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Start Date: 19-Dec-2016  
End Date: 21-Dec-2016

### FLAT PLATE DILATOMETER TEST SUMMARY

| Sounding ID | File Name                | Date        | Final Depth (ft) | Assumed Phreatic Surface (ft) | Northing <sup>2</sup> (feet) | Easting (feet) | Refer to Notation Number |
|-------------|--------------------------|-------------|------------------|-------------------------------|------------------------------|----------------|--------------------------|
| STR2_EB1_B1 | 16-54112_DMT STR2_EB1_B1 | 20-Dec-2016 | 33               |                               | 874653                       | 1777563        | 1                        |
| STR2_EB1_B2 | 16-54112_DMT STR2_EB1_B2 | 20-Dec-2016 | 20               |                               | 874584                       | 1777560        | 1                        |
| STR2_EB1_B3 | 16-54112_DMT STR2_EB1_B3 | 20-Dec-2016 | 30               |                               | 874621                       | 1777567        | 1                        |
| STR2_EB2_B1 | 16-54112_DMT STR2_EB2_B1 | 21-Dec-2016 | 25               |                               | 874655                       | 1777453        | 1                        |
| STR2_EB2_B2 | 16-54112_DMT STR2_EB2_B2 | 21-Dec-2016 | 21               |                               | 874591                       | 1777450        | 1                        |
| STR2_EB2_B3 | 16-54112_DMT STR2_EB2_B3 | 21-Dec-2016 | 28               |                               | 874627                       | 1777441        | 1                        |
| STR3_EB1_B1 | 16-54112_DMT STR3_EB1_B1 | 20-Dec-2016 | 32               |                               | 874663                       | 1777566        | 1                        |
| STR3_EB1_B2 | 16-54112_DMT STR3_EB1_B2 | 20-Dec-2016 | 32               |                               | 874724                       | 1777577        | 1                        |
| STR3_EB1_B3 | 16-54112_DMT STR3_EB1_B3 | 20-Dec-2016 | 32               |                               | 874701                       | 1777579        | 1                        |
| STR3_EB2_B1 | 16-54112_DMT STR3_EB2_B1 | 21-Dec-2016 | 28               |                               | 874672                       | 1777462        | 1                        |
| STR3_EB2_B2 | 16-54112_DMT STR3_EB2_B2 | 20-Dec-2016 | 28               |                               | 874736                       | 1777468        | 1                        |
| STR3_EB2_B3 | 16-54112_DMT STR3_EB2_B3 | 21-Dec-2016 | 27               |                               | 874716                       | 1777445        | 1                        |

1. Phreatic surface is assumed not to be encountered within exploration depth.
2. State Plane System 3200 - North Carolina. Coordinates were provided by client.



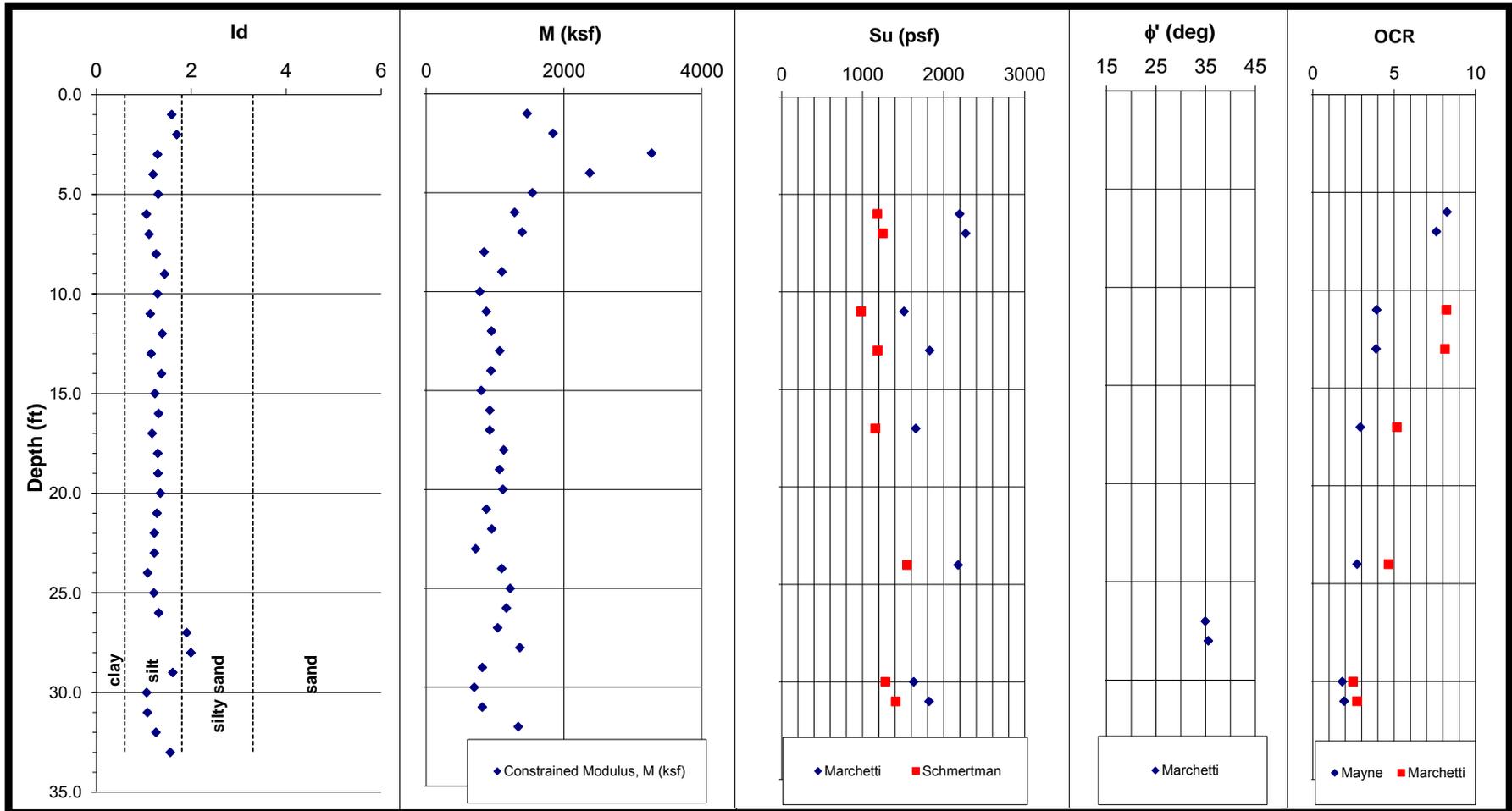
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





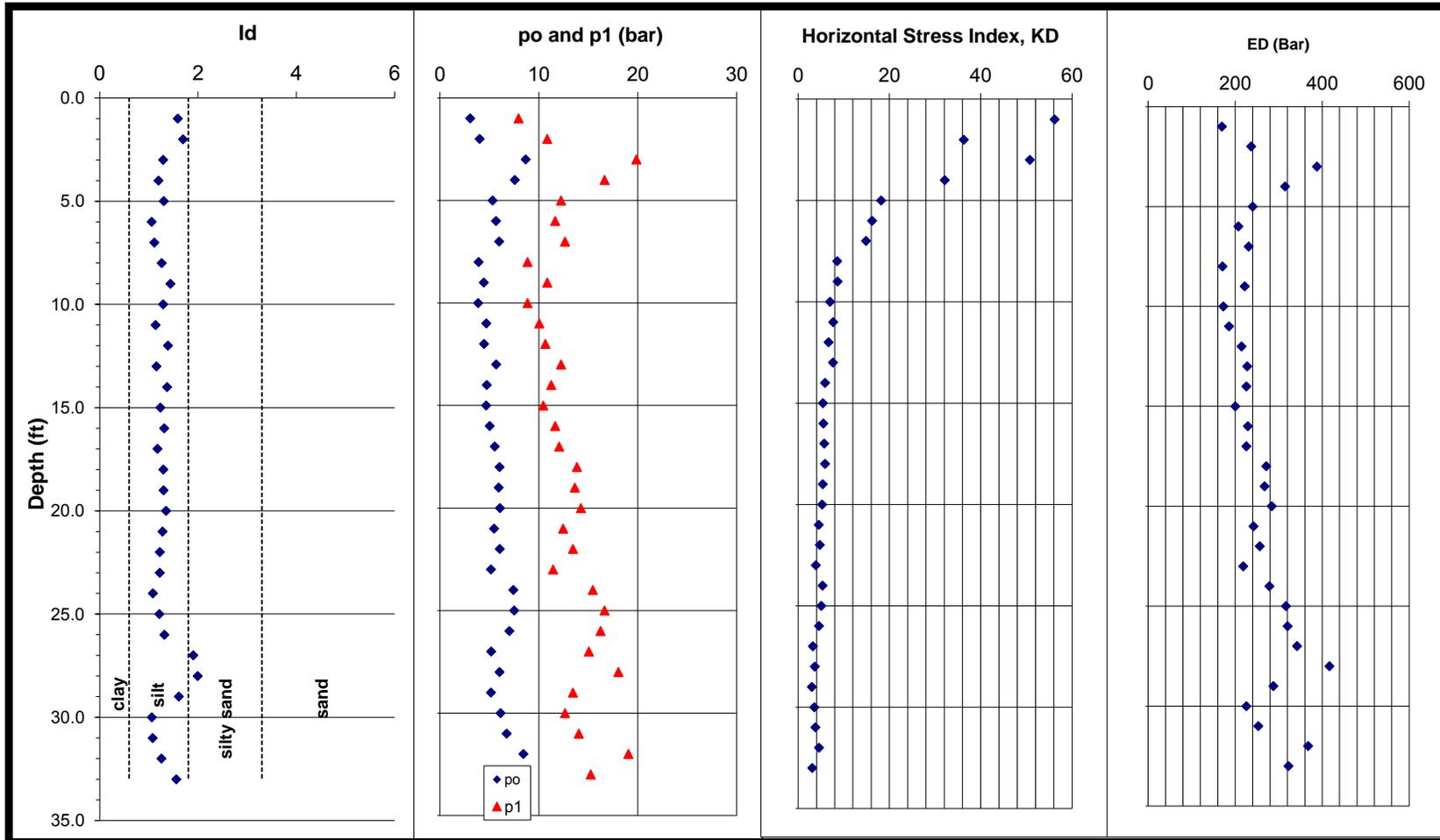
# DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 AND  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR2\_EB1\_B1  
 Ground Water Depth (ft): N/A

|              | Membrane 1 | Membrane 2 | Membrane 3 |
|--------------|------------|------------|------------|
| $\Delta A =$ | 0.2        | 0          | 0          |
| $\Delta B =$ | 0.35       | 0          | 0          |
| Zm=          | 0          | bar        |            |

Northing 874653  
 Easting 1777563

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



### DILATOMETER TEST RESULTS

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | po<br>(bar) | p1<br>(bar) | p2<br>(bar) | uo<br>(psf) | $\gamma_1^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | Id   | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>2</sup> | OCR <sup>3</sup> | $\phi^3$<br>(deg) | R <sub>u</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |      |
|----------------------------|------------|------------|------------|-------------|-------------|-------------|-------------|-----------------------|------------------------|-------------------------|------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|------|
| 1.0                        | 3.1        | 8.3        |            | 3.1         | 7.95        |             | 0           | 114                   | 114                    | 114                     | 1.59 | 56.2           | 169                     |                |                  |                  |                   | 4.13           | 354                     |                                      |                                      | 1463       |      |
| 2.0                        | 4.15       | 11.2       |            | 4.0         | 10.85       |             | 0           | 117                   | 231                    | 231                     | 1.70 | 36.3           | 237                     |                |                  |                  |                   | 3.72           | 495                     |                                      |                                      | 1841       |      |
| 3.0                        | 9          | 20.2       | 0          | 8.7         | 19.85       |             | 0           | 125                   | 356                    | 356                     | 1.29 | 50.8           | 388                     |                |                  |                  |                   | 4.04           | 810                     |                                      |                                      | 3273       |      |
| 4.0                        | 7.8        | 17         |            | 7.6         | 16.65       |             | 0           | 123                   | 492                    | 492                     | 1.20 | 32.1           | 315                     |                |                  |                  |                   | 3.61           | 658                     |                                      |                                      | 2373       |      |
| 5.0                        | 5.45       | 12.6       |            | 5.3         | 12.25       |             | 0           | 119                   | 611                    | 611                     | 1.30 | 18.2           | 240                     |                |                  |                  |                   | 3.07           | 502                     |                                      |                                      | 1540       |      |
| 6.0                        | 5.75       | 12         | 0          | 5.7         | 11.65       |             | 0           | 119                   | 730                    | 730                     | 1.06 | 16.2           | 208                     | 2.5            | 8.3              | 26.2             |                   | 2.96           | 434                     | 2196                                 | 1183                                 | 1283       |      |
| 7.0                        | 6.1        | 13         |            | 6.0         | 12.65       |             | 0           | 120                   | 838                    | 838                     | 1.11 | 14.9           | 231                     | 2.3            | 7.6              | 23.0             |                   | 2.88           | 483                     | 2271                                 | 1249                                 | 1391       |      |
| 8.0                        | 3.95       | 9.2        |            | 3.9         | 8.85        |             | 0           | 115                   | 953                    | 953                     | 1.26 | 8.6            | 171                     |                |                  |                  |                   | 2.35           | 358                     |                                      |                                      | 840        |      |
| 9.0                        | 4.55       | 11.2       | 0          | 4.4         | 10.85       |             | 0           | 118                   | 1071                   | 1071                    | 1.44 | 8.7            | 222                     |                |                  |                  |                   | 2.36           | 464                     |                                      |                                      | 1096       |      |
| 10.0                       | 3.9        | 9.2        |            | 3.9         | 8.85        |             | 0           | 115                   | 1154                   | 1154                    | 1.29 | 7.0            | 173                     |                |                  |                  |                   | 2.15           | 361                     |                                      |                                      | 777        |      |
| 11.0                       | 4.75       | 10.4       |            | 4.7         | 10.05       |             | 0           | 117                   | 1271                   | 1271                    | 1.14 | 7.7            | 186                     | 1.6            | 3.9              | 8.2              |                   | 2.24           | 388                     | 1512                                 | 981                                  | 871        |      |
| 12.0                       | 4.55       | 11         | 0          | 4.5         | 10.65       |             | 0           | 117                   | 1388                   | 1388                    | 1.39 | 6.7            | 215                     |                |                  |                  |                   | 2.11           | 449                     |                                      |                                      | 948        |      |
| 13.0                       | 5.8        | 12.6       |            | 5.7         | 12.25       |             | 0           | 119                   | 1550                   | 1550                    | 1.15 | 7.7            | 228                     | 1.6            | 3.9              | 8.1              |                   | 2.24           | 476                     | 1828                                 | 1188                                 | 1064       |      |
| 14.0                       | 4.85       | 11.6       |            | 4.7         | 11.25       |             | 0           | 118                   | 1668                   | 1668                    | 1.37 | 5.9            | 226                     |                |                  |                  |                   | 1.99           | 472                     |                                      |                                      | 939        |      |
| 15.0                       | 4.75       | 10.8       | 0          | 4.7         | 10.45       |             | 0           | 117                   | 1786                   | 1786                    | 1.24 | 5.5            | 200                     |                |                  |                  |                   | 1.91           | 419                     |                                      |                                      | 798        |      |
| 16.0                       | 5.15       | 12         |            | 5.0         | 11.65       |             | 0           | 119                   | 1897                   | 1897                    | 1.31 | 5.5            | 230                     |                |                  |                  |                   | 1.92           | 479                     |                                      |                                      | 922        |      |
| 17.0                       | 5.65       | 12.4       |            | 5.5         | 12.05       |             | 0           | 119                   | 2016                   | 2016                    | 1.18 | 5.7            | 226                     | 1.3            | 2.9              | 5.2              |                   | 1.95           | 472                     | 1656                                 | 1157                                 | 921        |      |
| 18.0                       | 6.2        | 14.2       | 0          | 6.0         | 13.85       |             | 0           | 121                   | 2137                   | 2137                    | 1.30 | 5.9            | 271                     |                |                  |                  |                   | 1.98           | 567                     |                                      |                                      | 1123       |      |
| 19.0                       | 6.1        | 14         |            | 5.9         | 13.65       |             | 0           | 120                   | 2289                   | 2289                    | 1.30 | 5.4            | 268                     |                |                  |                  |                   | 1.90           | 559                     |                                      |                                      | 1062       |      |
| 20.0                       | 6.25       | 14.6       |            | 6.1         | 14.25       |             | 0           | 121                   | 2410                   | 2410                    | 1.35 | 5.3            | 284                     |                |                  |                  |                   | 1.87           | 594                     |                                      |                                      | 1111       |      |
| 21.0                       | 5.6        | 12.8       | 0          | 5.5         | 12.45       |             | 0           | 119                   | 2529                   | 2529                    | 1.28 | 4.5            | 242                     |                |                  |                  |                   | 1.72           | 506                     |                                      |                                      | 870        |      |
| 22.0                       | 6.2        | 13.8       |            | 6.0         | 13.45       |             | 0           | 120                   | 2648                   | 2648                    | 1.22 | 4.8            | 257                     |                |                  |                  |                   | 1.77           | 536                     |                                      |                                      | 950        |      |
| 23.0                       | 5.25       | 11.8       |            | 5.2         | 11.45       |             | 0           | 118                   | 2766                   | 2766                    | 1.22 | 3.9            | 219                     |                |                  |                  |                   | 1.57           | 457                     |                                      |                                      | 717        |      |
| 24.0                       | 7.6        | 15.8       | 0.1        | 7.4         | 15.45       | 0.30        | 0           | 122                   | 2888                   | 2888                    | 1.08 | 5.4            | 279                     | 1.2            | 2.7              | 4.7              |                   | 1.88           | 582                     | 2181                                 | 1549                                 | 1095       |      |
| 25.0                       | 7.75       | 17         |            | 7.5         | 16.65       |             | 0           | 123                   | 3074                   | 3074                    | 1.22 | 5.1            | 317                     |                |                  |                  |                   | 1.84           | 662                     |                                      |                                      | 1217       |      |
| 26.0                       | 7.25       | 16.6       |            | 7.0         | 16.25       |             | 0           | 123                   | 3196                   | 3196                    | 1.32 | 4.6            | 321                     |                |                  |                  |                   | 1.74           | 670                     |                                      |                                      | 1163       |      |
| 27.0                       | 5.45       | 15.4       | 0.05       | 5.2         | 15.05       | 0.25        | 0           | 121                   | 3317                   | 3317                    | 1.91 | 3.3            | 342                     |                |                  |                  |                   |                |                         |                                      |                                      | 1035       |      |
| 28.0                       | 6.4        | 18.4       |            | 6.0         | 18.05       |             | 0           | 123                   | 3452                   | 3452                    | 1.99 | 3.6            | 417                     |                |                  |                  |                   | 34.9           | 1.45                    | 715                                  |                                      |            | 1357 |
| 29.0                       | 5.35       | 13.8       |            | 5.2         | 13.45       |             | 0           | 120                   | 3572                   | 3572                    | 1.61 | 3.0            | 288                     |                |                  |                  |                   | 35.5           | 1.56                    | 871                                  |                                      |            | 1357 |
| 30.0                       | 6.25       | 13         | 1.25       | 6.1         | 12.65       | 1.45        | 0           | 120                   | 3590                   | 3590                    | 1.06 | 3.6            | 226                     | 0.9            | 1.8              | 2.5              |                   | 1.35           | 601                     |                                      |                                      | 811        |      |
| 31.0                       | 6.9        | 14.4       |            | 6.8         | 14.05       |             | 0           | 121                   | 3711                   | 3711                    | 1.08 | 3.8            | 253                     | 0.9            | 1.9              | 2.7              |                   | 1.48           | 472                     | 1631                                 | 1282                                 | 696        |      |
| 32.0                       | 8.75       | 19.4       |            | 8.4         | 19.05       |             | 0           | 125                   | 3835                   | 3835                    | 1.26 | 4.6            | 368                     |                |                  |                  |                   | 1.54           | 529                     | 1821                                 | 1410                                 | 814        |      |
| 33.0                       | 6.2        | 15.6       | 0          | 6.0         | 15.25       |             | 0           | 122                   | 4014                   | 4014                    | 1.26 | 4.6            | 368                     |                |                  |                  |                   | 1.74           | 769                     |                                      |                                      | 1335       |      |
| 33.0                       | 6.2        | 15.6       | 0          | 6.0         | 15.25       |             | 0           | 122                   | 4014                   | 4014                    | 1.56 | 3.1            | 322                     |                |                  |                  |                   | 1.74           | 769                     |                                      |                                      | 1335       |      |
| 33.0                       | 6.2        | 15.6       | 0          | 6.0         | 15.25       |             | 0           | 122                   | 4014                   | 4014                    | 1.56 | 3.1            | 322                     |                |                  |                  |                   | 1.37           | 673                     |                                      |                                      | 925        |      |



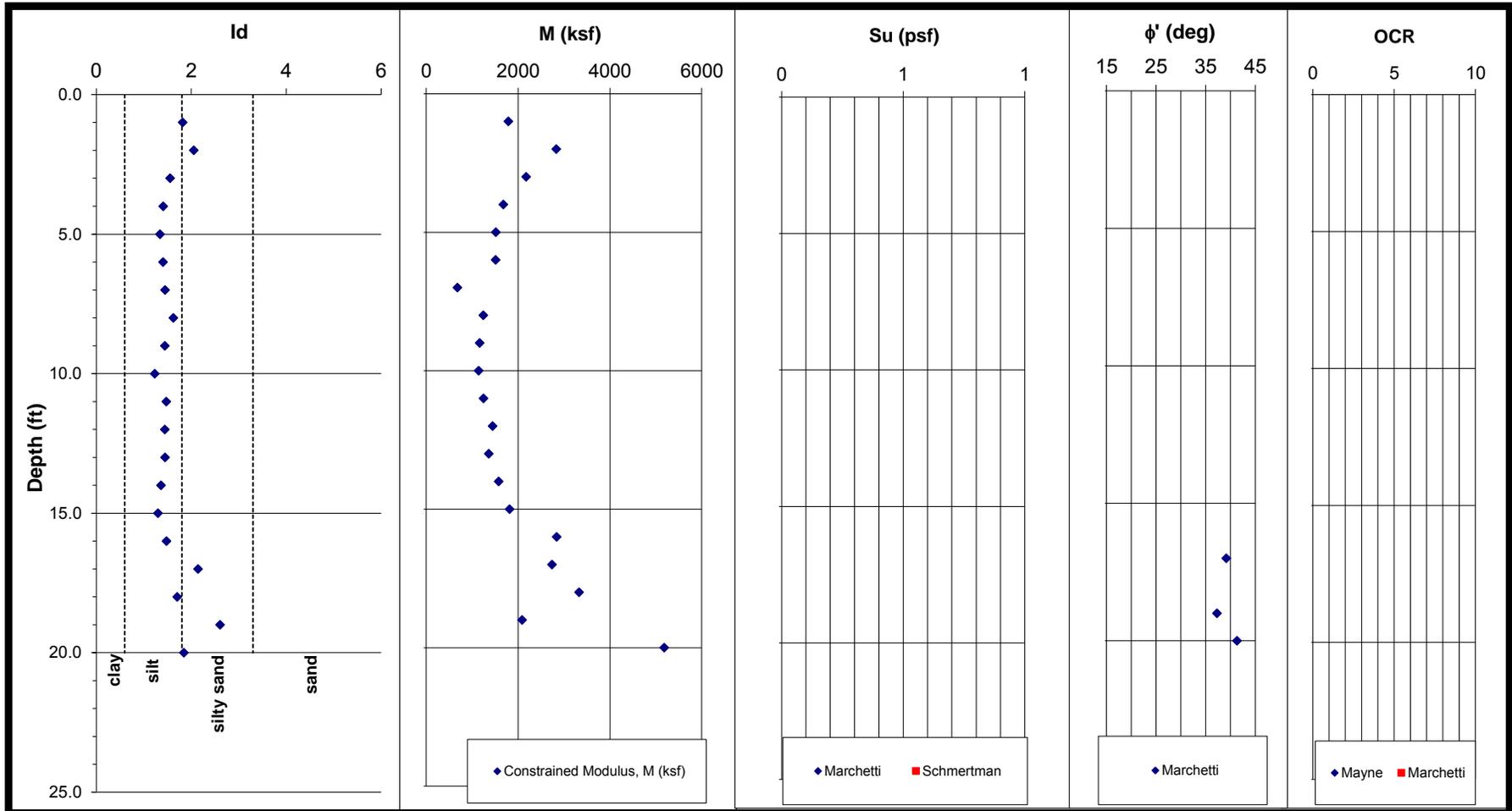
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





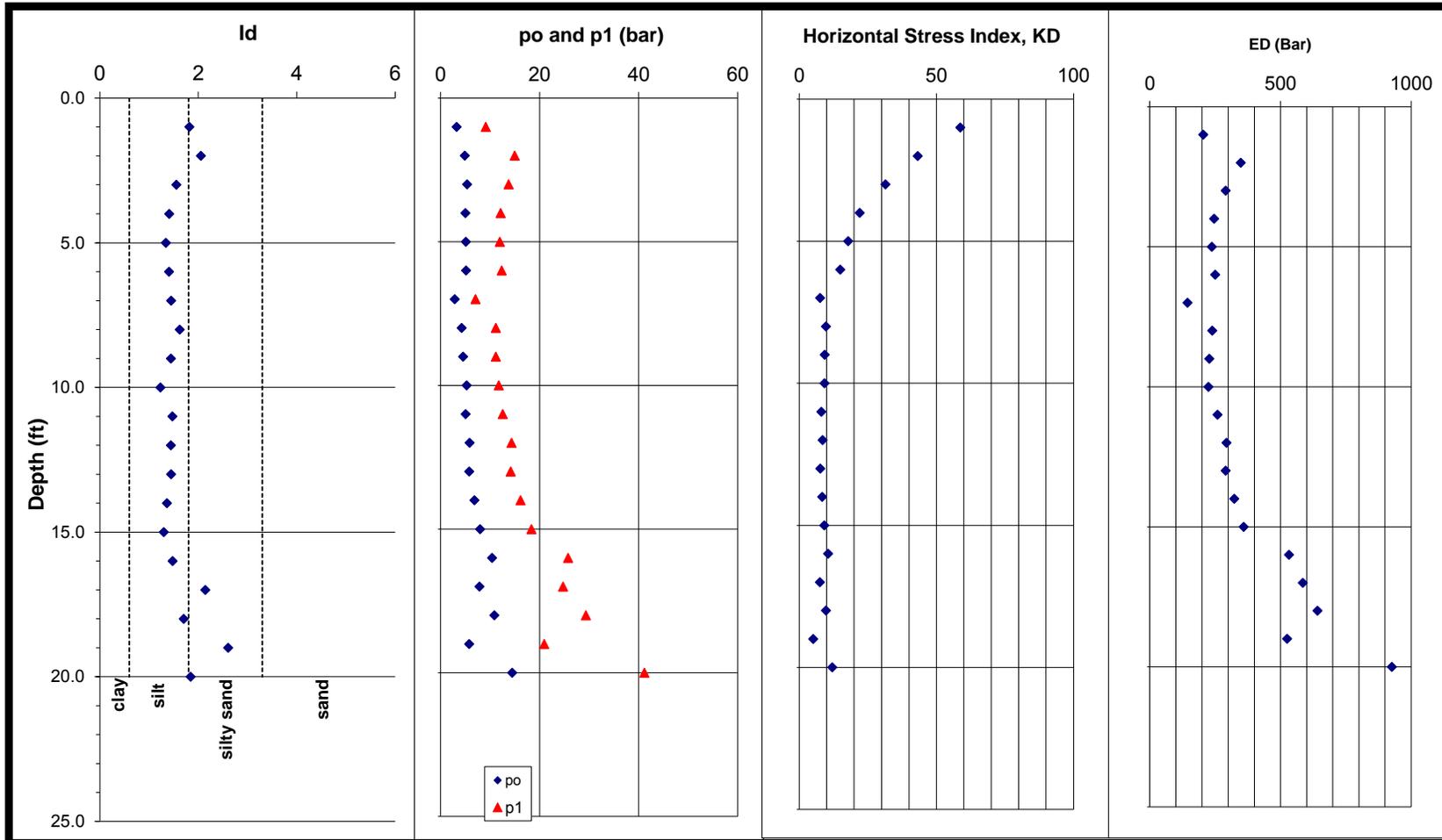
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR2\_EB1\_B2  
 Ground Water Depth (ft): N/A

|              | Membrane 1 | Membrane 2 | Membrane 3 |
|--------------|------------|------------|------------|
| $\Delta A =$ | 0.125      | 0          | 0          |
| $\Delta B =$ | 0.65       | 0          | 0          |
| Zm=          | 0          | bar        |            |

Northing 874584  
 Easting 1777560

- <sup>1</sup> Depth Below Existing Ground Surface
- <sup>2</sup> Mayne, 1995
- <sup>3</sup> Marchetti, 2001
- <sup>4</sup> Schmertman, 1991
- <sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_T^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>r</sup> | $\phi^{i3}$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |      |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|----------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|------|
| 1.0                        | 3.4        | 9.8        |            | 3.2                     | 9.15                    |                         | 0                       | 115                   | 115                    | 115                     | 1.82           | 58.7           | 205                     |                |                  |                  | 47.3                 | 4.18           | 428                     |                                      |                                      | 1788       |      |
| 2.0                        | 5.25       | 15.6       |            | 4.9                     | 14.95                   |                         | 0                       | 121                   | 236                    | 236                     | 2.05           | 43.3           | 349                     |                |                  |                  | 46.3                 | 3.89           | 729                     |                                      |                                      | 2832       |      |
| 3.0                        | 5.65       | 14.4       | 0          | 5.4                     | 13.75                   |                         | 0                       | 120                   | 357                    | 357                     | 1.56           | 31.5           | 291                     |                |                  |                  |                      | 3.59           | 607                     |                                      |                                      | 2176       |      |
| 4.0                        | 5.25       | 12.8       |            | 5.0                     | 12.15                   |                         | 0                       | 119                   | 476                    | 476                     | 1.41           | 22.1           | 247                     |                |                  |                  |                      | 3.25           | 516                     |                                      |                                      | 1676       |      |
| 5.0                        | 5.3        | 12.6       |            | 5.1                     | 11.95                   |                         | 0                       | 119                   | 595                    | 595                     | 1.34           | 17.9           | 238                     |                |                  |                  |                      | 3.05           | 497                     |                                      |                                      | 1515       |      |
| 6.0                        | 5.35       | 13         | 0          | 5.1                     | 12.35                   |                         | 0                       | 119                   | 714                    | 714                     | 1.41           | 15.0           | 250                     |                |                  |                  |                      | 2.88           | 523                     |                                      |                                      | 1509       |      |
| 7.0                        | 2.95       | 7.7        |            | 2.9                     | 7.05                    |                         | 0                       | 113                   | 789                    | 789                     | 1.45           | 7.6            | 145                     |                |                  |                  |                      | 2.24           | 302                     |                                      |                                      | 676        |      |
| 8.0                        | 4.45       | 11.8       |            | 4.2                     | 11.15                   |                         | 0                       | 118                   | 907                    | 907                     | 1.63           | 9.8            | 240                     |                |                  |                  |                      | 2.48           | 500                     |                                      |                                      | 1240       |      |
| 9.0                        | 4.75       | 11.8       | 0          | 4.6                     | 11.15                   |                         | 0                       | 118                   | 1025                   | 1025                    | 1.44           | 9.3            | 229                     |                |                  |                  |                      | 2.43           | 478                     |                                      |                                      | 1160       |      |
| 10.0                       | 5.45       | 12.4       |            | 5.3                     | 11.75                   |                         | 0                       | 119                   | 1187                   | 1187                    | 1.23           | 9.3            | 225                     |                |                  |                  |                      | 2.42           | 470                     |                                      |                                      | 1139       |      |
| 11.0                       | 5.3        | 13.2       |            | 5.1                     | 12.55                   |                         | 0                       | 119                   | 1307                   | 1307                    | 1.48           | 8.1            | 260                     |                |                  |                  |                      | 2.30           | 542                     |                                      |                                      | 1245       |      |
| 12.0                       | 6.15       | 15         | 0          | 5.9                     | 14.35                   |                         | 0                       | 121                   | 1428                   | 1428                    | 1.44           | 8.6            | 294                     |                |                  |                  |                      | 2.35           | 614                     |                                      |                                      | 1446       |      |
| 13.0                       | 6.05       | 14.8       |            | 5.8                     | 14.15                   |                         | 0                       | 121                   | 1571                   | 1571                    | 1.45           | 7.7            | 291                     |                |                  |                  |                      | 2.24           | 607                     |                                      |                                      | 1362       |      |
| 14.0                       | 7.15       | 16.8       |            | 6.8                     | 16.15                   |                         | 0                       | 122                   | 1693                   | 1693                    | 1.36           | 8.4            | 323                     |                |                  |                  |                      | 2.33           | 675                     |                                      |                                      | 1576       |      |
| 15.0                       | 8.35       | 19         | 0          | 8.0                     | 18.35                   |                         | 0                       | 124                   | 1817                   | 1817                    | 1.30           | 9.2            | 360                     |                |                  |                  |                      | 2.42           | 751                     |                                      |                                      | 1815       |      |
| 16.0                       | 11         | 26.4       |            | 10.4                    | 25.75                   |                         | 0                       | 128                   | 2052                   | 2052                    | 1.48           | 10.6           | 533                     |                |                  |                  |                      | 2.55           | 1113                    |                                      |                                      | 2842       |      |
| 17.0                       | 8.55       | 25.4       |            | 7.9                     | 24.75                   |                         | 0                       | 127                   | 2179                   | 2179                    | 2.14           | 7.5            | 586                     |                |                  |                  | 39.2                 | 2.24           | 1223                    |                                      |                                      | 2740       |      |
| 18.0                       | 11.6       | 30         | 0          | 10.8                    | 29.35                   |                         | 0                       | 130                   | 2309                   | 2309                    | 1.71           | 9.8            | 642                     |                |                  |                  |                      | 2.48           | 1341                    |                                      |                                      | 3328       |      |
| 19.0                       | 6.4        | 21.6       |            | 5.8                     | 20.95                   |                         | 0                       | 124                   | 2365                   | 2365                    | 2.61           | 5.1            | 526                     |                |                  |                  |                      | 37.3           | 1.90                    | 1098                                 |                                      |            | 2088 |
| 20.0                       | 15.6       | 41.8       |            | 14.5                    | 41.15                   |                         | 0                       | 134                   | 2499                   | 2499                    | 1.85           | 12.1           | 926                     |                |                  |                  |                      | 41.3           | 2.68                    | 1935                                 |                                      |            | 5183 |



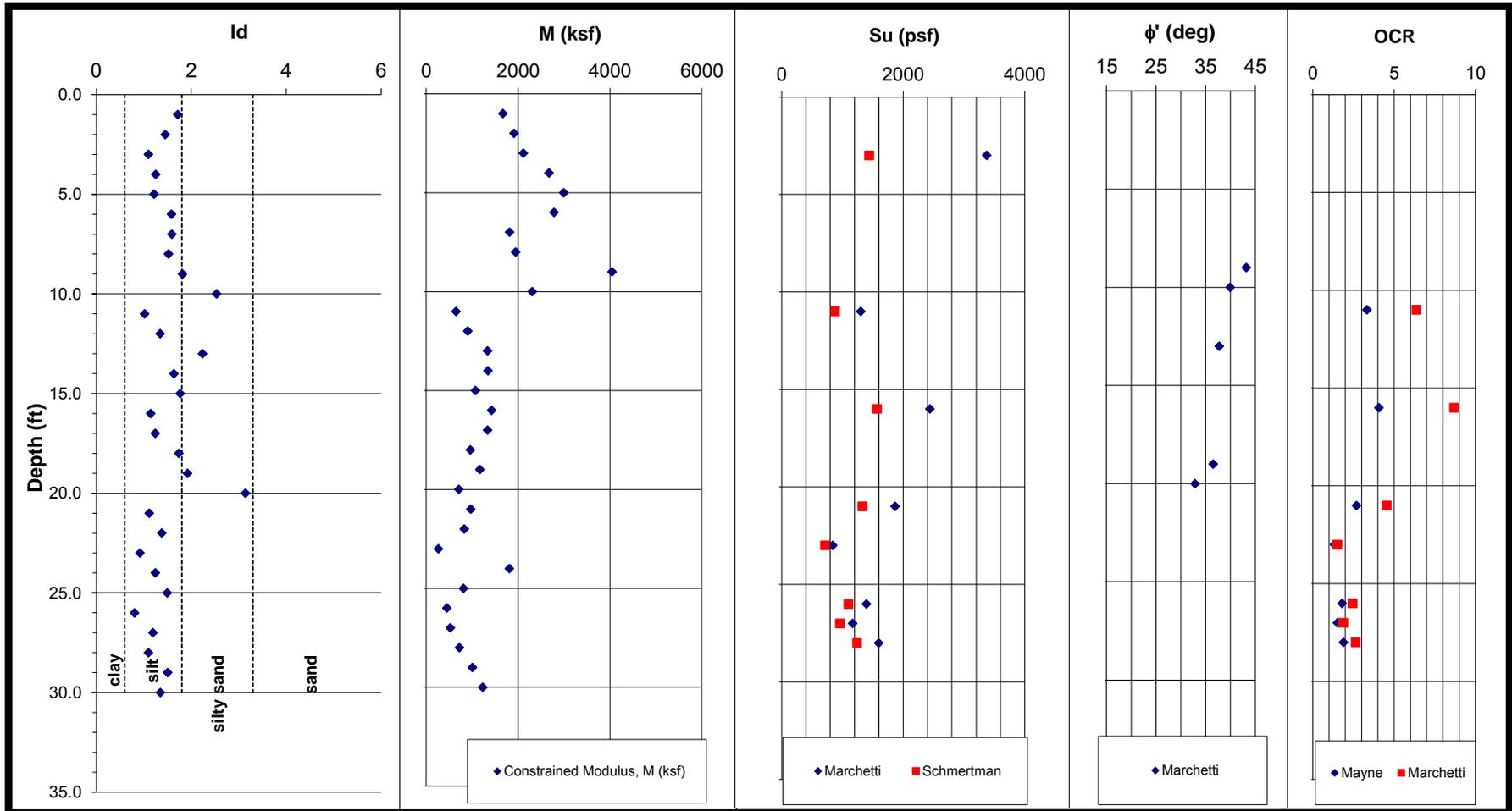
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

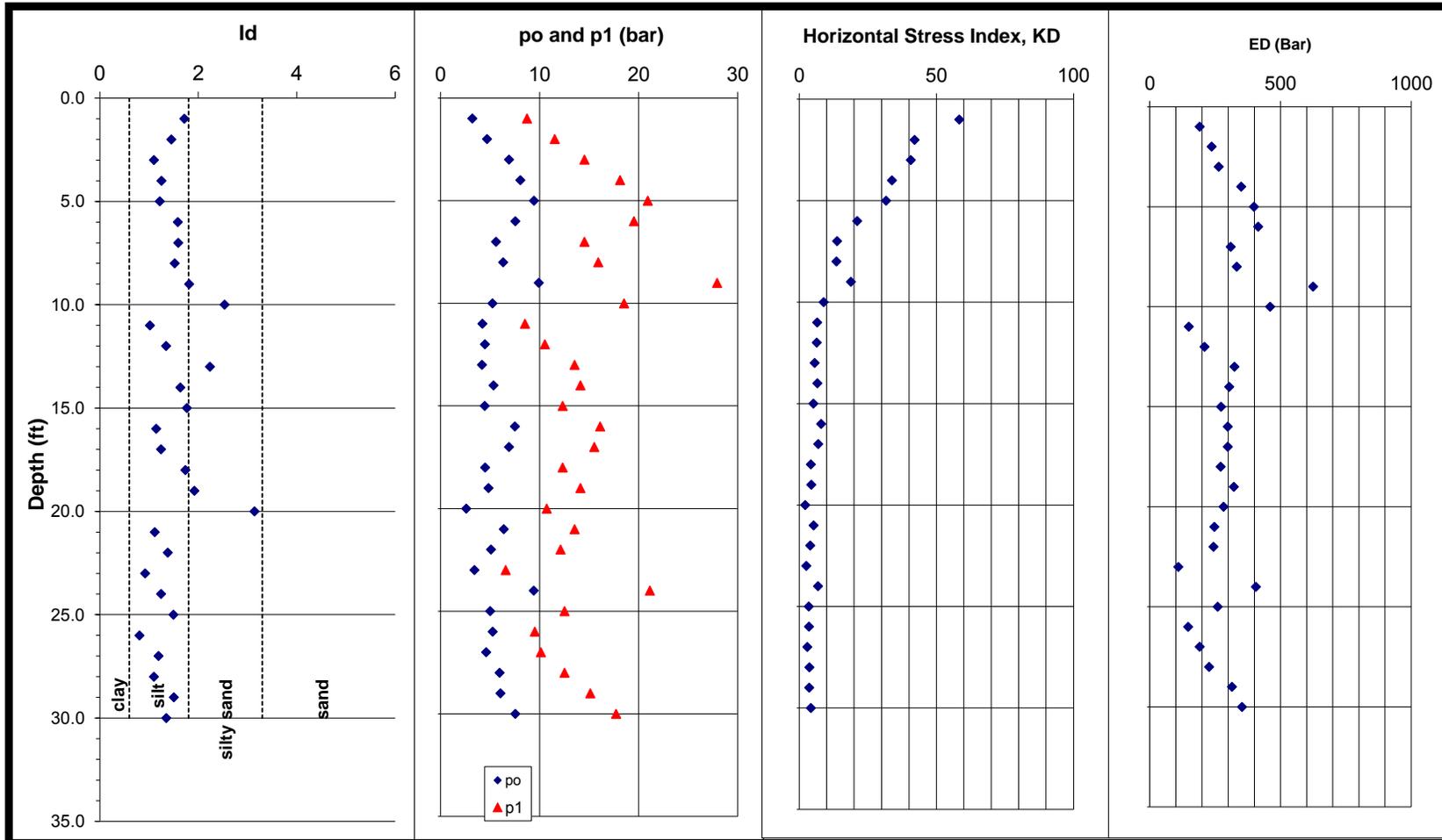
Project No.: 16-54112





### DILATOMETER TEST RESULTS

Test ID: STR2\_EB1\_B3  
Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Location: Greensboro, NC  
Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 AND  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR2\_EB1\_B3  
 Ground Water Depth (ft): N/A

Membrane 1    Membrane 2    Membrane 3  
 $\Delta A =$  0.175            0            0  
 $\Delta B =$  0.475            0            0  
 Zm= 0            bar

Latitude: 36.15071  
 Longitude: -79.75336

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_T^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>s</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 3.3        | 9.2        |            | 3.2                     | 8.725                   |                         | 0                       | 115                   | 115                    | 115                     | 1.72           | 58.4           | 191                     |                |                  |                  |                   | 4.17           | 400                     |                                      |                                      | 1666       |
| 2.0                        | 4.85       | 12         |            | 4.7                     | 11.525                  |                         | 0                       | 118                   | 233                    | 233                     | 1.45           | 42.1           | 237                     |                |                  |                  |                   | 3.86           | 495                     |                                      |                                      | 1910       |
| 3.0                        | 7.1        | 15         | 0          | 6.9                     | 14.525                  |                         | 0                       | 121                   | 355                    | 355                     | 1.10           | 40.7           | 264                     | 4.1            | 20.7             | 110.1            |                   | 3.83           | 552                     | 3373                                 | 1444                                 | 2113       |
| 4.0                        | 8.35       | 18.6       |            | 8.0                     | 18.125                  |                         | 0                       | 124                   | 496                    | 496                     | 1.25           | 33.9           | 350                     |                |                  |                  |                   | 3.66           | 731                     |                                      |                                      | 2670       |
| 5.0                        | 9.8        | 21.4       |            | 9.4                     | 20.925                  |                         | 0                       | 126                   | 622                    | 622                     | 1.22           | 31.7           | 399                     |                |                  |                  |                   | 3.59           | 833                     |                                      |                                      | 2993       |
| 6.0                        | 7.95       | 20         | 0.6        | 7.6                     | 19.525                  | 0.78                    | 0                       | 125                   | 746                    | 746                     | 1.58           | 21.1           | 415                     |                |                  |                  |                   | 3.21           | 867                     |                                      |                                      | 2784       |
| 7.0                        | 5.85       | 15         |            | 5.6                     | 14.525                  |                         | 0                       | 121                   | 847                    | 847                     | 1.59           | 13.8           | 310                     |                |                  |                  |                   | 2.81           | 647                     |                                      |                                      | 1815       |
| 8.0                        | 6.6        | 16.4       |            | 6.3                     | 15.925                  |                         | 0                       | 122                   | 969                    | 969                     | 1.52           | 13.6           | 333                     |                |                  |                  |                   | 2.79           | 696                     |                                      |                                      | 1944       |
| 9.0                        | 10.6       | 28.4       | 1.1        | 9.9                     | 27.925                  | 1.28                    | 0                       | 129                   | 1098                   | 1098                    | 1.82           | 18.9           | 625                     |                |                  |                  | 43.2              | 3.10           | 1305                    |                                      |                                      | 4047       |
| 10.0                       | 5.7        | 19         |            | 5.2                     | 18.525                  |                         | 0                       | 123                   | 1230                   | 1230                    | 2.53           | 8.9            | 461                     |                |                  |                  | 40.0              | 2.40           | 963                     |                                      |                                      | 2306       |
| 11.0                       | 4.25       | 9          |            | 4.2                     | 8.525                   |                         | 0                       | 115                   | 1345                   | 1345                    | 1.02           | 6.6            | 149                     | 1.4            | 3.3              | 6.4              |                   | 2.08           | 312                     | 1304                                 | 881                                  | 648        |
| 12.0                       | 4.6        | 11         | 0          | 4.5                     | 10.525                  |                         | 0                       | 117                   | 1463                   | 1463                    | 1.35           | 6.4            | 210                     |                |                  |                  |                   | 2.07           | 438                     |                                      |                                      | 904        |
| 13.0                       | 4.45       | 14         |            | 4.2                     | 13.525                  |                         | 0                       | 120                   | 1554                   | 1554                    | 2.24           | 5.6            | 324                     |                |                  |                  | 37.8              | 1.97           | 677                     |                                      |                                      | 1335       |
| 14.0                       | 5.6        | 14.6       |            | 5.4                     | 14.125                  |                         | 0                       | 121                   | 1674                   | 1674                    | 1.64           | 6.7            | 304                     |                |                  |                  |                   | 2.11           | 635                     |                                      |                                      | 1343       |
| 15.0                       | 4.65       | 12.8       | 0          | 4.5                     | 12.325                  |                         | 0                       | 119                   | 1793                   | 1793                    | 1.77           | 5.2            | 273                     |                |                  |                  |                   | 1.88           | 571                     |                                      |                                      | 1071       |
| 16.0                       | 7.75       | 16.6       |            | 7.5                     | 16.125                  |                         | 0                       | 123                   | 1961                   | 1961                    | 1.15           | 8.0            | 299                     | 1.6            | 4.1              | 8.7              |                   | 2.28           | 624                     | 2442                                 | 1570                                 | 1422       |
| 17.0                       | 7.15       | 16         |            | 6.9                     | 15.525                  |                         | 0                       | 122                   | 2083                   | 2083                    | 1.25           | 6.9            | 299                     |                |                  |                  |                   | 2.14           | 624                     |                                      |                                      | 1335       |
| 18.0                       | 4.7        | 12.8       | 0          | 4.5                     | 12.325                  |                         | 0                       | 119                   | 2202                   | 2202                    | 1.74           | 4.3            | 271                     |                |                  |                  |                   | 1.69           | 567                     |                                      |                                      | 959        |
| 19.0                       | 5.1        | 14.6       |            | 4.8                     | 14.125                  |                         | 0                       | 120                   | 2287                   | 2287                    | 1.92           | 4.4            | 322                     |                |                  |                  | 36.5              | 1.73           | 673                     |                                      |                                      | 1167       |
| 20.0                       | 2.8        | 11.2       |            | 2.6                     | 10.725                  |                         | 0                       | 116                   | 2403                   | 2403                    | 3.14           | 2.2            | 282                     |                |                  |                  | 32.9              | 1.20           | 590                     |                                      |                                      | 710        |
| 21.0                       | 6.55       | 14         | 0          | 6.4                     | 13.525                  |                         | 0                       | 120                   | 2523                   | 2523                    | 1.12           | 5.3            | 248                     | 1.2            | 2.7              | 4.6              |                   | 1.87           | 517                     | 1870                                 | 1334                                 | 967        |
| 22.0                       | 5.25       | 12.6       |            | 5.1                     | 12.125                  |                         | 0                       | 119                   | 2618                   | 2618                    | 1.38           | 4.1            | 244                     |                |                  |                  |                   | 1.62           | 510                     |                                      |                                      | 827        |
| 23.0                       | 3.4        | 7.05       |            | 3.4                     | 6.575                   |                         | 0                       | 112                   | 2730                   | 2730                    | 0.92           | 2.6            | 109                     | 0.7            | 1.3              | 1.5              |                   | 1.16           | 228                     | 842                                  | 715                                  | 264        |
| 24.0                       | 9.8        | 21.6       | 0          | 9.4                     | 21.125                  |                         | 0                       | 126                   | 2856                   | 2856                    | 1.24           | 6.9            | 406                     |                |                  |                  |                   | 2.13           | 848                     |                                      |                                      | 1810       |
| 25.0                       | 5.2        | 13         |            | 5.0                     | 12.525                  |                         | 0                       | 119                   | 2983                   | 2983                    | 1.50           | 3.5            | 261                     |                |                  |                  |                   | 1.49           | 544                     |                                      |                                      | 810        |
| 26.0                       | 5.3        | 10         |            | 5.3                     | 9.525                   |                         | 0                       | 116                   | 3099                   | 3099                    | 0.81           | 3.6            | 148                     | 0.9            | 1.8              | 2.5              |                   | 1.45           | 308                     | 1398                                 | 1101                                 | 448        |
| 27.0                       | 4.7        | 10.6       | 0          | 4.6                     | 10.125                  |                         | 0                       | 117                   | 3216                   | 3216                    | 1.20           | 3.0            | 191                     | 0.8            | 1.5              | 1.9              |                   | 1.31           | 400                     | 1172                                 | 963                                  | 524        |
| 28.0                       | 6.1        | 13         |            | 6.0                     | 12.525                  |                         | 0                       | 120                   | 3347                   | 3347                    | 1.10           | 3.7            | 228                     | 0.9            | 1.9              | 2.6              |                   | 1.52           | 476                     | 1600                                 | 1245                                 | 722        |
| 29.0                       | 6.3        | 15.6       |            | 6.0                     | 15.125                  |                         | 0                       | 122                   | 3469                   | 3469                    | 1.50           | 3.6            | 315                     |                |                  |                  |                   | 1.52           | 658                     |                                      |                                      | 1003       |
| 30.0                       | 7.85       | 18.2       | 0          | 7.5                     | 17.725                  |                         | 0                       | 124                   | 3709                   | 3709                    | 1.35           | 4.2            | 353                     |                |                  |                  |                   | 1.66           | 738                     |                                      |                                      | 1228       |



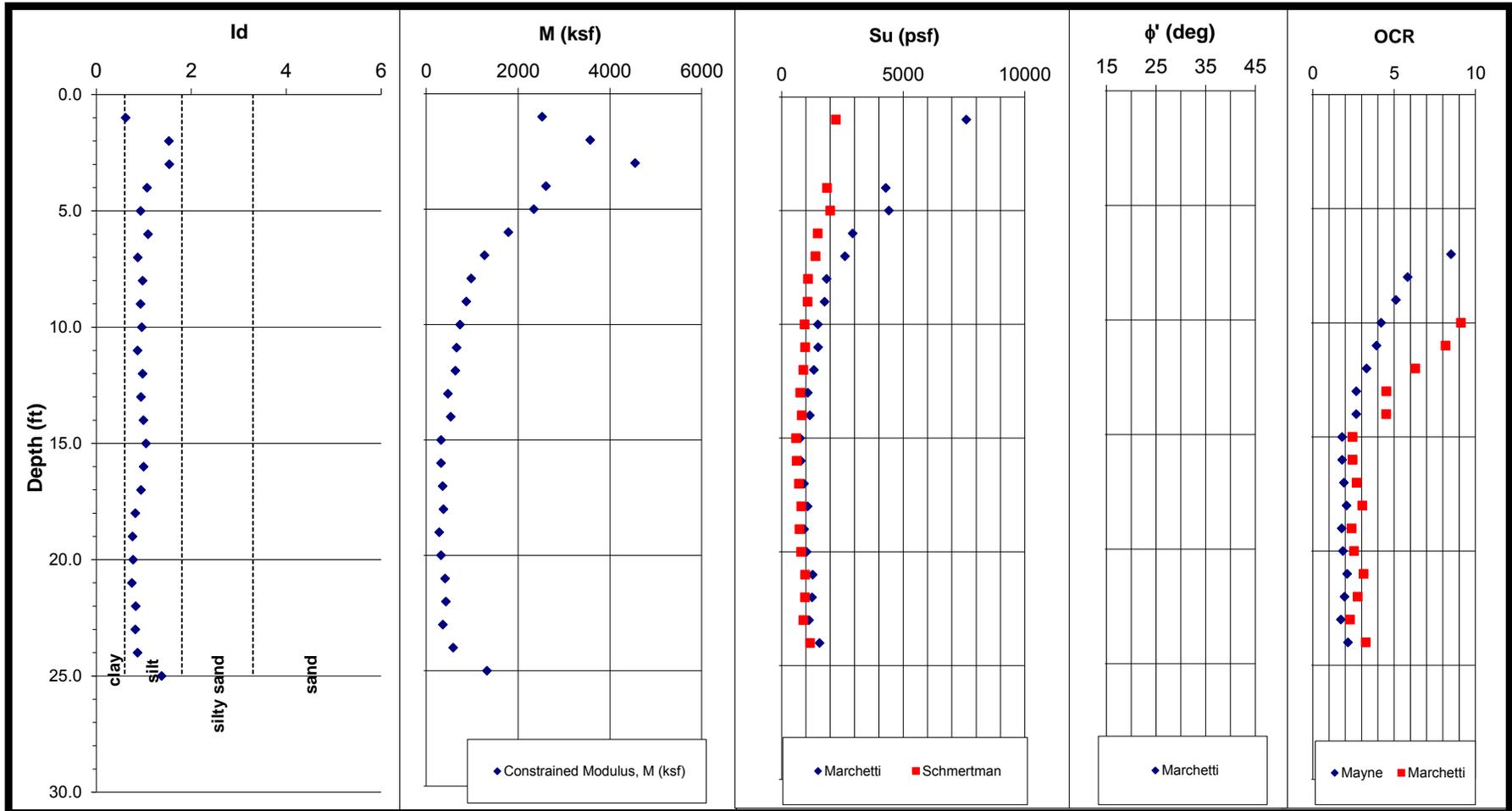
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

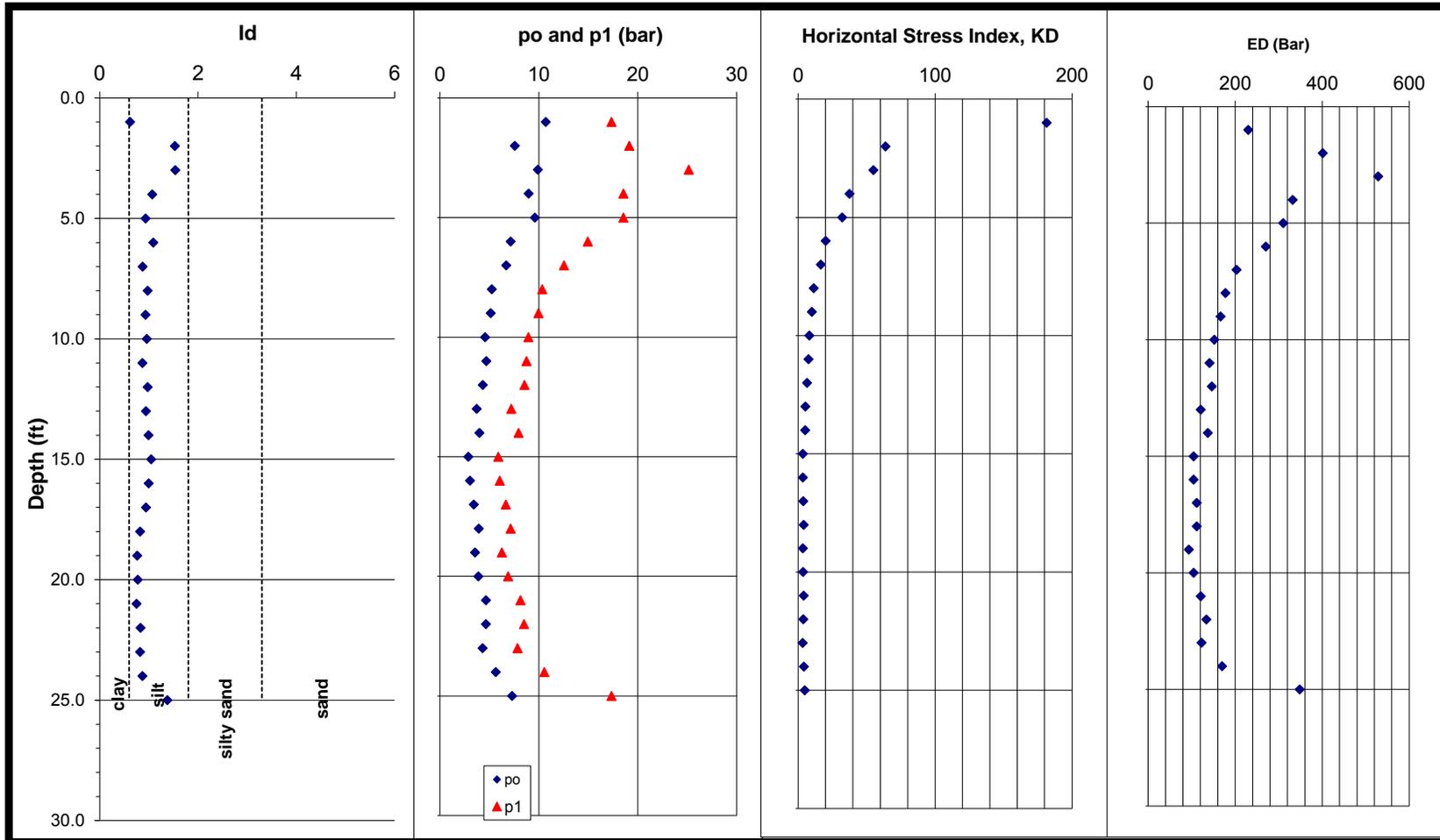
Project No.: 16-54112





### DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B1  
Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Location: Greensboro, NC  
Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-21-16  
 Sounding No: STR2\_EB2\_B1  
 Ground Water Depth (ft): N/A

|              | Membrane 1 | Membrane 2 | Membrane 3 |
|--------------|------------|------------|------------|
| $\Delta A =$ | 0.225      | 0          | 0          |
| $\Delta B =$ | 0.25       | 0          | 0          |
| Zm=          | 0          | bar        |            |

Northing 874655  
 Easting 1777453

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



### DILATOMETER TEST RESULTS

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | po<br>(bar) | p1<br>(bar) | p2<br>(bar) | uo<br>(psf) | $\gamma_1^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}^1$<br>(psf) | ld   | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------|-------------|-------------|-------------|-----------------------|------------------------|--------------------------|------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 10.8       | 17.6       |            | 10.7        | 17.35       |             | 0           | 123                   | 123                    | 123                      | 0.62 | 181.6          | 230                     | 8.9            | 92.4             | 1134.0           |                   | 5.24           | 481                     | 7594                                 | 2237                                 | 2524       |
| 2.0                        | 7.9        | 19.4       |            | 7.6         | 19.15       |             | 0           | 124                   | 248                    | 248                      | 1.53 | 63.9           | 402                     |                |                  |                  |                   | 4.26           | 839                     |                                      |                                      | 3570       |
| 3.0                        | 10.4       | 25.4       | 0.15       | 9.9         | 25.15       | 0.38        | 0           | 128                   | 376                    | 376                      | 1.54 | 55.1           | 529                     |                |                  |                  |                   | 4.11           | 1105                    |                                      |                                      | 4548       |
| 4.0                        | 9.2        | 18.8       |            | 9.0         | 18.55       |             | 0           | 124                   | 497                    | 497                      | 1.07 | 37.7           | 332                     | 3.9            | 19.2             | 97.5             |                   | 3.76           | 694                     | 4292                                 | 1873                                 | 2608       |
| 5.0                        | 9.8        | 18.8       |            | 9.6         | 18.55       |             | 0           | 124                   | 622                    | 622                      | 0.93 | 32.2           | 311                     | 3.6            | 16.4             | 76.5             |                   | 3.61           | 649                     | 4419                                 | 2005                                 | 2341       |
| 6.0                        | 7.3        | 15.2       | 0          | 7.2         | 14.95       |             | 0           | 122                   | 743                    | 743                      | 1.09 | 20.1           | 271                     | 2.8            | 10.2             | 36.6             |                   | 3.16           | 565                     | 2926                                 | 1494                                 | 1786       |
| 7.0                        | 6.75       | 12.8       |            | 6.7         | 12.55       |             | 0           | 120                   | 837                    | 837                      | 0.87 | 16.7           | 203                     | 2.5            | 8.5              | 27.4             |                   | 2.99           | 424                     | 2616                                 | 1399                                 | 1267       |
| 8.0                        | 5.25       | 10.6       |            | 5.2         | 10.35       |             | 0           | 117                   | 954                    | 954                      | 0.98 | 11.5           | 178                     | 2.0            | 5.8              | 15.2             |                   | 2.63           | 371                     | 1859                                 | 1093                                 | 975        |
| 9.0                        | 5.15       | 10.2       | 0          | 5.1         | 9.95        |             | 0           | 117                   | 1071                   | 1071                     | 0.93 | 10.0           | 167                     | 1.8            | 5.1              | 12.4             |                   | 2.50           | 348                     | 1770                                 | 1075                                 | 872        |
| 10.0                       | 4.55       | 9.2        |            | 4.6         | 8.95        |             | 0           | 116                   | 1156                   | 1156                     | 0.96 | 8.3            | 152                     | 1.6            | 4.2              | 9.1              |                   | 2.31           | 318                     | 1495                                 | 954                                  | 733        |
| 11.0                       | 4.65       | 9          |            | 4.7         | 8.75        |             | 0           | 115                   | 1271                   | 1271                     | 0.87 | 7.7            | 141                     | 1.6            | 3.9              | 8.2              |                   | 2.24           | 295                     | 1506                                 | 978                                  | 659        |
| 12.0                       | 4.3        | 8.8        | 0          | 4.3         | 8.55        |             | 0           | 115                   | 1386                   | 1386                     | 0.98 | 6.5            | 147                     | 1.4            | 3.3              | 6.3              |                   | 2.07           | 306                     | 1334                                 | 903                                  | 634        |
| 13.0                       | 3.65       | 7.45       |            | 3.7         | 7.2         |             | 0           | 113                   | 1470                   | 1470                     | 0.94 | 5.3            | 121                     | 1.2            | 2.7              | 4.5              |                   | 1.86           | 253                     | 1085                                 | 775                                  | 470        |
| 14.0                       | 3.95       | 8.2        |            | 4.0         | 7.95        |             | 0           | 114                   | 1585                   | 1585                     | 0.99 | 5.3            | 138                     | 1.2            | 2.7              | 4.5              |                   | 1.86           | 287                     | 1166                                 | 833                                  | 533        |
| 15.0                       | 2.8        | 6.15       | 0          | 2.9         | 5.9         |             | 0           | 111                   | 1695                   | 1695                     | 1.05 | 3.5            | 105                     | 0.9            | 1.8              | 2.4              |                   | 1.47           | 219                     | 764                                  | 602                                  | 321        |
| 16.0                       | 2.95       | 6.3        |            | 3.0         | 6.05        |             | 0           | 111                   | 1779                   | 1779                     | 1.00 | 3.6            | 105                     | 0.9            | 1.8              | 2.5              |                   | 1.47           | 219                     | 804                                  | 633                                  | 321        |
| 17.0                       | 3.35       | 6.9        |            | 3.4         | 6.65        |             | 0           | 112                   | 1891                   | 1891                     | 0.94 | 3.8            | 112                     | 0.9            | 1.9              | 2.7              |                   | 1.52           | 234                     | 922                                  | 715                                  | 357        |
| 18.0                       | 3.85       | 7.4        | 0          | 3.9         | 7.15        |             | 0           | 113                   | 2004                   | 2004                     | 0.82 | 4.1            | 112                     | 1.0            | 2.1              | 3.0              |                   | 1.60           | 234                     | 1077                                 | 819                                  | 373        |
| 19.0                       | 3.45       | 6.5        |            | 3.5         | 6.25        |             | 0           | 111                   | 2117                   | 2117                     | 0.76 | 3.5            | 94                      | 0.9            | 1.8              | 2.4              |                   | 1.43           | 196                     | 937                                  | 741                                  | 281        |
| 20.0                       | 3.8        | 7.15       |            | 3.9         | 6.9         |             | 0           | 113                   | 2230                   | 2230                     | 0.78 | 3.6            | 105                     | 0.9            | 1.9              | 2.5              |                   | 1.47           | 219                     | 1035                                 | 811                                  | 323        |
| 21.0                       | 4.6        | 8.4        | 0          | 4.7         | 8.15        |             | 0           | 114                   | 2344                   | 2344                     | 0.75 | 4.2            | 121                     | 1.0            | 2.1              | 3.1              |                   | 1.61           | 253                     | 1285                                 | 973                                  | 407        |
| 22.0                       | 4.6        | 8.75       |            | 4.6         | 8.5         |             | 0           | 115                   | 2529                   | 2529                     | 0.83 | 3.8            | 134                     | 1.0            | 2.0              | 2.8              |                   | 1.53           | 280                     | 1255                                 | 969                                  | 428        |
| 23.0                       | 4.25       | 8.1        |            | 4.3         | 7.85        |             | 0           | 114                   | 2643                   | 2643                     | 0.82 | 3.4            | 123                     | 0.9            | 1.7              | 2.3              |                   | 1.41           | 257                     | 1130                                 | 899                                  | 362        |
| 24.0                       | 5.65       | 10.8       | 0          | 5.6         | 10.55       |             | 0           | 117                   | 2761                   | 2761                     | 0.87 | 4.3            | 170                     | 1.0            | 2.2              | 3.3              |                   | 1.64           | 356                     | 1566                                 | 1178                                 | 584        |
| 25.0                       | 7.55       | 17.6       |            | 7.3         | 17.35       |             | 0           | 123                   | 3084                   | 3084                     | 1.38 | 4.9            | 349                     |                |                  |                  |                   | 1.81           | 729                     |                                      |                                      | 1321       |



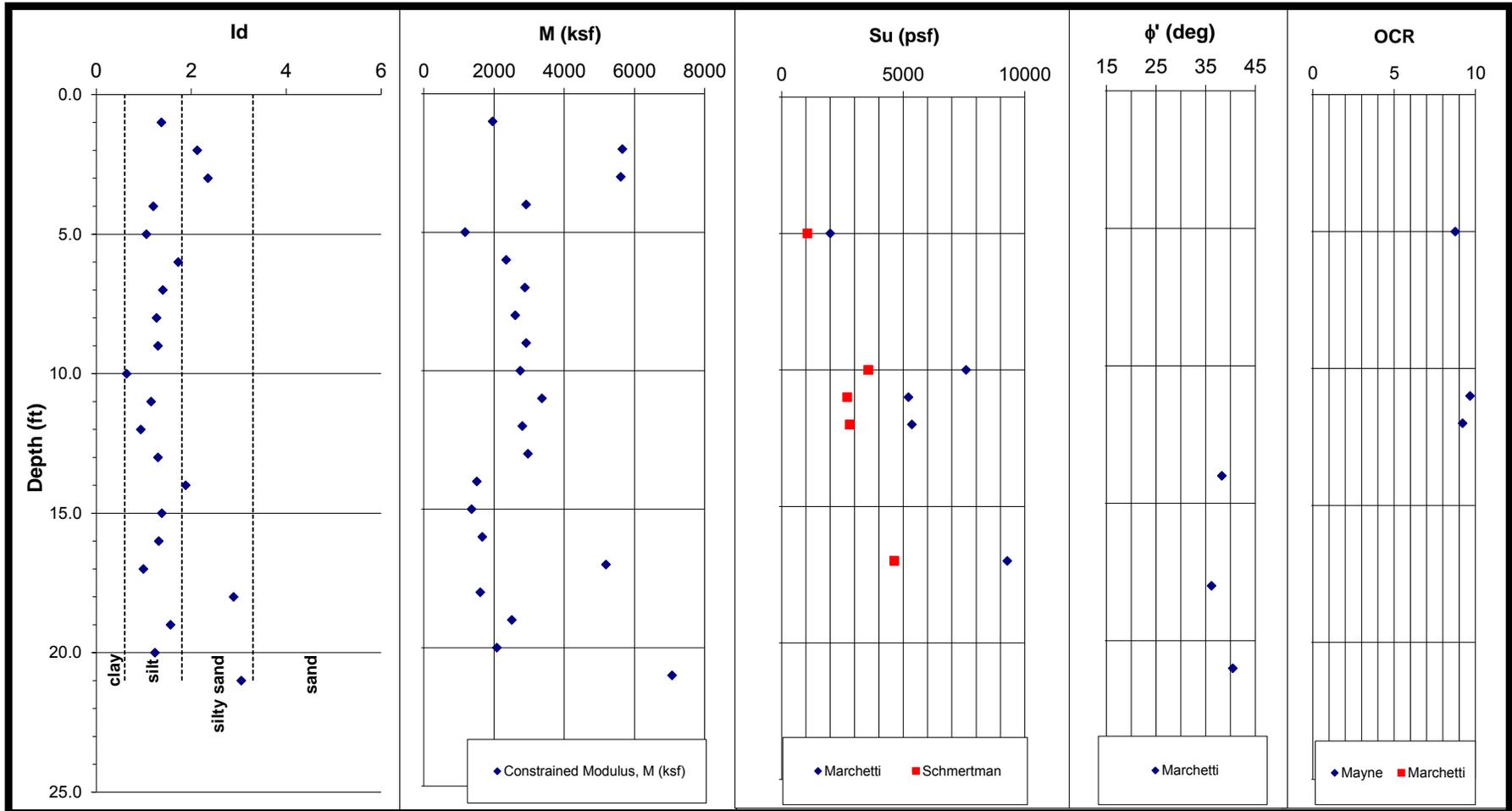
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





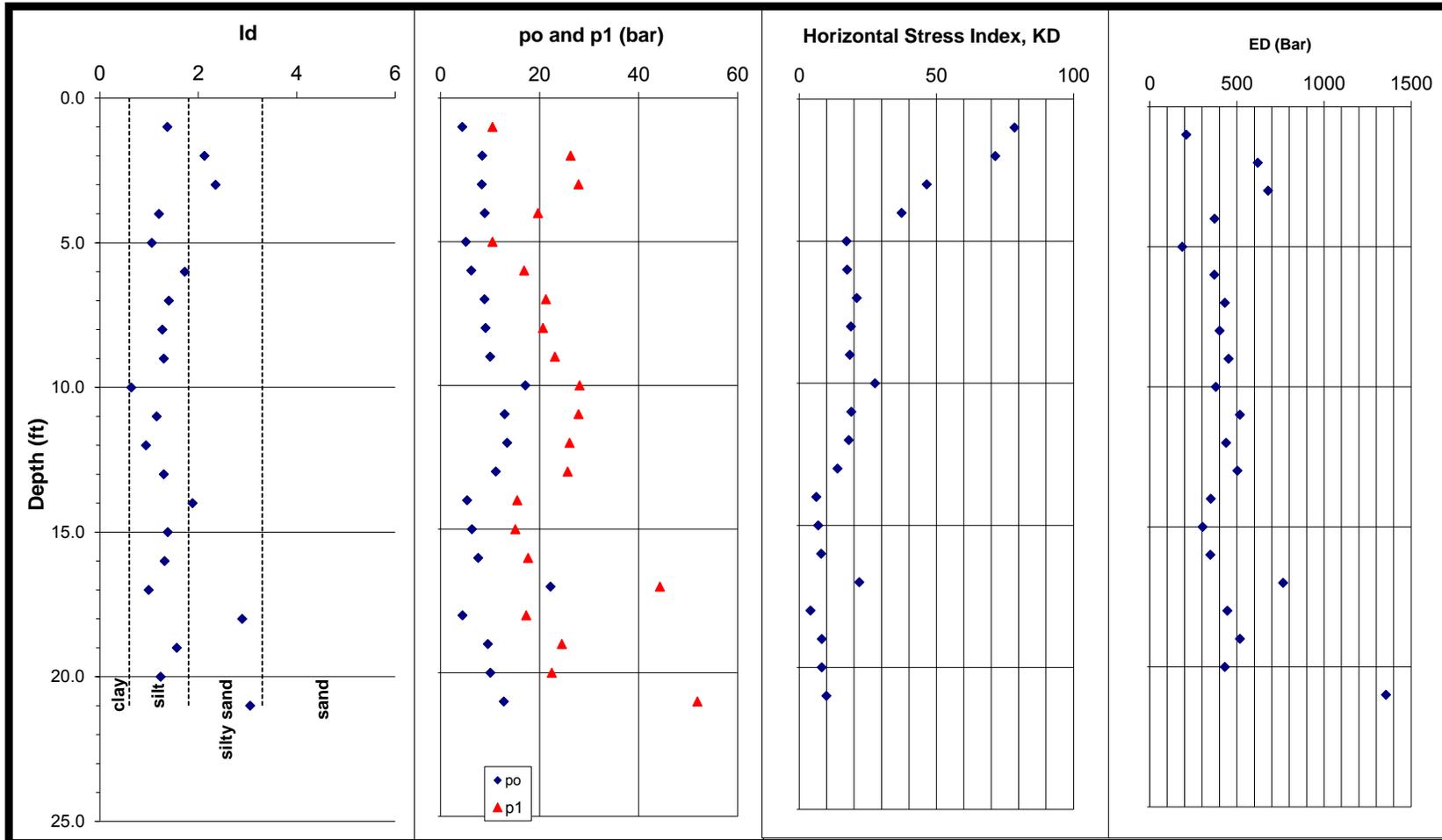
## DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI)  
 Job Location: Greensboro, NC  
 Date: 12-21-16  
 Sounding No: STR2\_EB2\_B2  
 Ground Water Depth (ft): N/A

|              |                   |                   |                   |
|--------------|-------------------|-------------------|-------------------|
|              | <b>Membrane 1</b> | <b>Membrane 2</b> | <b>Membrane 3</b> |
| $\Delta A =$ | 0.25              | 0                 | 0                 |
| $\Delta B =$ | 0.125             | 0                 | 0                 |
| $Z_m =$      | 0                 | bar               |                   |

Northing 874591  
 Easting 1777450

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



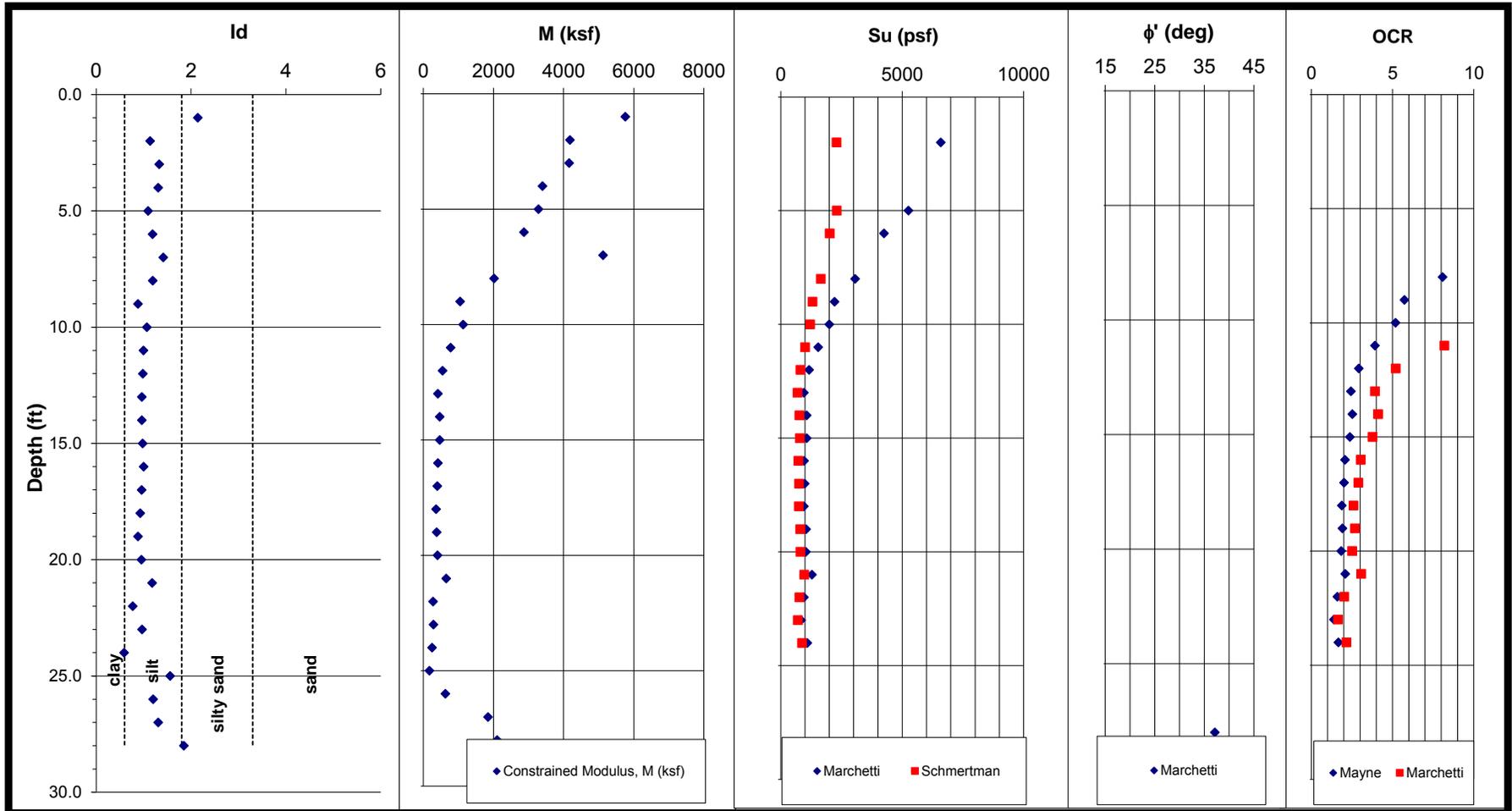
**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_r^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 4.45       | 10.6       |            | 4.4                     | 10.475                  |                         | 0                       | 117                   | 117                    | 117                     | 1.37           | 78.6           | 210                     |                |                  |                  |                   | 4.45           | 439                     |                                      |                                      | 1956       |
| 2.0                        | 9          | 26.4       |            | 8.4                     | 26.275                  |                         | 0                       | 128                   | 245                    | 245                     | 2.13           | 71.6           | 620                     |                |                  |                  | 47.9              | 4.36           | 1296                    |                                      |                                      | 5653       |
| 3.0                        | 9          | 28         | 0          | 8.3                     | 27.875                  |                         | 0                       | 128                   | 373                    | 373                     | 2.35           | 46.5           | 679                     |                |                  |                  | 46.5              | 3.96           | 1417                    |                                      |                                      | 5606       |
| 4.0                        | 9.2        | 19.8       |            | 8.9                     | 19.675                  |                         | 0                       | 125                   | 500                    | 500                     | 1.20           | 37.3           | 373                     |                |                  |                  |                   | 3.75           | 778                     |                                      |                                      | 2916       |
| 5.0                        | 5.1        | 10.6       |            | 5.1                     | 10.475                  |                         | 0                       | 117                   | 618                    | 618                     | 1.06           | 17.2           | 187                     | 2.5            | 8.8              | 28.8             |                   | 3.01           | 390                     | 2005                                 | 1064                                 | 1176       |
| 6.0                        | 6.45       | 17         | 0          | 6.2                     | 16.875                  |                         | 0                       | 123                   | 740                    | 740                     | 1.73           | 17.5           | 371                     |                |                  |                  |                   | 3.03           | 774                     |                                      |                                      | 2345       |
| 7.0                        | 9.2        | 21.4       |            | 8.9                     | 21.275                  |                         | 0                       | 126                   | 881                    | 881                     | 1.40           | 21.0           | 431                     |                |                  |                  |                   | 3.20           | 900                     |                                      |                                      | 2882       |
| 8.0                        | 9.4        | 20.8       |            | 9.1                     | 20.675                  |                         | 0                       | 126                   | 1007                   | 1007                    | 1.27           | 18.9           | 402                     |                |                  |                  |                   | 3.10           | 839                     |                                      |                                      | 2602       |
| 9.0                        | 10.4       | 23.2       | 0.15       | 10.0                    | 23.075                  | 0.40                    | 0                       | 127                   | 1134                   | 1134                    | 1.30           | 18.5           | 453                     |                |                  |                  |                   | 3.08           | 945                     |                                      |                                      | 2913       |
| 10.0                       | 17.4       | 28.2       |            | 17.1                    | 28.075                  |                         | 0                       | 129                   | 1293                   | 1293                    | 0.64           | 27.7           | 380                     | 3.3            | 14.1             | 60.3             |                   | 3.46           | 793                     | 7590                                 | 3577                                 | 2748       |
| 11.0                       | 13.4       | 28         |            | 12.9                    | 27.875                  |                         | 0                       | 129                   | 1422                   | 1422                    | 1.15           | 19.0           | 518                     | 2.7            | 9.7              | 33.5             |                   | 3.11           | 1082                    | 5219                                 | 2702                                 | 3364       |
| 12.0                       | 13.8       | 26.2       | 0.95       | 13.4                    | 26.075                  | 1.20                    | 0                       | 129                   | 1551                   | 1551                    | 0.94           | 18.1           | 438                     | 2.6            | 9.2              | 31.1             |                   | 3.06           | 915                     | 5360                                 | 2809                                 | 2802       |
| 13.0                       | 11.6       | 25.8       |            | 11.2                    | 25.675                  |                         | 0                       | 128                   | 1668                   | 1668                    | 1.30           | 14.0           | 504                     |                |                  |                  |                   | 2.82           | 1052                    |                                      |                                      | 2963       |
| 14.0                       | 5.6        | 15.6       |            | 5.4                     | 15.475                  |                         | 0                       | 122                   | 1790                   | 1790                    | 1.88           | 6.3            | 351                     |                |                  |                  | 38.3              | 2.06           | 732                     |                                      |                                      | 1509       |
| 15.0                       | 6.5        | 15.2       | 0.25       | 6.3                     | 15.075                  | 0.50                    | 0                       | 122                   | 1912                   | 1912                    | 1.38           | 6.9            | 303                     |                |                  |                  |                   | 2.14           | 633                     |                                      |                                      | 1357       |
| 16.0                       | 7.85       | 17.8       |            | 7.6                     | 17.675                  |                         | 0                       | 124                   | 1978                   | 1978                    | 1.32           | 8.0            | 349                     |                |                  |                  |                   | 2.29           | 729                     |                                      |                                      | 1667       |
| 17.0                       | 23         | 44.4       |            | 22.2                    | 44.275                  |                         | 0                       | 136                   | 2114                   | 2114                    | 0.99           | 21.9           | 766                     | 2.9            | 11.2             | 41.9             |                   | 3.24           | 1600                    | 9281                                 | 4636                                 | 5190       |
| 18.0                       | 4.8        | 17.4       | 0          | 4.4                     | 17.275                  |                         | 0                       | 122                   | 2235                   | 2235                    | 2.89           | 4.1            | 445                     |                |                  |                  | 36.2              | 1.73           | 930                     |                                      |                                      | 1609       |
| 19.0                       | 10         | 24.6       |            | 9.5                     | 24.475                  |                         | 0                       | 128                   | 2423                   | 2423                    | 1.57           | 8.2            | 518                     |                |                  |                  |                   | 2.31           | 1082                    |                                      |                                      | 2502       |
| 20.0                       | 10.4       | 22.6       |            | 10.1                    | 22.475                  |                         | 0                       | 127                   | 2549                   | 2549                    | 1.23           | 8.2            | 431                     |                |                  |                  |                   | 2.31           | 900                     |                                      |                                      | 2078       |
| 21.0                       | 14.4       | 52         | 0          | 12.8                    | 51.875                  |                         | 0                       | 136                   | 2685                   | 2685                    | 3.06           | 9.9            | 1356                    |                |                  |                  | 40.5              | 2.50           | 2833                    |                                      |                                      | 7069       |



# DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B3  
 Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
 Location: Greensboro, NC  
 Project No.: 16-54112





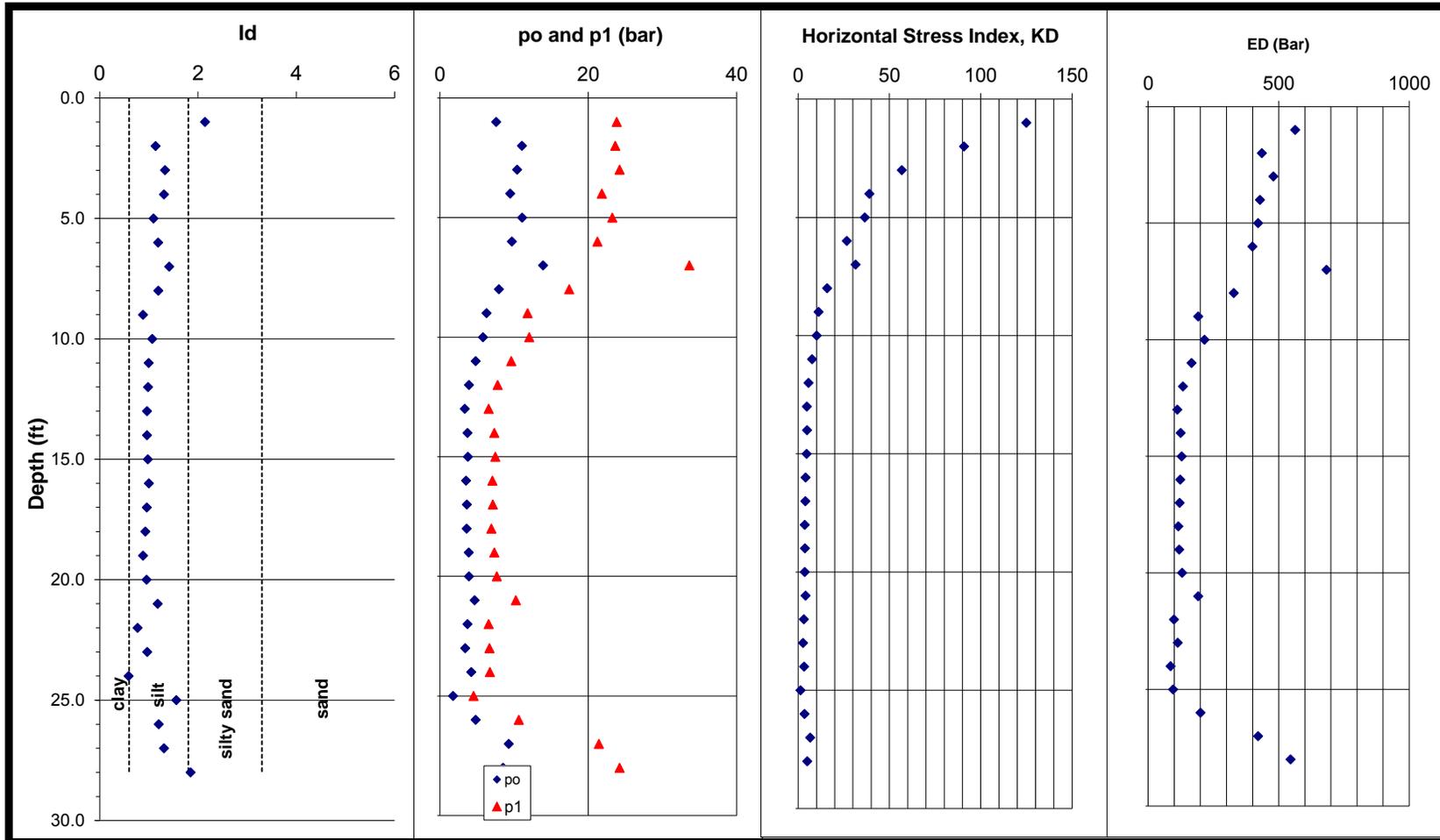
# DILATOMETER TEST RESULTS

Test ID: STR2\_EB2\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-21-16  
 Sounding No: STR2\_EB2\_B3  
 Ground Water Depth (ft): N/A

|              |                   |                   |                   |
|--------------|-------------------|-------------------|-------------------|
|              | <b>Membrane 1</b> | <b>Membrane 2</b> | <b>Membrane 3</b> |
| $\Delta A =$ | 0.25              | 0                 | 0                 |
| $\Delta B =$ | 0.175             | 0                 | 0                 |
| Zm=          | 0                 | bar               |                   |

Northing 874627  
 Easting 1777441

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_1^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 8.1        | 24         |            | 7.6                     | 23.825                  |                         | 0                       | 127                   | 127                    | 127                     | 2.14           | 125.0          | 564                     |                |                  |                  | 49.4              | 4.89           | 1178                    |                                      |                                      | 5760       |
| 2.0                        | 11.4       | 23.8       |            | 11.1                    | 23.625                  |                         | 0                       | 127                   | 254                    | 254                     | 1.14           | 90.9           | 436                     | 6.3            | 46.3             | 385.2            |                   | 4.59           | 911                     | 6592                                 | 2308                                 | 4182       |
| 3.0                        | 10.8       | 24.4       | 0          | 10.4                    | 24.225                  |                         | 0                       | 128                   | 382                    | 382                     | 1.33           | 56.9           | 480                     |                |                  |                  |                   | 4.15           | 1003                    |                                      |                                      | 4157       |
| 4.0                        | 9.8        | 22         |            | 9.5                     | 21.825                  |                         | 0                       | 126                   | 505                    | 505                     | 1.31           | 39.1           | 429                     |                |                  |                  |                   | 3.79           | 896                     |                                      |                                      | 3397       |
| 5.0                        | 11.4       | 23.4       |            | 11.1                    | 23.225                  |                         | 0                       | 127                   | 632                    | 632                     | 1.10           | 36.6           | 422                     | 3.9            | 18.6             | 93.1             |                   | 3.73           | 881                     | 5260                                 | 2312                                 | 3283       |
| 6.0                        | 10         | 21.4       | 0          | 9.7                     | 21.225                  |                         | 0                       | 126                   | 758                    | 758                     | 1.19           | 26.7           | 400                     | 3.3            | 13.6             | 57.1             |                   | 3.43           | 835                     | 4261                                 | 2026                                 | 2865       |
| 7.0                        | 14.6       | 33.8       |            | 13.9                    | 33.625                  |                         | 0                       | 132                   | 922                    | 922                     | 1.42           | 31.5           | 684                     |                |                  |                  |                   | 3.59           | 1429                    |                                      |                                      | 5124       |
| 8.0                        | 8.15       | 17.6       |            | 7.9                     | 17.425                  |                         | 0                       | 124                   | 1046                   | 1046                    | 1.19           | 15.9           | 329                     | 2.4            | 8.1              | 25.3             |                   | 2.94           | 687                     | 3065                                 | 1660                                 | 2017       |
| 9.0                        | 6.3        | 12         | 0.5        | 6.3                     | 11.825                  | 0.75                    | 0                       | 119                   | 1165                   | 1165                    | 0.88           | 11.3           | 192                     | 2.0            | 5.7              | 14.8             |                   | 2.61           | 401                     | 2225                                 | 1313                                 | 1049       |
| 10.0                       | 5.85       | 12.2       |            | 5.8                     | 12.025                  |                         | 0                       | 119                   | 1191                   | 1191                    | 1.07           | 10.2           | 216                     | 1.9            | 5.2              | 12.7             |                   | 2.52           | 451                     | 2003                                 | 1212                                 | 1135       |
| 11.0                       | 4.8        | 9.8        |            | 4.8                     | 9.625                   |                         | 0                       | 116                   | 1307                   | 1307                    | 1.00           | 7.7            | 167                     | 1.6            | 3.9              | 8.2              |                   | 2.24           | 348                     | 1552                                 | 1007                                 | 780        |
| 12.0                       | 3.85       | 7.95       | 0          | 3.9                     | 7.775                   |                         | 0                       | 114                   | 1421                   | 1421                    | 0.99           | 5.8            | 134                     | 1.3            | 2.9              | 5.2              |                   | 1.95           | 280                     | 1172                                 | 818                                  | 545        |
| 13.0                       | 3.25       | 6.75       |            | 3.3                     | 6.575                   |                         | 0                       | 112                   | 1457                   | 1457                    | 0.96           | 4.8            | 112                     | 1.1            | 2.4              | 3.9              |                   | 1.76           | 234                     | 957                                  | 699                                  | 413        |
| 14.0                       | 3.65       | 7.5        |            | 3.7                     | 7.325                   |                         | 0                       | 113                   | 1570                   | 1570                    | 0.96           | 5.0            | 125                     | 1.2            | 2.5              | 4.1              |                   | 1.80           | 261                     | 1075                                 | 779                                  | 469        |
| 15.0                       | 3.7        | 7.65       | 0          | 3.8                     | 7.475                   |                         | 0                       | 114                   | 1684                   | 1684                    | 0.98           | 4.7            | 128                     | 1.1            | 2.4              | 3.8              |                   | 1.74           | 268                     | 1072                                 | 788                                  | 467        |
| 16.0                       | 3.45       | 7.25       |            | 3.5                     | 7.075                   |                         | 0                       | 113                   | 1807                   | 1807                    | 1.00           | 4.1            | 123                     | 1.0            | 2.1              | 3.0              |                   | 1.61           | 257                     | 970                                  | 738                                  | 412        |
| 17.0                       | 3.55       | 7.3        |            | 3.6                     | 7.125                   |                         | 0                       | 113                   | 1920                   | 1920                    | 0.96           | 4.0            | 121                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 253                     | 990                                  | 759                                  | 397        |
| 18.0                       | 3.5        | 7.1        | 0          | 3.6                     | 6.925                   |                         | 0                       | 113                   | 2032                   | 2032                    | 0.93           | 3.7            | 116                     | 0.9            | 1.9              | 2.6              |                   | 1.50           | 242                     | 962                                  | 750                                  | 362        |
| 19.0                       | 3.8        | 7.5        |            | 3.9                     | 7.325                   |                         | 0                       | 113                   | 2152                   | 2152                    | 0.88           | 3.8            | 119                     | 0.9            | 1.9              | 2.7              |                   | 1.52           | 249                     | 1046                                 | 812                                  | 378        |
| 20.0                       | 3.85       | 7.85       |            | 3.9                     | 7.675                   |                         | 0                       | 114                   | 2266                   | 2266                    | 0.96           | 3.6            | 130                     | 0.9            | 1.8              | 2.5              |                   | 1.48           | 272                     | 1044                                 | 819                                  | 403        |
| 21.0                       | 4.7        | 10.4       | 0          | 4.7                     | 10.225                  |                         | 0                       | 117                   | 2383                   | 2383                    | 1.18           | 4.1            | 192                     | 1.0            | 2.1              | 3.1              |                   | 1.62           | 401                     | 1289                                 | 979                                  | 651        |
| 22.0                       | 3.6        | 6.75       |            | 3.7                     | 6.575                   |                         | 0                       | 112                   | 2464                   | 2464                    | 0.77           | 3.1            | 99                      | 0.8            | 1.6              | 2.0              |                   | 1.33           | 207                     | 956                                  | 776                                  | 275        |
| 23.0                       | 3.3        | 6.85       |            | 3.4                     | 6.675                   |                         | 0                       | 112                   | 2576                   | 2576                    | 0.97           | 2.8            | 114                     | 0.7            | 1.4              | 1.6              |                   | 1.21           | 238                     | 844                                  | 709                                  | 287        |
| 24.0                       | 4.1        | 6.9        | 0          | 4.2                     | 6.725                   |                         | 0                       | 112                   | 2688                   | 2688                    | 0.59           | 3.3            | 87                      | 0.8            | 1.7              | 2.2              |                   | 1.36           | 181                     | 1101                                 | 884                                  | 246        |
| 25.0                       | 1.65       | 4.7        |            | 1.8                     | 4.525                   |                         | 0                       | 108                   | 2693                   | 2693                    | 1.56           | 1.4            | 96                      |                |                  |                  |                   | 0.85           | 200                     |                                      |                                      | 170        |
| 26.0                       | 4.85       | 10.8       |            | 4.8                     | 10.625                  |                         | 0                       | 118                   | 2810                   | 2810                    | 1.20           | 3.6            | 201                     |                |                  |                  |                   | 1.49           | 420                     |                                      |                                      | 626        |
| 27.0                       | 9.6        | 21.6       | 0          | 9.3                     | 21.425                  |                         | 0                       | 126                   | 2936                   | 2936                    | 1.31           | 6.6            | 422                     |                |                  |                  |                   | 2.09           | 881                     |                                      |                                      | 1843       |
| 28.0                       | 9          | 24.4       |            | 8.5                     | 24.225                  |                         | 0                       | 127                   | 3559                   | 3559                    | 1.85           | 5.0            | 546                     |                |                  |                  | 37.2              | 1.84           | 1140                    |                                      |                                      | 2101       |



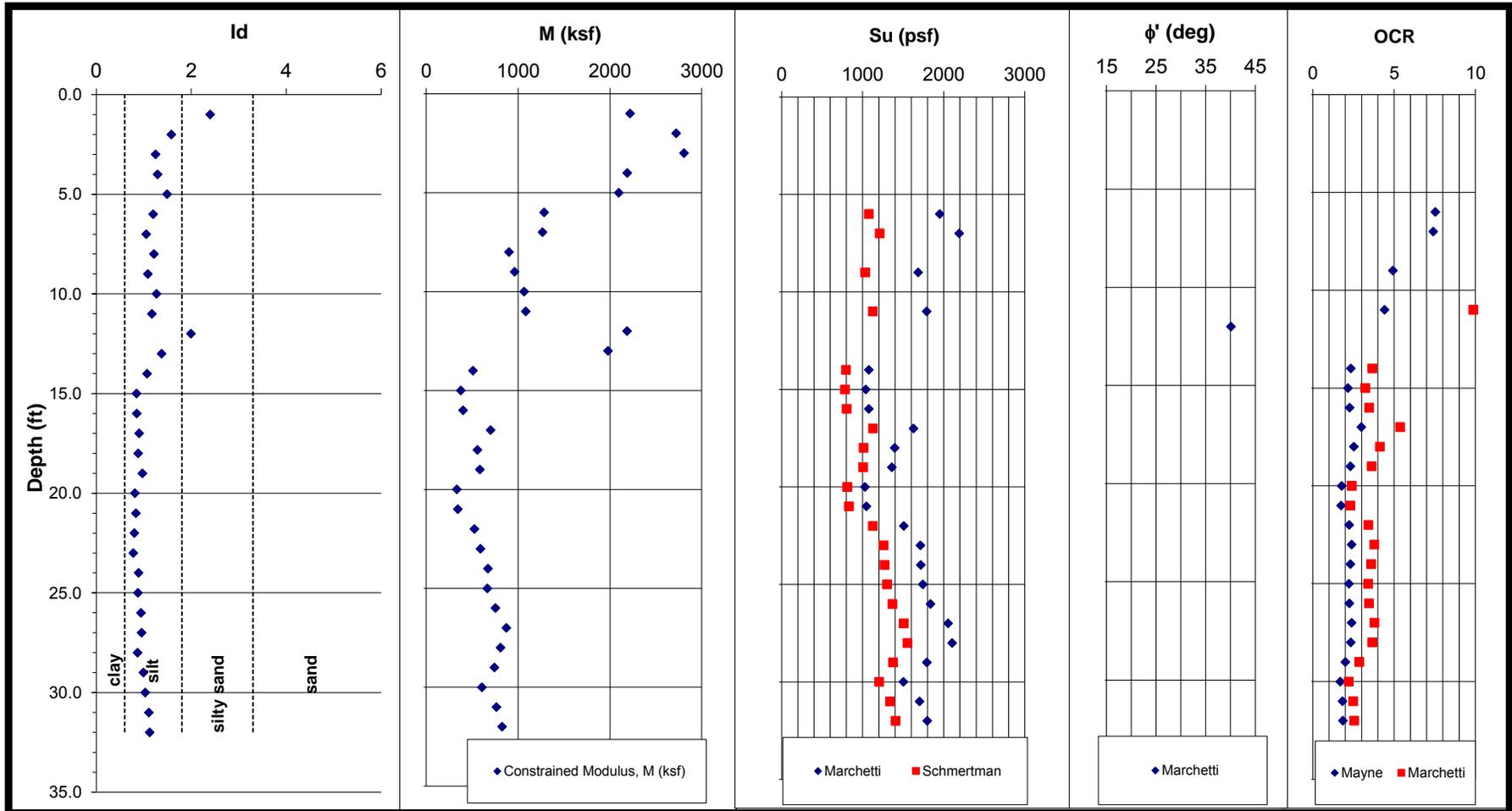
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

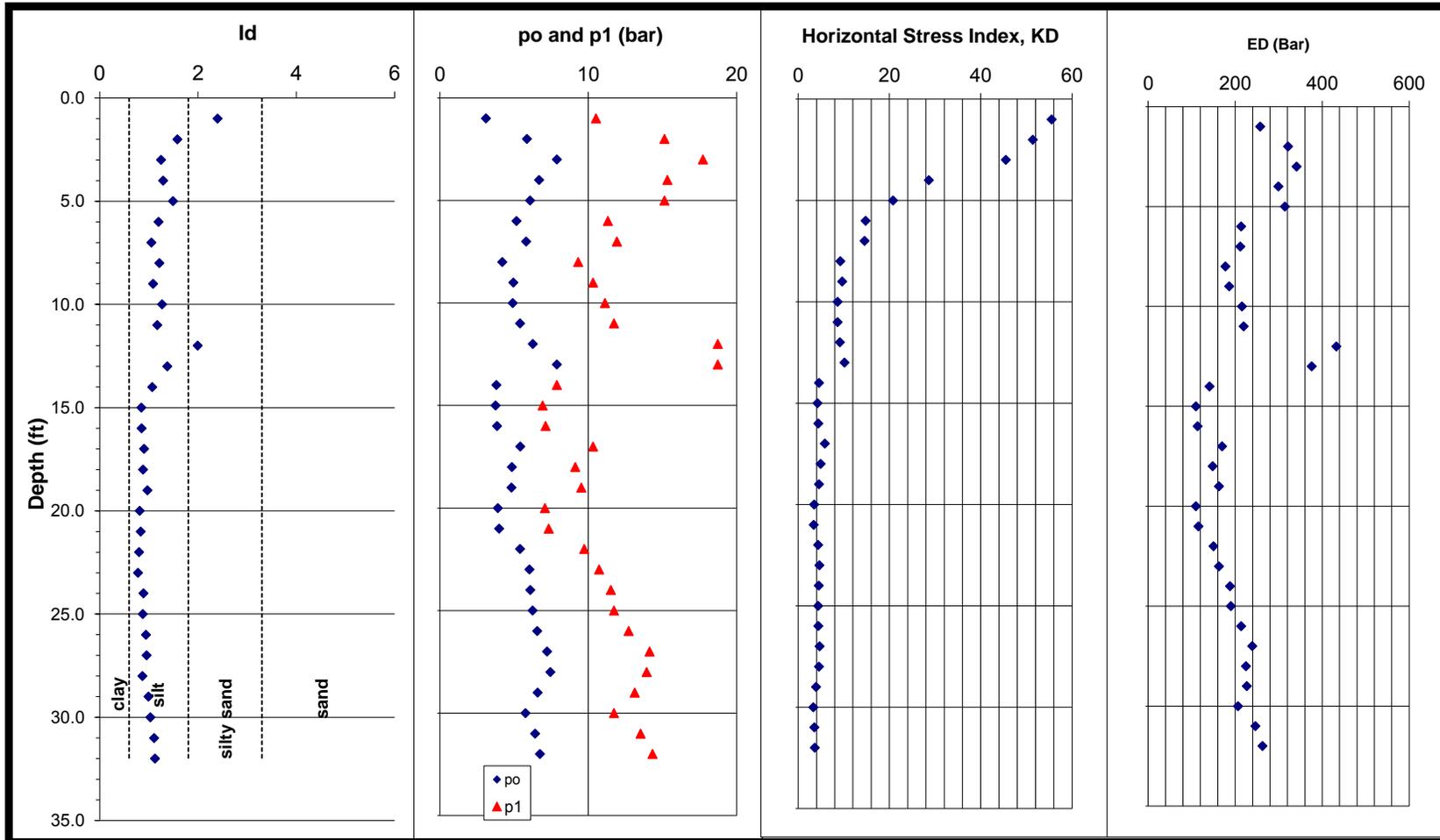
Project No.: 16-54112





### DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B1  
Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Location: Greensboro, NC  
Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR3\_EB1\_B1  
 Ground Water Depth (ft): N/A

Membrane 1    Membrane 2    Membrane 3  
 $\Delta A =$  0.2            0            0  
 $\Delta B =$  0.275         0            0  
 $Z_m =$  0            bar

Northing    874663  
 Easting     1777566

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_1^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | I <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 3.25       | 10.8       |            | 3.1                     | 10.525                  |                         | 0                       | 116                   | 116                    | 116                     | 2.40           | 55.6           | 258                     |                |                  |                  | 47.1              | 4.12           | 538                     |                                      |                                      | 2220       |
| 2.0                        | 6.1        | 15.4       |            | 5.9                     | 15.125                  |                         | 0                       | 122                   | 238                    | 238                     | 1.58           | 51.4           | 322                     |                |                  |                  |                   | 4.05           | 672                     |                                      |                                      | 2720       |
| 3.0                        | 8.15       | 18         | 0          | 7.9                     | 17.725                  |                         | 0                       | 124                   | 362                    | 362                     | 1.25           | 45.5           | 342                     |                |                  |                  |                   | 3.93           | 713                     |                                      |                                      | 2807       |
| 4.0                        | 6.9        | 15.6       |            | 6.7                     | 15.325                  |                         | 0                       | 122                   | 488                    | 488                     | 1.29           | 28.7           | 300                     |                |                  |                  |                   | 3.50           | 626                     |                                      |                                      | 2189       |
| 5.0                        | 6.3        | 15.4       |            | 6.1                     | 15.125                  |                         | 0                       | 122                   | 609                    | 609                     | 1.49           | 20.8           | 314                     |                |                  |                  |                   | 3.19           | 656                     |                                      |                                      | 2096       |
| 6.0                        | 5.25       | 11.6       | 0          | 5.2                     | 11.325                  |                         | 0                       | 118                   | 727                    | 727                     | 1.20           | 14.8           | 214                     | 2.3            | 7.5              | 22.7             |                   | 2.87           | 447                     | 1954                                 | 1077                                 | 1284       |
| 7.0                        | 5.9        | 12.2       |            | 5.8                     | 11.925                  |                         | 0                       | 119                   | 833                    | 833                     | 1.05           | 14.6           | 212                     | 2.3            | 7.4              | 22.1             |                   | 2.86           | 443                     | 2192                                 | 1213                                 | 1266       |
| 8.0                        | 4.25       | 9.6        |            | 4.2                     | 9.325                   |                         | 0                       | 116                   | 949                    | 949                     | 1.22           | 9.3            | 178                     |                |                  |                  |                   | 2.42           | 371                     |                                      |                                      | 899        |
| 9.0                        | 5          | 10.6       | 0          | 4.9                     | 10.325                  |                         | 0                       | 117                   | 1066                   | 1066                    | 1.09           | 9.7            | 187                     | 1.8            | 4.9              | 11.7             |                   | 2.47           | 390                     | 1685                                 | 1033                                 | 963        |
| 10.0                       | 5          | 11.4       |            | 4.9                     | 11.125                  |                         | 0                       | 118                   | 1181                   | 1181                    | 1.27           | 8.7            | 216                     |                |                  |                  |                   | 2.36           | 451                     |                                      |                                      | 1064       |
| 11.0                       | 5.5        | 12         |            | 5.4                     | 11.725                  |                         | 0                       | 119                   | 1299                   | 1299                    | 1.17           | 8.7            | 220                     | 1.7            | 4.4              | 9.9              |                   | 2.36           | 458                     | 1790                                 | 1128                                 | 1082       |
| 12.0                       | 6.65       | 19         | 0          | 6.3                     | 18.725                  |                         | 0                       | 124                   | 1423                   | 1423                    | 1.99           | 9.2            | 433                     |                |                  |                  | 40.1              | 2.42           | 904                     |                                      |                                      | 2187       |
| 13.0                       | 8.2        | 19         |            | 7.9                     | 18.725                  |                         | 0                       | 124                   | 1616                   | 1616                    | 1.38           | 10.2           | 376                     |                |                  |                  |                   | 2.52           | 786                     |                                      |                                      | 1978       |
| 14.0                       | 3.8        | 8.15       |            | 3.8                     | 7.875                   |                         | 0                       | 114                   | 1730                   | 1730                    | 1.07           | 4.6            | 141                     | 1.1            | 2.3              | 3.7              |                   | 1.73           | 295                     | 1077                                 | 795                                  | 509        |
| 15.0                       | 3.7        | 7.2        | 0          | 3.7                     | 6.925                   |                         | 0                       | 113                   | 1843                   | 1843                    | 0.85           | 4.2            | 110                     | 1.0            | 2.2              | 3.2              |                   | 1.64           | 230                     | 1040                                 | 783                                  | 377        |
| 16.0                       | 3.8        | 7.4        |            | 3.8                     | 7.125                   |                         | 0                       | 113                   | 1807                   | 1807                    | 0.85           | 4.4            | 114                     | 1.1            | 2.3              | 3.5              |                   | 1.68           | 238                     | 1078                                 | 803                                  | 400        |
| 17.0                       | 5.45       | 10.6       |            | 5.4                     | 10.325                  |                         | 0                       | 117                   | 1925                   | 1925                    | 0.91           | 5.9            | 170                     | 1.3            | 3.0              | 5.4              |                   | 1.97           | 356                     | 1629                                 | 1131                                 | 699        |
| 18.0                       | 4.85       | 9.4        | 0          | 4.8                     | 9.125                   |                         | 0                       | 116                   | 2040                   | 2040                    | 0.88           | 5.0            | 148                     | 1.2            | 2.5              | 4.1              |                   | 1.79           | 310                     | 1397                                 | 1012                                 | 556        |
| 19.0                       | 4.85       | 9.8        |            | 4.8                     | 9.525                   |                         | 0                       | 116                   | 2210                   | 2210                    | 0.97           | 4.6            | 163                     | 1.1            | 2.3              | 3.6              |                   | 1.71           | 341                     | 1363                                 | 1008                                 | 584        |
| 20.0                       | 3.85       | 7.35       |            | 3.9                     | 7.075                   |                         | 0                       | 113                   | 2323                   | 2323                    | 0.81           | 3.5            | 110                     | 0.9            | 1.8              | 2.4              |                   | 1.44           | 230                     | 1031                                 | 814                                  | 332        |
| 21.0                       | 3.95       | 7.6        | 0          | 4.0                     | 7.325                   |                         | 0                       | 113                   | 2436                   | 2436                    | 0.84           | 3.4            | 116                     | 0.9            | 1.7              | 2.3              |                   | 1.42           | 242                     | 1049                                 | 834                                  | 342        |
| 22.0                       | 5.4        | 10         |            | 5.4                     | 9.725                   |                         | 0                       | 116                   | 2563                   | 2563                    | 0.80           | 4.4            | 150                     | 1.1            | 2.2              | 3.4              |                   | 1.67           | 314                     | 1509                                 | 1127                                 | 524        |
| 23.0                       | 6.05       | 11         |            | 6.0                     | 10.725                  |                         | 0                       | 118                   | 2680                   | 2680                    | 0.78           | 4.7            | 163                     | 1.1            | 2.4              | 3.8              |                   | 1.73           | 341                     | 1714                                 | 1259                                 | 590        |
| 24.0                       | 6.15       | 11.8       | 0          | 6.1                     | 11.525                  |                         | 0                       | 119                   | 2799                   | 2799                    | 0.89           | 4.5            | 189                     | 1.1            | 2.3              | 3.6              |                   | 1.71           | 394                     | 1718                                 | 1272                                 | 672        |
| 25.0                       | 6.3        | 12         |            | 6.2                     | 11.725                  |                         | 0                       | 119                   | 2968                   | 2968                    | 0.88           | 4.4            | 190                     | 1.1            | 2.2              | 3.4              |                   | 1.67           | 398                     | 1745                                 | 1303                                 | 664        |
| 26.0                       | 6.65       | 13         |            | 6.6                     | 12.725                  |                         | 0                       | 120                   | 3088                   | 3088                    | 0.94           | 4.4            | 214                     | 1.1            | 2.3              | 3.5              |                   | 1.68           | 447                     | 1838                                 | 1369                                 | 753        |
| 27.0                       | 7.35       | 14.4       | 0          | 7.2                     | 14.125                  |                         | 0                       | 121                   | 3209                   | 3209                    | 0.96           | 4.7            | 240                     | 1.1            | 2.4              | 3.8              |                   | 1.74           | 500                     | 2054                                 | 1508                                 | 872        |
| 28.0                       | 7.55       | 14.2       |            | 7.4                     | 13.925                  |                         | 0                       | 121                   | 3382                   | 3382                    | 0.87           | 4.6            | 225                     | 1.1            | 2.3              | 3.7              |                   | 1.72           | 470                     | 2105                                 | 1554                                 | 807        |
| 29.0                       | 6.7        | 13.4       |            | 6.6                     | 13.125                  |                         | 0                       | 120                   | 3502                   | 3502                    | 0.99           | 3.9            | 227                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 474                     | 1792                                 | 1376                                 | 742        |
| 30.0                       | 5.85       | 12         | 0          | 5.8                     | 11.725                  |                         | 0                       | 119                   | 3621                   | 3621                    | 1.03           | 3.3            | 207                     | 0.9            | 1.7              | 2.2              |                   | 1.40           | 432                     | 1504                                 | 1204                                 | 606        |
| 31.0                       | 6.55       | 13.8       |            | 6.4                     | 13.525                  |                         | 0                       | 120                   | 3734                   | 3734                    | 1.11           | 3.6            | 247                     | 0.9            | 1.8              | 2.5              |                   | 1.48           | 516                     | 1704                                 | 1339                                 | 765        |
| 32.0                       | 6.9        | 14.6       |            | 6.7                     | 14.325                  |                         | 0                       | 121                   | 3855                   | 3855                    | 1.13           | 3.7            | 263                     | 0.9            | 1.9              | 2.6              |                   | 1.50           | 550                     | 1799                                 | 1407                                 | 826        |



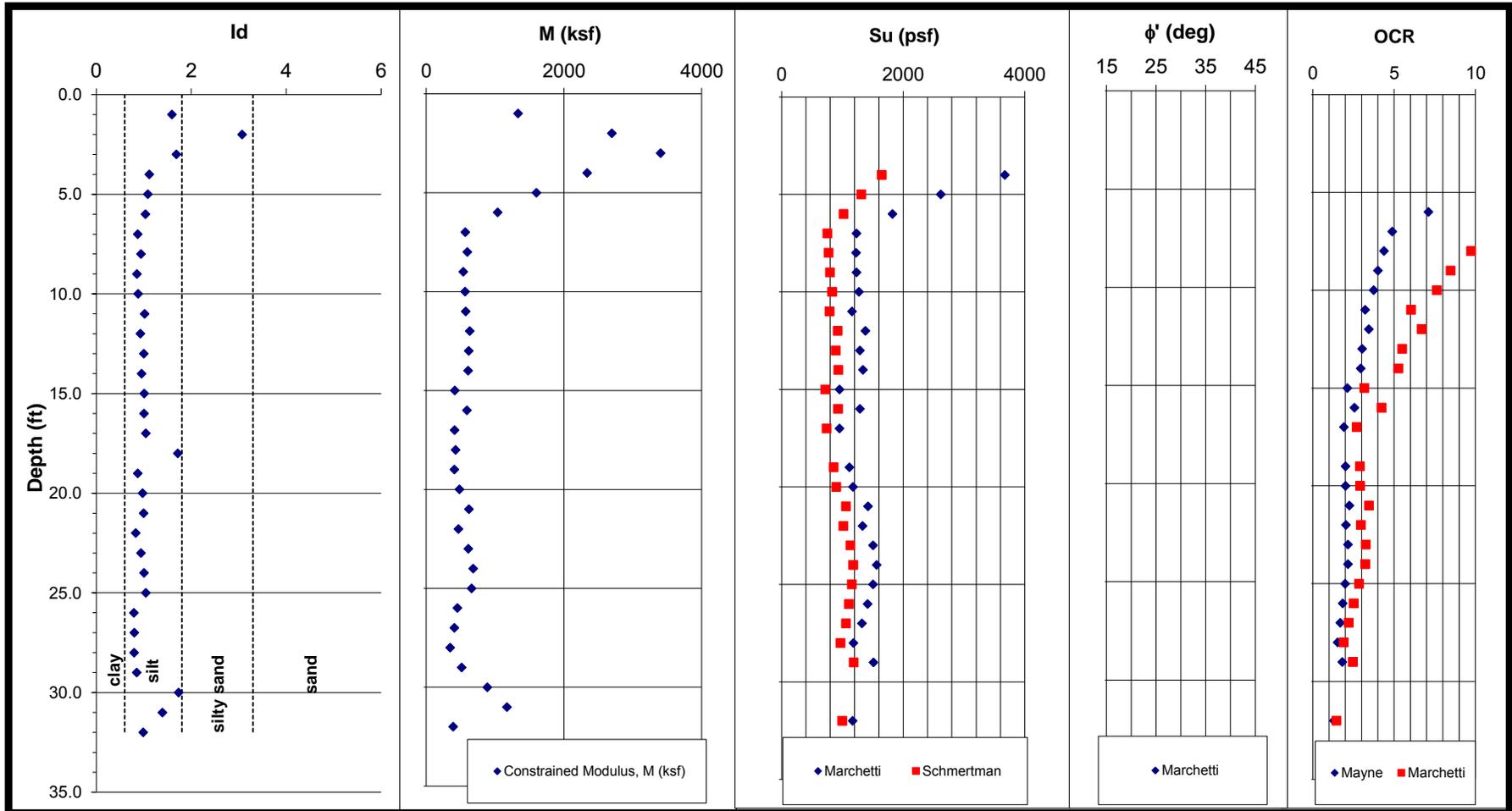
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





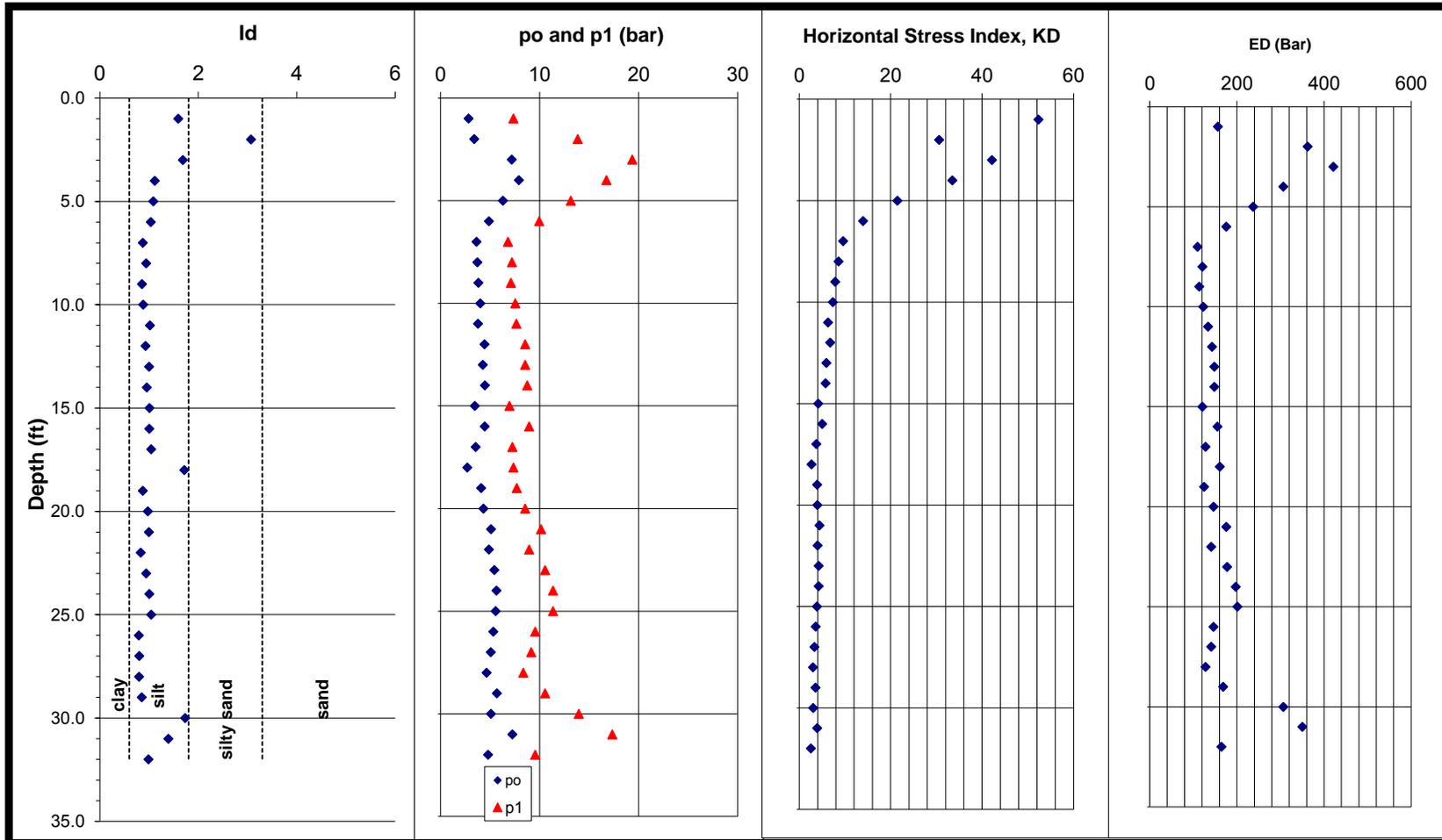
### DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI)  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR3\_EB1\_B2  
 Ground Water Depth (ft): N/A

Membrane 1    Membrane 2    Membrane 3  
 $\Delta A =$  0.25    0.175    0  
 $\Delta B =$  0.15    0.45    0  
 $Z_m =$  0    bar

Latitude: 36.15101  
 Longitude: -79.75339

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | po<br>(bar) | p1<br>(bar) | p2<br>(bar) | uo<br>(psf) | $\gamma_r^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | ld   | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>O</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------|-------------|-------------|-------------|-----------------------|------------------------|-------------------------|------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 2.8        | 7.5        |            | 2.8         | 7.35        |             | 0           | 113                   | 113                    | 113                     | 1.59 | 52.4           | 157                     |                |                  |                  |                   | 4.07           | 327                     |                                      |                                      | 1331       |
| 2.0                        | 3.65       | 14         |            | 3.4         | 13.85       |             | 0           | 119                   | 232                    | 232                     | 3.07 | 30.6           | 363                     |                |                  |                  | 45.1              | 3.56           | 757                     |                                      |                                      | 2695       |
| 3.0                        | 7.6        | 19.8       | 0          | 7.2         | 19.35       |             | 0           | 124                   | 356                    | 356                     | 1.69 | 42.2           | 422                     |                |                  |                  |                   | 3.86           | 881                     |                                      |                                      | 3402       |
| 4.0                        | 8.15       | 17.2       |            | 7.9         | 16.75       |             | 0           | 123                   | 492                    | 492                     | 1.12 | 33.5           | 307                     | 3.7            | 17.1             | 81.3             |                   | 3.65           | 641                     | 3674                                 | 1651                                 | 2337       |
| 5.0                        | 6.45       | 13.6       |            | 6.3         | 13.15       |             | 0           | 120                   | 612                    | 612                     | 1.09 | 21.5           | 238                     | 2.9            | 10.9             | 40.6             |                   | 3.22           | 497                     | 2620                                 | 1316                                 | 1601       |
| 6.0                        | 4.95       | 10.4       | 0          | 4.9         | 9.95        |             | 0           | 117                   | 729                    | 729                     | 1.04 | 14.0           | 176                     | 2.3            | 7.1              | 20.8             |                   | 2.82           | 367                     | 1825                                 | 1020                                 | 1035       |
| 7.0                        | 3.6        | 7.25       |            | 3.6         | 6.8         |             | 0           | 112                   | 787                    | 787                     | 0.88 | 9.6            | 110                     | 1.8            | 4.9              | 11.6             |                   | 2.46           | 230                     | 1233                                 | 757                                  | 566        |
| 8.0                        | 3.7        | 7.65       |            | 3.7         | 7.2         |             | 0           | 113                   | 900                    | 900                     | 0.94 | 8.6            | 121                     | 1.7            | 4.4              | 9.7              |                   | 2.35           | 253                     | 1227                                 | 775                                  | 594        |
| 9.0                        | 3.8        | 7.55       |            | 3.8         | 7.1         |             | 0           | 113                   | 1013                   | 1013                    | 0.86 | 7.9            | 114                     | 1.6            | 4.0              | 8.5              |                   | 2.26           | 238                     | 1236                                 | 798                                  | 537        |
| 10.0                       | 4          | 8          |            | 4.0         | 7.55        |             | 0           | 114                   | 1136                   | 1136                    | 0.88 | 7.4            | 123                     | 1.5            | 3.7              | 7.6              |                   | 2.19           | 257                     | 1275                                 | 837                                  | 563        |
| 11.0                       | 3.8        | 8.1        |            | 3.8         | 7.65        |             | 0           | 114                   | 1250                   | 1250                    | 1.02 | 6.3            | 134                     | 1.4            | 3.2              | 6.0              |                   | 2.04           | 280                     | 1162                                 | 792                                  | 572        |
| 12.0                       | 4.45       | 9          | 0          | 4.4         | 8.55        |             | 0           | 115                   | 1365                   | 1365                    | 0.93 | 6.8            | 143                     | 1.4            | 3.4              | 6.7              |                   | 2.11           | 299                     | 1380                                 | 925                                  | 630        |
| 13.0                       | 4.3        | 9          |            | 4.3         | 8.55        |             | 0           | 115                   | 1496                   | 1496                    | 1.00 | 6.0            | 148                     | 1.3            | 3.0              | 5.5              |                   | 1.98           | 310                     | 1289                                 | 892                                  | 615        |
| 14.0                       | 4.5        | 9.2        |            | 4.5         | 8.75        |             | 0           | 115                   | 1611                   | 1611                    | 0.96 | 5.8            | 148                     | 1.3            | 3.0              | 5.3              |                   | 1.95           | 310                     | 1340                                 | 934                                  | 606        |
| 15.0                       | 3.45       | 7.4        | 0          | 3.5         | 6.95        |             | 0           | 113                   | 1724                   | 1724                    | 1.01 | 4.2            | 121                     | 1.0            | 2.1              | 3.2              |                   | 1.63           | 253                     | 956                                  | 722                                  | 413        |
| 16.0                       | 4.5        | 9.4        |            | 4.5         | 8.95        |             | 0           | 116                   | 1850                   | 1850                    | 1.01 | 5.0            | 156                     | 1.2            | 2.6              | 4.2              |                   | 1.82           | 325                     | 1291                                 | 932                                  | 591        |
| 17.0                       | 3.55       | 7.7        |            | 3.5         | 7.25        |             | 0           | 113                   | 1963                   | 1963                    | 1.04 | 3.8            | 128                     | 0.9            | 1.9              | 2.7              |                   | 1.53           | 268                     | 956                                  | 741                                  | 410        |
| 18.0                       | 2.75       | 7.8        | 0          | 2.7         | 7.35        |             | 0           | 113                   | 2076                   | 2076                    | 1.72 | 2.7            | 161                     |                |                  |                  |                   | 1.26           | 337                     |                                      |                                      | 424        |
| 19.0                       | 4.1        | 8.15       |            | 4.1         | 7.7         |             | 0           | 114                   | 2163                   | 2163                    | 0.88 | 4.0            | 125                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 261                     | 1119                                 | 857                                  | 409        |
| 20.0                       | 4.35       | 9          |            | 4.3         | 8.55        |             | 0           | 115                   | 2278                   | 2278                    | 0.98 | 4.0            | 147                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 306                     | 1179                                 | 903                                  | 482        |
| 21.0                       | 5.15       | 10.6       | 0.1        | 5.1         | 10.15       | 0.35        | 0           | 117                   | 2395                   | 2395                    | 1.00 | 4.4            | 176                     | 1.1            | 2.3              | 3.5              |                   | 1.69           | 367                     | 1425                                 | 1062                                 | 619        |
| 22.0                       | 4.9        | 9.4        |            | 4.9         | 8.95        |             | 0           | 116                   | 2542                   | 2542                    | 0.83 | 4.0            | 141                     | 1.0            | 2.0              | 3.0              |                   | 1.58           | 295                     | 1334                                 | 1019                                 | 465        |
| 23.0                       | 5.5        | 11         |            | 5.4         | 10.55       |             | 0           | 118                   | 2660                   | 2660                    | 0.94 | 4.3            | 178                     | 1.0            | 2.2              | 3.3              |                   | 1.65           | 371                     | 1508                                 | 1134                                 | 610        |
| 24.0                       | 5.75       | 11.8       | 0          | 5.7         | 11.35       |             | 0           | 118                   | 2778                   | 2778                    | 1.01 | 4.3            | 198                     | 1.0            | 2.2              | 3.2              |                   | 1.65           | 413                     | 1568                                 | 1181                                 | 679        |
| 25.0                       | 5.65       | 11.8       |            | 5.5         | 11.35       |             | 0           | 118                   | 2959                   | 2959                    | 1.05 | 3.9            | 201                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 420                     | 1508                                 | 1159                                 | 659        |
| 26.0                       | 5.35       | 10         |            | 5.3         | 9.55        |             | 0           | 116                   | 3076                   | 3076                    | 0.79 | 3.6            | 147                     | 0.9            | 1.8              | 2.5              |                   | 1.47           | 306                     | 1418                                 | 1112                                 | 450        |
| 27.0                       | 5.1        | 9.6        | 0.15       | 5.1         | 9.15        | 0.40        | 0           | 116                   | 3191                   | 3191                    | 0.80 | 3.3            | 141                     | 0.9            | 1.7              | 2.2              |                   | 1.39           | 295                     | 1326                                 | 1061                                 | 409        |
| 28.0                       | 4.65       | 8.8        |            | 4.6         | 8.35        |             | 0           | 115                   | 3212                   | 3212                    | 0.80 | 3.0            | 128                     | 0.8            | 1.5              | 1.9              |                   | 1.29           | 268                     | 1184                                 | 971                                  | 346        |
| 29.0                       | 5.75       | 11         |            | 5.7         | 10.55       |             | 0           | 117                   | 3330                   | 3330                    | 0.85 | 3.6            | 169                     | 0.9            | 1.8              | 2.5              |                   | 1.46           | 352                     | 1512                                 | 1189                                 | 514        |
| 30.0                       | 5.35       | 14.4       | 1.35       | 5.1         | 13.95       | 1.60        | 0           | 120                   | 3450                   | 3450                    | 1.73 | 3.1            | 307                     |                |                  |                  |                   | 1.38           | 641                     |                                      |                                      | 887        |
| 31.0                       | 7.55       | 17.8       |            | 7.2         | 17.35       |             | 0           | 123                   | 3824                   | 3824                    | 1.40 | 4.0            | 351                     |                |                  |                  |                   | 1.60           | 732                     |                                      |                                      | 1170       |
| 32.0                       | 4.85       | 10         |            | 4.8         | 9.55        |             | 0           | 116                   | 3940                   | 3940                    | 0.99 | 2.5            | 165                     | 0.7            | 1.3              | 1.5              |                   | 1.13           | 344                     | 1171                                 | 1002                                 | 390        |



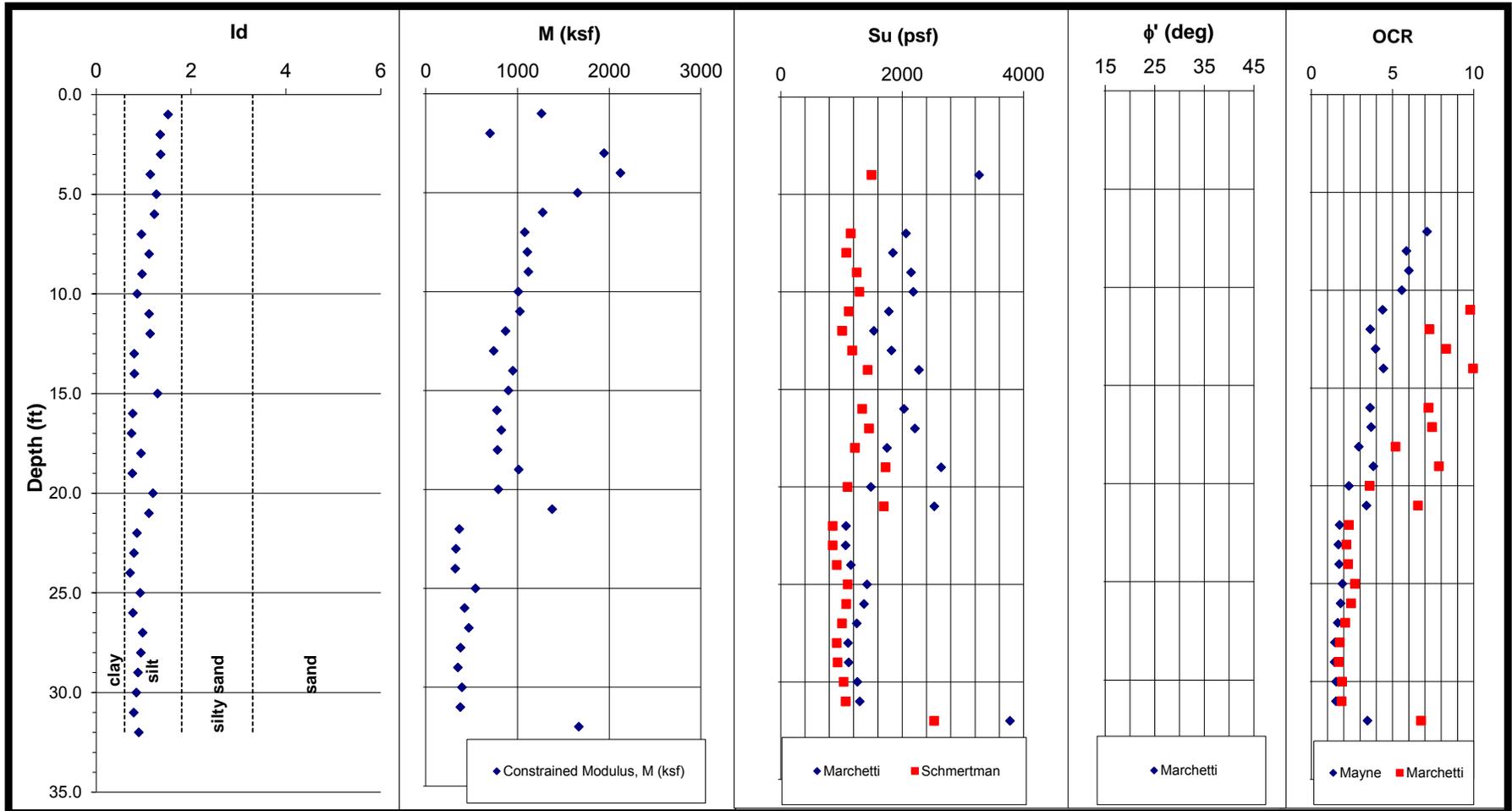
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





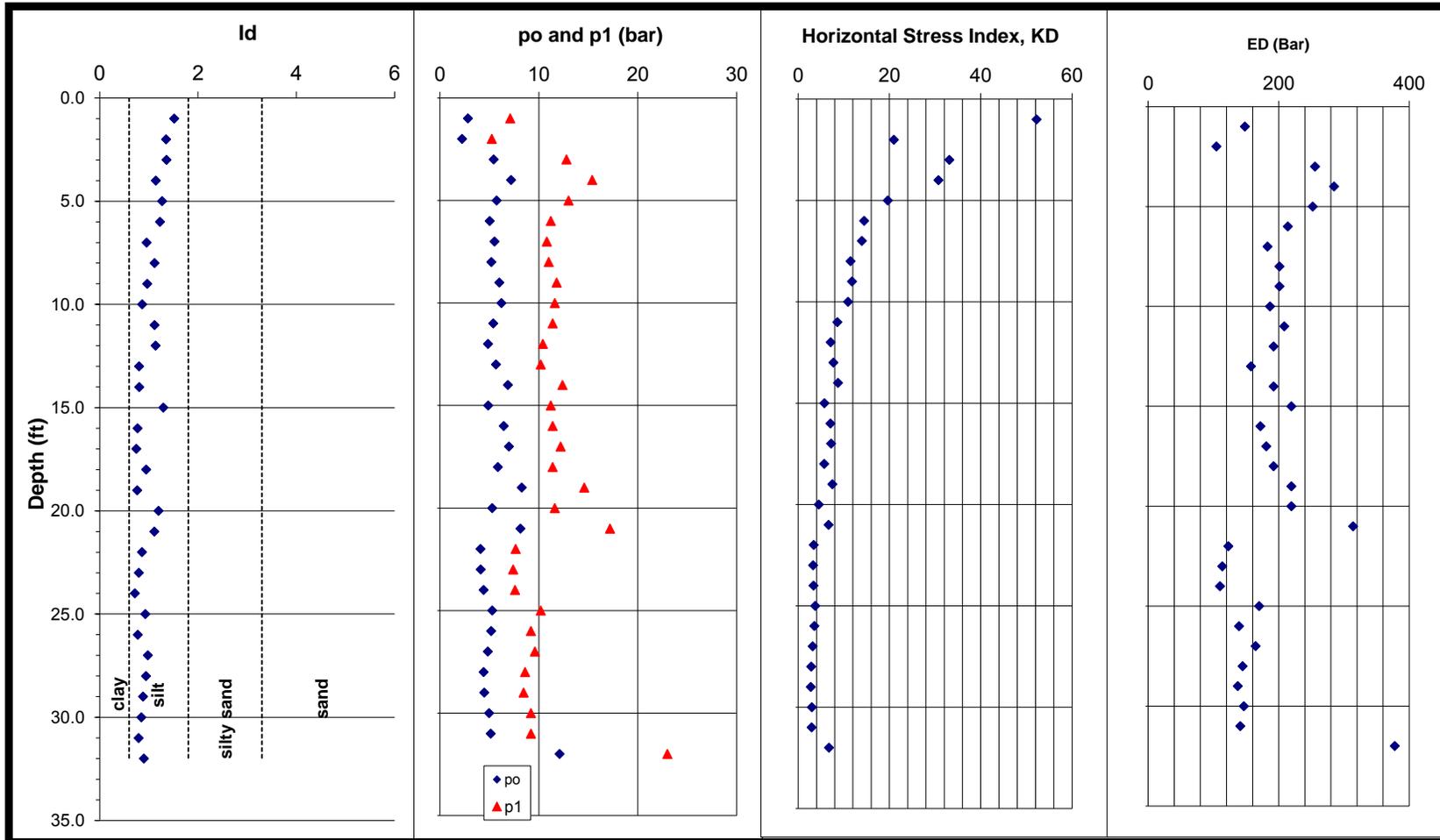
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB1\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR3\_EB1\_B3  
 Ground Water Depth (ft): N/A

Membrane 1    Membrane 2    Membrane 3  
 $\Delta A =$  0.225    0    0  
 $\Delta B =$  0.2    0    0  
 $Z_m =$  0    bar

Northing 874701  
 Easting 1777579

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



**DILATOMETER TEST RESULTS**

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | po<br>(bar) | p1<br>(bar) | p2<br>(bar) | uo<br>(psf) | $\gamma_r^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}^1$<br>(psf) | ld   | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------|-------------|-------------|-------------|-----------------------|------------------------|--------------------------|------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 2.8        | 7.3        |            | 2.8         | 7.1         |             | 0           | 113                   | 113                    | 113                      | 1.52 | 52.3           | 148                     |                |                  |                  |                   | 4.07           | 310                     |                                      |                                      | 1261       |
| 2.0                        | 2.15       | 5.45       |            | 2.2         | 5.25        |             | 0           | 109                   | 222                    | 222                      | 1.35 | 21.0           | 105                     |                |                  |                  |                   | 3.20           | 219                     |                                      |                                      | 700        |
| 3.0                        | 5.55       | 13         | 0          | 5.4         | 12.8        |             | 0           | 120                   | 342                    | 342                      | 1.36 | 33.1           | 256                     |                |                  |                  |                   | 3.63           | 535                     |                                      |                                      | 1943       |
| 4.0                        | 7.35       | 15.6       |            | 7.2         | 15.4        |             | 0           | 122                   | 488                    | 488                      | 1.14 | 30.7           | 285                     | 3.5            | 15.6             | 71.0             |                   | 3.56           | 595                     | 3268                                 | 1500                                 | 2122       |
| 5.0                        | 5.85       | 13.2       |            | 5.7         | 13          |             | 0           | 120                   | 608                    | 608                      | 1.27 | 19.7           | 252                     |                |                  |                  |                   | 3.14           | 527                     |                                      |                                      | 1655       |
| 6.0                        | 5.1        | 11.4       | 0          | 5.0         | 11.2        |             | 0           | 118                   | 726                    | 726                      | 1.23 | 14.5           | 214                     |                |                  |                  |                   | 2.85           | 447                     |                                      |                                      | 1274       |
| 7.0                        | 5.55       | 11         |            | 5.5         | 10.8        |             | 0           | 118                   | 825                    | 825                      | 0.96 | 14.0           | 183                     | 2.3            | 7.1              | 20.8             |                   | 2.82           | 382                     | 2064                                 | 1154                                 | 1078       |
| 8.0                        | 5.25       | 11.2       |            | 5.2         | 11          |             | 0           | 118                   | 943                    | 943                      | 1.12 | 11.5           | 201                     | 2.0            | 5.9              | 15.4             |                   | 2.63           | 420                     | 1850                                 | 1086                                 | 1107       |
| 9.0                        | 6.05       | 12         | 0          | 6.0         | 11.8        |             | 0           | 119                   | 1061                   | 1061                     | 0.97 | 11.8           | 201                     | 2.0            | 6.0              | 16.0             |                   | 2.66           | 420                     | 2148                                 | 1253                                 | 1117       |
| 10.0                       | 6.25       | 11.8       |            | 6.2         | 11.6        |             | 0           | 119                   | 1186                   | 1186                     | 0.87 | 11.0           | 187                     | 1.9            | 5.6              | 14.2             |                   | 2.59           | 390                     | 2185                                 | 1299                                 | 1009       |
| 11.0                       | 5.45       | 11.6       |            | 5.4         | 11.4        |             | 0           | 118                   | 1304                   | 1304                     | 1.12 | 8.6            | 209                     | 1.7            | 4.4              | 9.8              |                   | 2.35           | 436                     | 1784                                 | 1125                                 | 1025       |
| 12.0                       | 4.9        | 10.6       | 0          | 4.9         | 10.4        |             | 0           | 117                   | 1422                   | 1422                     | 1.14 | 7.1            | 192                     | 1.5            | 3.6              | 7.3              |                   | 2.17           | 401                     | 1535                                 | 1015                                 | 870        |
| 13.0                       | 5.65       | 10.4       |            | 5.7         | 10.2        |             | 0           | 117                   | 1522                   | 1522                     | 0.80 | 7.8            | 158                     | 1.6            | 4.0              | 8.3              |                   | 2.24           | 329                     | 1825                                 | 1182                                 | 739        |
| 14.0                       | 6.9        | 12.6       |            | 6.9         | 12.4        |             | 0           | 119                   | 1641                   | 1641                     | 0.81 | 8.7            | 192                     | 1.7            | 4.4              | 10.0             |                   | 2.36           | 401                     | 2279                                 | 1433                                 | 948        |
| 15.0                       | 4.95       | 11.4       | 0          | 4.9         | 11.2        |             | 0           | 118                   | 1759                   | 1759                     | 1.30 | 5.8            | 220                     |                |                  |                  |                   | 1.96           | 458                     |                                      |                                      | 901        |
| 16.0                       | 6.45       | 11.6       |            | 6.4         | 11.4        |             | 0           | 118                   | 1893                   | 1893                     | 0.77 | 7.1            | 172                     | 1.5            | 3.6              | 7.2              |                   | 2.15           | 360                     | 2031                                 | 1345                                 | 774        |
| 17.0                       | 7          | 12.4       |            | 7.0         | 12.2        |             | 0           | 119                   | 2012                   | 2012                     | 0.75 | 7.2            | 181                     | 1.5            | 3.7              | 7.4              |                   | 2.17           | 379                     | 2211                                 | 1457                                 | 822        |
| 18.0                       | 5.9        | 11.6       | 0.15       | 5.9         | 11.4        | 0.38        | 0           | 118                   | 2131                   | 2131                     | 0.94 | 5.7            | 192                     | 1.3            | 2.9              | 5.2              |                   | 1.94           | 401                     | 1753                                 | 1224                                 | 780        |
| 19.0                       | 8.35       | 14.8       |            | 8.3         | 14.6        |             | 0           | 121                   | 2304                   | 2304                     | 0.76 | 7.5            | 220                     | 1.5            | 3.8              | 7.9              |                   | 2.21           | 458                     | 2645                                 | 1728                                 | 1012       |
| 20.0                       | 5.35       | 11.8       |            | 5.3         | 11.6        |             | 0           | 119                   | 2423                   | 2423                     | 1.20 | 4.5            | 220                     | 1.1            | 2.3              | 3.6              |                   | 1.72           | 458                     | 1488                                 | 1101                                 | 790        |
| 21.0                       | 8.35       | 17.4       | 0.2        | 8.1         | 17.2        | 0.43        | 0           | 123                   | 2546                   | 2546                     | 1.11 | 6.7            | 314                     | 1.4            | 3.4              | 6.6              |                   | 2.10           | 656                     | 2529                                 | 1701                                 | 1378       |
| 22.0                       | 4.05       | 7.85       |            | 4.1         | 7.65        |             | 0           | 114                   | 2503                   | 2503                     | 0.86 | 3.4            | 123                     | 0.9            | 1.7              | 2.3              |                   | 1.42           | 257                     | 1079                                 | 858                                  | 365        |
| 23.0                       | 4.05       | 7.6        |            | 4.1         | 7.4         |             | 0           | 113                   | 2616                   | 2616                     | 0.80 | 3.3            | 114                     | 0.8            | 1.7              | 2.2              |                   | 1.37           | 238                     | 1071                                 | 860                                  | 327        |
| 24.0                       | 4.35       | 7.8        | 0.05       | 4.4         | 7.6         | 0.28        | 0           | 114                   | 2730                   | 2730                     | 0.72 | 3.4            | 110                     | 0.9            | 1.7              | 2.3              |                   | 1.40           | 230                     | 1159                                 | 924                                  | 322        |
| 25.0                       | 5.3        | 10.4       |            | 5.3         | 10.2        |             | 0           | 117                   | 2928                   | 2928                     | 0.93 | 3.8            | 170                     | 0.9            | 1.9              | 2.7              |                   | 1.52           | 356                     | 1425                                 | 1105                                 | 542        |
| 26.0                       | 5.15       | 9.4        |            | 5.2         | 9.2         |             | 0           | 116                   | 3044                   | 3044                     | 0.77 | 3.6            | 139                     | 0.9            | 1.8              | 2.5              |                   | 1.45           | 291                     | 1375                                 | 1083                                 | 423        |
| 27.0                       | 4.85       | 9.8        | 0          | 4.8         | 9.6         |             | 0           | 116                   | 3160                   | 3160                     | 0.98 | 3.2            | 165                     | 0.8            | 1.6              | 2.1              |                   | 1.36           | 344                     | 1253                                 | 1013                                 | 469        |
| 28.0                       | 4.4        | 8.8        |            | 4.4         | 8.6         |             | 0           | 115                   | 3224                   | 3224                     | 0.94 | 2.9            | 145                     | 0.8            | 1.5              | 1.8              |                   | 1.25           | 302                     | 1113                                 | 924                                  | 377        |
| 29.0                       | 4.45       | 8.65       |            | 4.5         | 8.45        |             | 0           | 115                   | 3339                   | 3339                     | 0.88 | 2.8            | 138                     | 0.7            | 1.4              | 1.7              |                   | 1.22           | 287                     | 1122                                 | 937                                  | 351        |
| 30.0                       | 4.95       | 9.4        | 0.55       | 5.0         | 9.2         | 0.78        | 0           | 116                   | 3455                   | 3455                     | 0.85 | 3.0            | 147                     | 0.8            | 1.5              | 1.9              |                   | 1.29           | 306                     | 1265                                 | 1039                                 | 394        |
| 31.0                       | 5.1        | 9.4        |            | 5.1         | 9.2         |             | 0           | 116                   | 3591                   | 3591                     | 0.79 | 3.0            | 141                     | 0.8            | 1.5              | 1.9              |                   | 1.28           | 295                     | 1303                                 | 1072                                 | 376        |
| 32.0                       | 12.4       | 23.2       |            | 12.1        | 23          |             | 0           | 127                   | 3718                   | 3718                     | 0.90 | 6.8            | 378                     | 1.4            | 3.5              | 6.7              |                   | 2.11           | 789                     | 3777                                 | 2528                                 | 1668       |



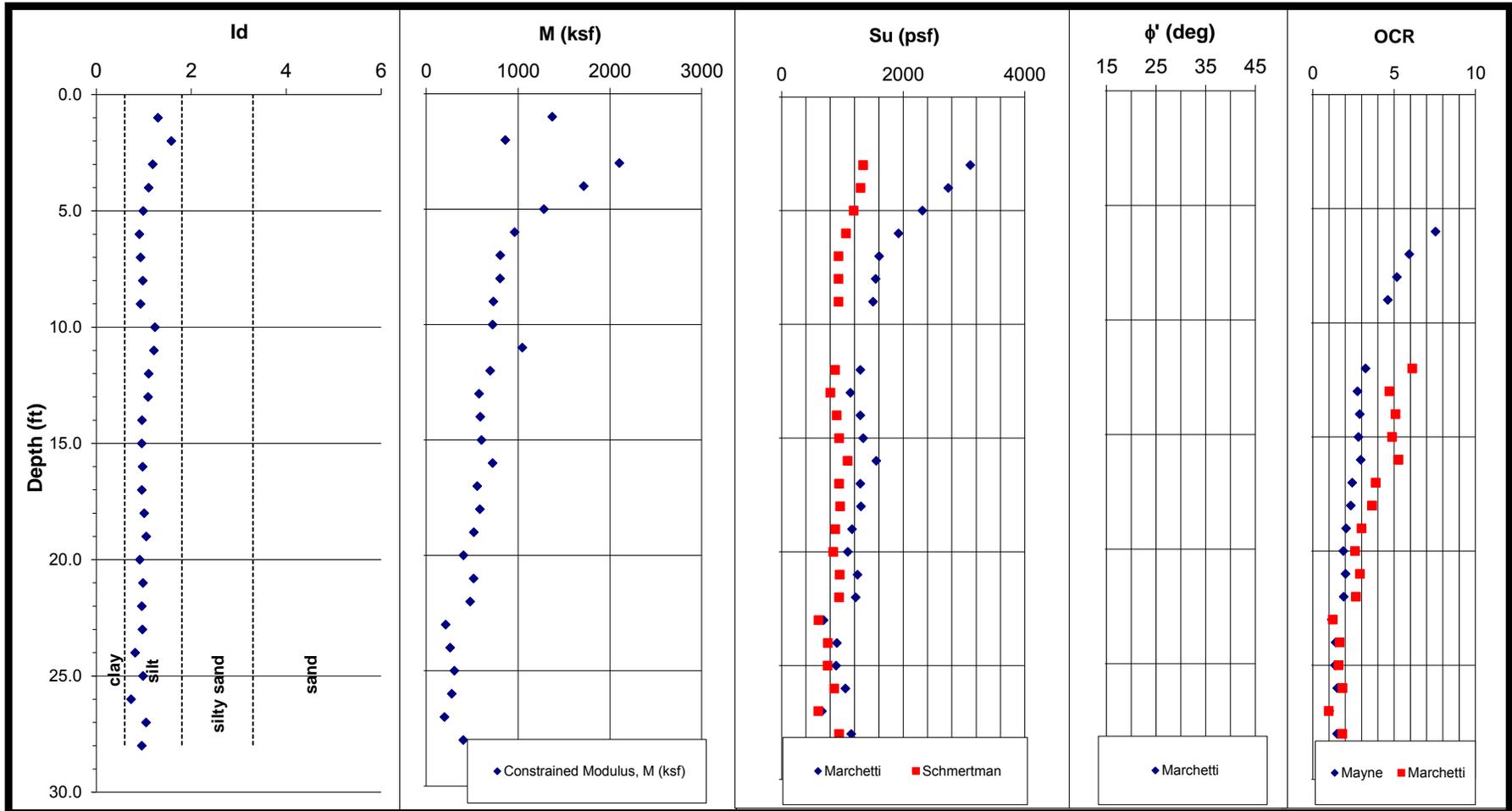
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





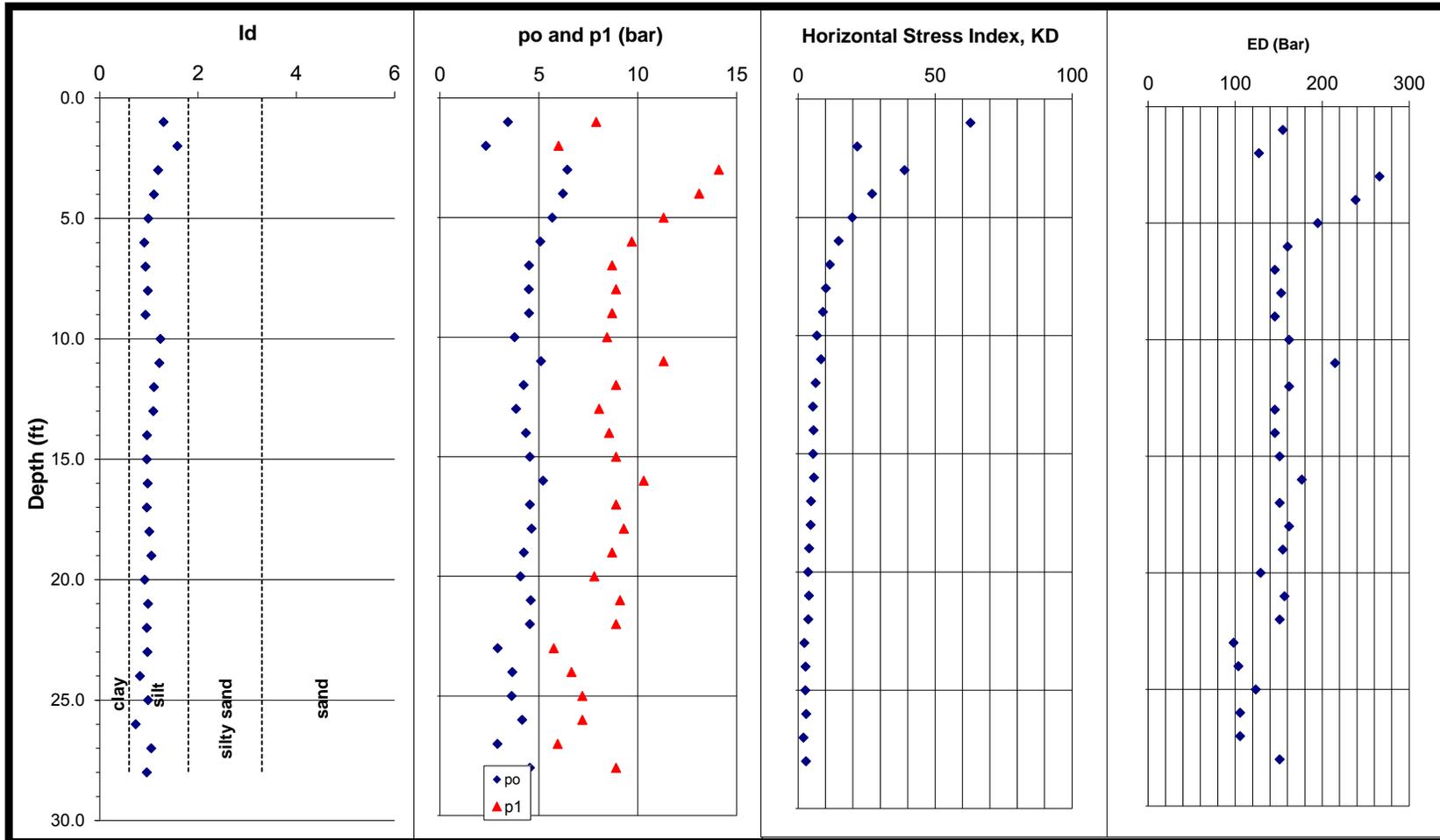
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B1

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 AND  
 Job Location: Greensboro, NC  
 Date: 12-21-16  
 Sounding No: STR3\_EB2\_B1  
 Ground Water Depth (ft): N/A

|              |                   |                   |                   |
|--------------|-------------------|-------------------|-------------------|
|              | <b>Membrane 1</b> | <b>Membrane 2</b> | <b>Membrane 3</b> |
| $\Delta A =$ | 0.2               | 0                 | 0                 |
| $\Delta B =$ | 0.3               | 0                 | 0                 |
| $Z_m =$      | 0                 | bar               |                   |

Northing 874672  
 Easting 1777462

- <sup>1</sup> Depth Below Existing Ground Surface
- <sup>2</sup> Mayne, 1995
- <sup>3</sup> Marchetti, 2001
- <sup>4</sup> Schmertman, 1991
- <sup>5</sup> Mayne, 2002



### DILATOMETER TEST RESULTS

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_T^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>s</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 3.45       | 8.2        |            | 3.4                     | 7.9                     |                         | 0                       | 114                   | 114                    | 114                     | 1.30           | 62.9           | 155                     |                |                  |                  |                   | 4.24           | 323                     |                                      |                                      | 1372       |
| 2.0                        | 2.3        | 6.3        |            | 2.3                     | 6                       |                         | 0                       | 111                   | 225                    | 225                     | 1.58           | 21.6           | 128                     |                |                  |                  |                   | 3.23           | 266                     |                                      |                                      | 860        |
| 3.0                        | 6.6        | 14.4       |            | 6.4                     | 14.1                    |                         | 0                       | 121                   | 346                    | 346                     | 1.19           | 38.9           | 266                     | 4.0            | 19.8             | 102.4            |                   | 3.79           | 556                     | 3104                                 | 1344                                 | 2103       |
| 4.0                        | 6.35       | 13.4       |            | 6.2                     | 13.1                    |                         | 0                       | 120                   | 480                    | 480                     | 1.11           | 27.1           | 239                     | 3.3            | 13.8             | 58.2             |                   | 3.44           | 498                     | 2742                                 | 1300                                 | 1716       |
| 5.0                        | 5.75       | 11.6       |            | 5.7                     | 11.3                    |                         | 0                       | 118                   | 599                    | 599                     | 0.99           | 19.8           | 195                     | 2.8            | 10.1             | 35.8             |                   | 3.15           | 407                     | 2316                                 | 1187                                 | 1282       |
| 6.0                        | 5.1        | 10         | 0          | 5.1                     | 9.7                     |                         | 0                       | 117                   | 715                    | 715                     | 0.91           | 14.8           | 160                     | 2.3            | 7.6              | 22.8             |                   | 2.87           | 335                     | 1926                                 | 1061                                 | 962        |
| 7.0                        | 4.5        | 9          |            | 4.5                     | 8.7                     |                         | 0                       | 115                   | 807                    | 807                     | 0.93           | 11.6           | 146                     | 2.0            | 5.9              | 15.6             |                   | 2.64           | 304                     | 1606                                 | 940                                  | 805        |
| 8.0                        | 4.5        | 9.2        |            | 4.5                     | 8.9                     |                         | 0                       | 116                   | 922                    | 922                     | 0.98           | 10.2           | 153                     | 1.9            | 5.2              | 12.6             |                   | 2.52           | 320                     | 1549                                 | 938                                  | 804        |
| 9.0                        | 4.5        | 9          | 0          | 4.5                     | 8.7                     |                         | 0                       | 115                   | 1038                   | 1038                    | 0.93           | 9.1            | 146                     | 1.7            | 4.6              | 10.6             |                   | 2.40           | 304                     | 1508                                 | 940                                  | 731        |
| 10.0                       | 3.8        | 8.75       |            | 3.8                     | 8.45                    |                         | 0                       | 115                   | 1149                   | 1149                    | 1.24           | 6.9            | 162                     |                |                  |                  |                   | 2.13           | 339                     |                                      |                                      | 721        |
| 11.0                       | 5.2        | 11.6       |            | 5.1                     | 11.3                    |                         | 0                       | 118                   | 1267                   | 1267                    | 1.21           | 8.4            | 215                     |                |                  |                  |                   | 2.33           | 449                     |                                      |                                      | 1046       |
| 12.0                       | 4.25       | 9.2        | 0          | 4.2                     | 8.9                     |                         | 0                       | 116                   | 1383                   | 1383                    | 1.11           | 6.4            | 162                     | 1.4            | 3.3              | 6.1              |                   | 2.06           | 339                     | 1298                                 | 883                                  | 696        |
| 13.0                       | 3.85       | 8.35       |            | 3.9                     | 8.05                    |                         | 0                       | 114                   | 1487                   | 1487                    | 1.09           | 5.4            | 146                     | 1.2            | 2.8              | 4.7              |                   | 1.89           | 304                     | 1134                                 | 804                                  | 575        |
| 14.0                       | 4.35       | 8.85       |            | 4.4                     | 8.55                    |                         | 0                       | 115                   | 1602                   | 1602                    | 0.97           | 5.7            | 146                     | 1.3            | 2.9              | 5.1              |                   | 1.93           | 304                     | 1297                                 | 909                                  | 588        |
| 15.0                       | 4.55       | 9.2        | 0          | 4.5                     | 8.9                     |                         | 0                       | 116                   | 1717                   | 1717                    | 0.96           | 5.5            | 151                     | 1.2            | 2.8              | 4.9              |                   | 1.91           | 316                     | 1345                                 | 949                                  | 602        |
| 16.0                       | 5.25       | 10.6       |            | 5.2                     | 10.3                    |                         | 0                       | 117                   | 1876                   | 1876                    | 0.98           | 5.8            | 177                     | 1.3            | 3.0              | 5.3              |                   | 1.95           | 369                     | 1561                                 | 1088                                 | 721        |
| 17.0                       | 4.55       | 9.2        |            | 4.5                     | 8.9                     |                         | 0                       | 116                   | 1991                   | 1991                    | 0.96           | 4.8            | 151                     | 1.1            | 2.4              | 3.9              |                   | 1.76           | 316                     | 1297                                 | 949                                  | 555        |
| 18.0                       | 4.65       | 9.6        | 0          | 4.6                     | 9.3                     |                         | 0                       | 116                   | 2107                   | 2107                    | 1.01           | 4.6            | 162                     | 1.1            | 2.3              | 3.6              |                   | 1.72           | 339                     | 1308                                 | 966                                  | 583        |
| 19.0                       | 4.25       | 9          |            | 4.2                     | 8.7                     |                         | 0                       | 115                   | 2190                   | 2190                    | 1.05           | 4.0            | 155                     | 1.0            | 2.1              | 3.0              |                   | 1.60           | 323                     | 1161                                 | 885                                  | 517        |
| 20.0                       | 4.05       | 8.1        |            | 4.1                     | 7.8                     |                         | 0                       | 114                   | 2304                   | 2304                    | 0.92           | 3.7            | 129                     | 0.9            | 1.9              | 2.6              |                   | 1.50           | 270                     | 1091                                 | 851                                  | 405        |
| 21.0                       | 4.6        | 9.4        | 0          | 4.6                     | 9.1                     |                         | 0                       | 116                   | 2420                   | 2420                    | 0.98           | 4.0            | 157                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 327                     | 1249                                 | 958                                  | 515        |
| 22.0                       | 4.55       | 9.2        |            | 4.5                     | 8.9                     |                         | 0                       | 116                   | 2542                   | 2542                    | 0.96           | 3.7            | 151                     | 0.9            | 1.9              | 2.6              |                   | 1.51           | 316                     | 1220                                 | 949                                  | 478        |
| 23.0                       | 2.85       | 6.05       |            | 2.9                     | 5.75                    |                         | 0                       | 111                   | 2652                   | 2652                    | 0.97           | 2.3            | 98                      | 0.6            | 1.2              | 1.2              |                   | 1.03           | 205                     | 693                                  | 609                                  | 211        |
| 24.0                       | 3.6        | 6.95       | 0          | 3.7                     | 6.65                    |                         | 0                       | 112                   | 2764                   | 2764                    | 0.82           | 2.8            | 104                     | 0.7            | 1.4              | 1.7              |                   | 1.20           | 217                     | 911                                  | 764                                  | 260        |
| 25.0                       | 3.6        | 7.5        |            | 3.6                     | 7.2                     |                         | 0                       | 113                   | 2828                   | 2828                    | 0.98           | 2.7            | 124                     | 0.7            | 1.4              | 1.6              |                   | 1.18           | 259                     | 897                                  | 758                                  | 306        |
| 26.0                       | 4.1        | 7.5        |            | 4.2                     | 7.2                     |                         | 0                       | 113                   | 2941                   | 2941                    | 0.73           | 3.0            | 106                     | 0.8            | 1.5              | 1.8              |                   | 1.26           | 221                     | 1052                                 | 868                                  | 278        |
| 27.0                       | 2.85       | 6.25       | 0          | 2.9                     | 5.95                    |                         | 0                       | 111                   | 3052                   | 3052                    | 1.05           | 2.0            | 106                     | 0.5            | 1.0              | 1.0              |                   | 0.89           | 221                     | 666                                  | 607                                  | 197        |
| 28.0                       | 4.55       | 9.2        |            | 4.5                     | 8.9                     |                         | 0                       | 116                   | 3235                   | 3235                    | 0.96           | 2.9            | 151                     | 0.8            | 1.5              | 1.8              |                   | 1.27           | 316                     | 1148                                 | 949                                  | 402        |



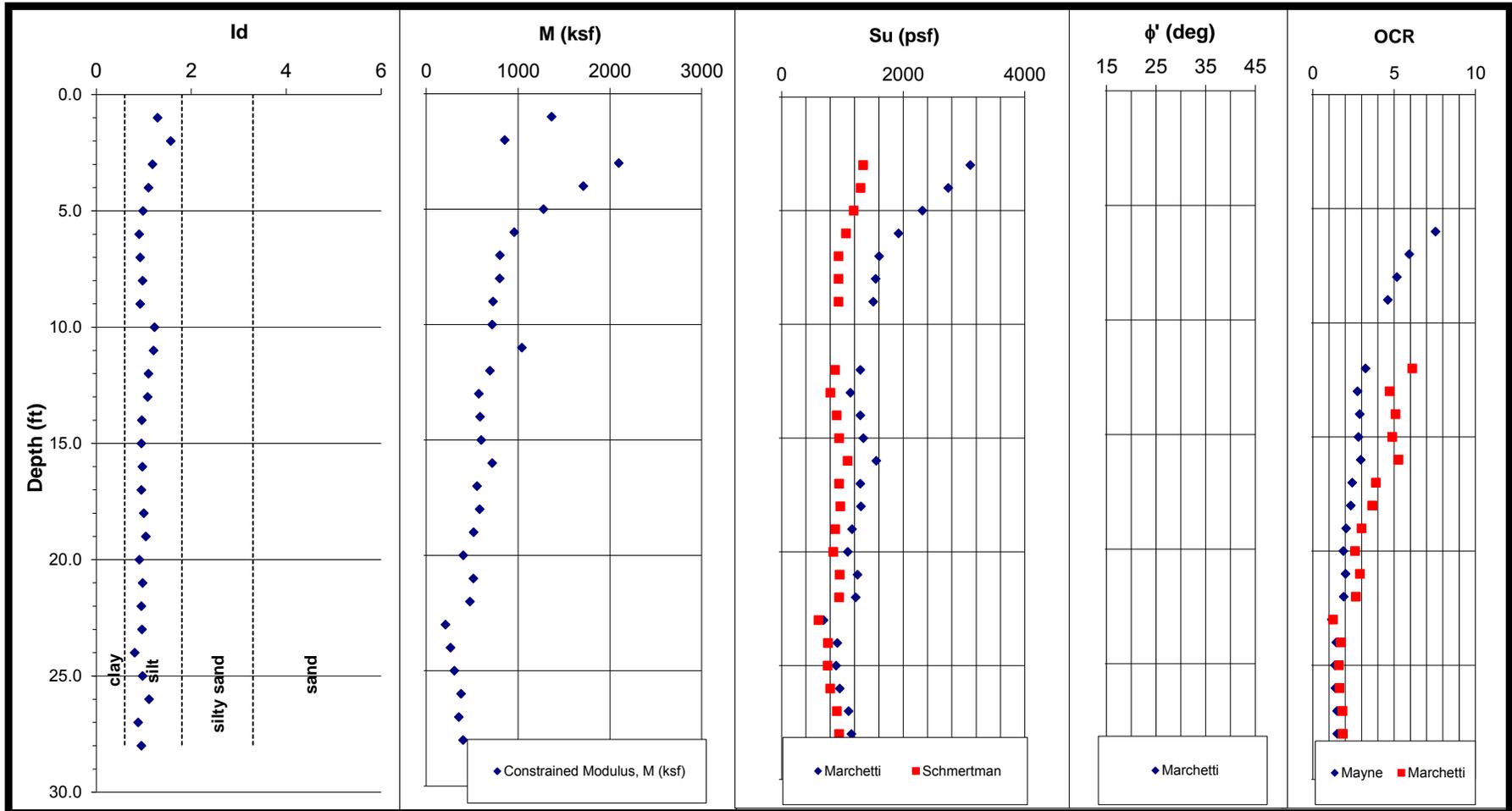
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B2

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

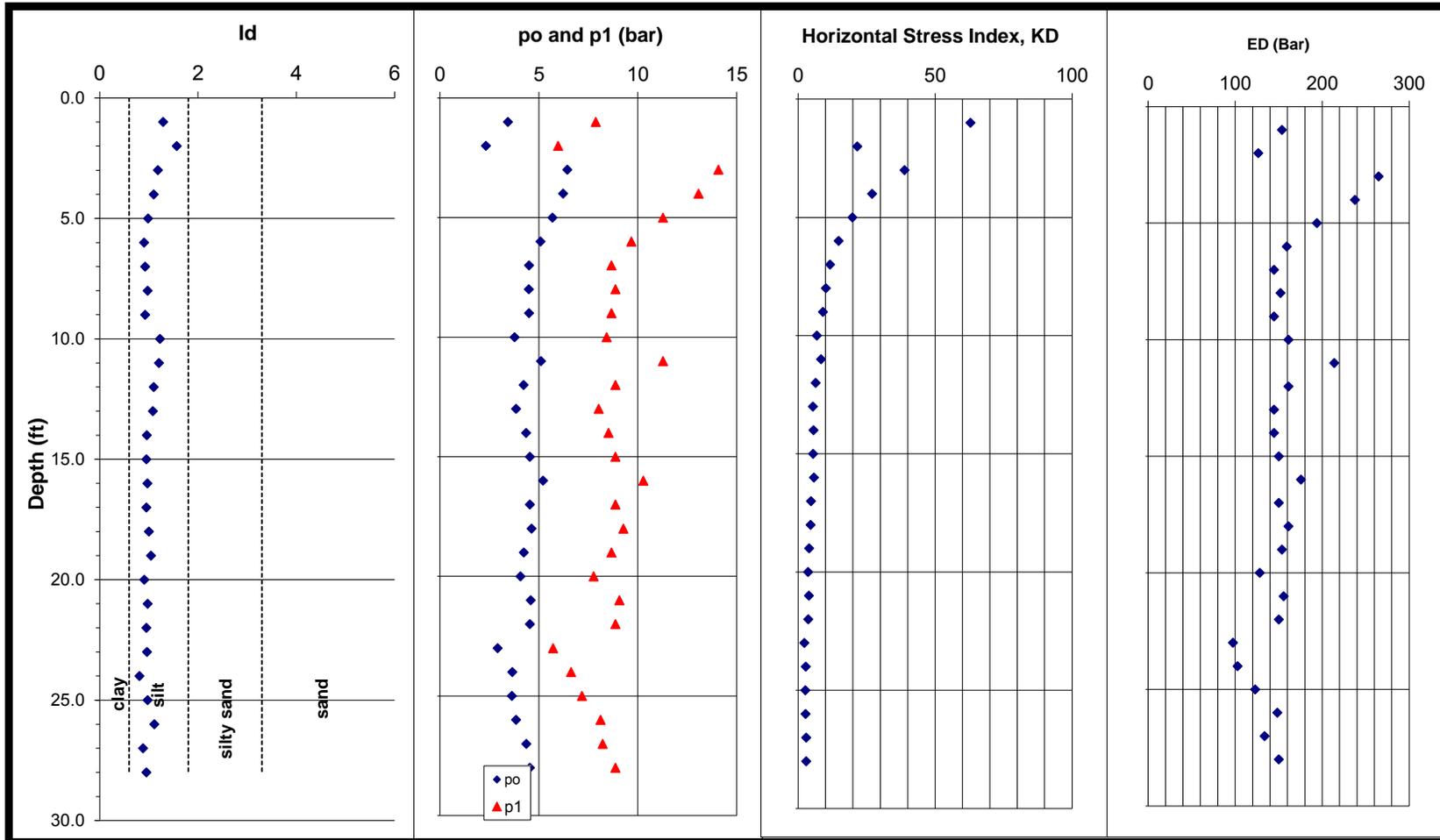
Project No.: 16-54112





### DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B2  
Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)  
Location: Greensboro, NC  
Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 AND  
 Job Location: Greensboro, NC  
 Date: 12-20-16  
 Sounding No: STR3\_EB2\_B2  
 Ground Water Depth (ft): N/A

|              | Membrane 1 | Membrane 2 | Membrane 3 |
|--------------|------------|------------|------------|
| $\Delta A =$ | 0.2        | 0          | 0          |
| $\Delta B =$ | 0.325      | 0          | 0          |
| Zm=          | 0          | bar        |            |

Northing 874736  
 Easting 1777468

- <sup>1</sup> Depth Below Existing Ground Surface
- <sup>2</sup> Mayne, 1995
- <sup>3</sup> Marchetti, 2001
- <sup>4</sup> Schmertman, 1991
- <sup>5</sup> Mayne, 2002



### DILATOMETER TEST RESULTS

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | $\gamma_1^5$<br>(pcf) | $\sigma_{vo}$<br>(psf) | $\sigma_{vo}'$<br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>b</sup> | $\phi^3$<br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|------------------------|-------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 3.45       | 8.2        |            | 3.4                     | 7.875                   |                         | 0                       | 114                   | 114                    | 114                     | 1.29           | 63.0           | 154                     |                |                  |                  |                   | 4.24           | 322                     |                                      |                                      | 1364       |
| 2.0                        | 2.3        | 6.3        |            | 2.3                     | 5.975                   |                         | 0                       | 111                   | 225                    | 225                     | 1.57           | 21.6           | 127                     |                |                  |                  |                   | 3.23           | 264                     |                                      |                                      | 854        |
| 3.0                        | 6.6        | 14.4       |            | 6.4                     | 14.075                  |                         | 0                       | 121                   | 346                    | 346                     | 1.19           | 38.9           | 265                     | 4.0            | 19.8             | 102.4            |                   | 3.79           | 554                     | 3105                                 | 1344                                 | 2096       |
| 4.0                        | 6.35       | 13.4       |            | 6.2                     | 13.075                  |                         | 0                       | 120                   | 480                    | 480                     | 1.10           | 27.1           | 238                     | 3.3            | 13.8             | 58.2             |                   | 3.44           | 497                     | 2743                                 | 1300                                 | 1709       |
| 5.0                        | 5.75       | 11.6       |            | 5.7                     | 11.275                  |                         | 0                       | 118                   | 599                    | 599                     | 0.98           | 19.8           | 194                     | 2.8            | 10.1             | 35.8             |                   | 3.15           | 405                     | 2317                                 | 1187                                 | 1276       |
| 6.0                        | 5.1        | 10         | 0          | 5.1                     | 9.675                   |                         | 0                       | 116                   | 715                    | 715                     | 0.90           | 14.8           | 159                     | 2.3            | 7.6              | 22.8             |                   | 2.87           | 333                     | 1927                                 | 1061                                 | 957        |
| 7.0                        | 4.5        | 9          |            | 4.5                     | 8.675                   |                         | 0                       | 115                   | 807                    | 807                     | 0.93           | 11.7           | 145                     | 2.0            | 5.9              | 15.6             |                   | 2.64           | 302                     | 1607                                 | 940                                  | 800        |
| 8.0                        | 4.5        | 9.2        |            | 4.5                     | 8.875                   |                         | 0                       | 116                   | 922                    | 922                     | 0.98           | 10.2           | 152                     | 1.9            | 5.2              | 12.6             |                   | 2.52           | 318                     | 1550                                 | 938                                  | 799        |
| 9.0                        | 4.5        | 9          | 0          | 4.5                     | 8.675                   |                         | 0                       | 115                   | 1037                   | 1037                    | 0.93           | 9.1            | 145                     | 1.7            | 4.6              | 10.6             |                   | 2.40           | 302                     | 1509                                 | 940                                  | 726        |
| 10.0                       | 3.8        | 8.75       |            | 3.8                     | 8.425                   |                         | 0                       | 115                   | 1148                   | 1148                    | 1.23           | 6.9            | 161                     |                |                  |                  |                   | 2.13           | 337                     |                                      |                                      | 718        |
| 11.0                       | 5.2        | 11.6       |            | 5.1                     | 11.275                  |                         | 0                       | 118                   | 1267                   | 1267                    | 1.21           | 8.4            | 214                     |                |                  |                  |                   | 2.33           | 447                     |                                      |                                      | 1042       |
| 12.0                       | 4.25       | 9.2        | 0          | 4.2                     | 8.875                   |                         | 0                       | 115                   | 1382                   | 1382                    | 1.10           | 6.4            | 161                     | 1.4            | 3.3              | 6.1              |                   | 2.06           | 337                     | 1299                                 | 883                                  | 692        |
| 13.0                       | 3.85       | 8.35       |            | 3.9                     | 8.025                   |                         | 0                       | 114                   | 1486                   | 1486                    | 1.08           | 5.4            | 145                     | 1.2            | 2.8              | 4.7              |                   | 1.89           | 302                     | 1135                                 | 804                                  | 572        |
| 14.0                       | 4.35       | 8.85       |            | 4.4                     | 8.525                   |                         | 0                       | 115                   | 1601                   | 1601                    | 0.96           | 5.7            | 145                     | 1.3            | 2.9              | 5.1              |                   | 1.93           | 302                     | 1297                                 | 909                                  | 585        |
| 15.0                       | 4.55       | 9.2        | 0          | 4.5                     | 8.875                   |                         | 0                       | 115                   | 1717                   | 1717                    | 0.95           | 5.5            | 150                     | 1.2            | 2.8              | 4.9              |                   | 1.91           | 314                     | 1346                                 | 949                                  | 598        |
| 16.0                       | 5.25       | 10.6       |            | 5.2                     | 10.275                  |                         | 0                       | 117                   | 1875                   | 1875                    | 0.97           | 5.8            | 176                     | 1.3            | 3.0              | 5.3              |                   | 1.96           | 367                     | 1562                                 | 1088                                 | 718        |
| 17.0                       | 4.55       | 9.2        |            | 4.5                     | 8.875                   |                         | 0                       | 115                   | 1991                   | 1991                    | 0.95           | 4.8            | 150                     | 1.1            | 2.4              | 3.9              |                   | 1.76           | 314                     | 1297                                 | 949                                  | 552        |
| 18.0                       | 4.65       | 9.6        | 0          | 4.6                     | 9.275                   |                         | 0                       | 116                   | 2107                   | 2107                    | 1.00           | 4.6            | 161                     | 1.1            | 2.3              | 3.7              |                   | 1.72           | 337                     | 1309                                 | 967                                  | 580        |
| 19.0                       | 4.25       | 9          |            | 4.2                     | 8.675                   |                         | 0                       | 115                   | 2189                   | 2189                    | 1.05           | 4.0            | 154                     | 1.0            | 2.1              | 3.0              |                   | 1.60           | 322                     | 1161                                 | 885                                  | 514        |
| 20.0                       | 4.05       | 8.1        |            | 4.1                     | 7.775                   |                         | 0                       | 114                   | 2303                   | 2303                    | 0.91           | 3.7            | 128                     | 0.9            | 1.9              | 2.6              |                   | 1.50           | 268                     | 1091                                 | 851                                  | 402        |
| 21.0                       | 4.6        | 9.4        | 0          | 4.6                     | 9.075                   |                         | 0                       | 116                   | 2419                   | 2419                    | 0.98           | 4.0            | 156                     | 1.0            | 2.0              | 2.9              |                   | 1.57           | 325                     | 1250                                 | 958                                  | 512        |
| 22.0                       | 4.55       | 9.2        |            | 4.5                     | 8.875                   |                         | 0                       | 115                   | 2541                   | 2541                    | 0.95           | 3.7            | 150                     | 0.9            | 1.9              | 2.6              |                   | 1.51           | 314                     | 1220                                 | 949                                  | 475        |
| 23.0                       | 2.85       | 6.05       |            | 2.9                     | 5.725                   |                         | 0                       | 111                   | 2652                   | 2652                    | 0.96           | 2.3            | 97                      | 0.6            | 1.2              | 1.2              |                   | 1.03           | 204                     | 694                                  | 609                                  | 209        |
| 24.0                       | 3.6        | 6.95       | 0          | 3.7                     | 6.625                   |                         | 0                       | 112                   | 2691                   | 2691                    | 0.81           | 2.8            | 103                     | 0.7            | 1.4              | 1.7              |                   | 1.23           | 215                     | 918                                  | 764                                  | 264        |
| 25.0                       | 3.6        | 7.5        |            | 3.6                     | 7.175                   |                         | 0                       | 113                   | 2804                   | 2804                    | 0.98           | 2.7            | 123                     | 0.7            | 1.4              | 1.6              |                   | 1.19           | 257                     | 900                                  | 758                                  | 306        |
| 26.0                       | 3.85       | 8.45       |            | 3.8                     | 8.125                   |                         | 0                       | 114                   | 2918                   | 2918                    | 1.11           | 2.8            | 148                     | 0.7            | 1.4              | 1.6              |                   | 1.22           | 310                     | 957                                  | 803                                  | 379        |
| 27.0                       | 4.35       | 8.55       | 0.05       | 4.4                     | 8.225                   | 0.25                    | 0                       | 115                   | 3094                   | 3094                    | 0.88           | 2.9            | 134                     | 0.8            | 1.5              | 1.8              |                   | 1.27           | 280                     | 1105                                 | 912                                  | 355        |
| 28.0                       | 4.55       | 9.2        |            | 4.5                     | 8.875                   |                         | 0                       | 115                   | 3210                   | 3210                    | 0.95           | 3.0            | 150                     | 0.8            | 1.5              | 1.8              |                   | 1.28           | 314                     | 1151                                 | 949                                  | 401        |



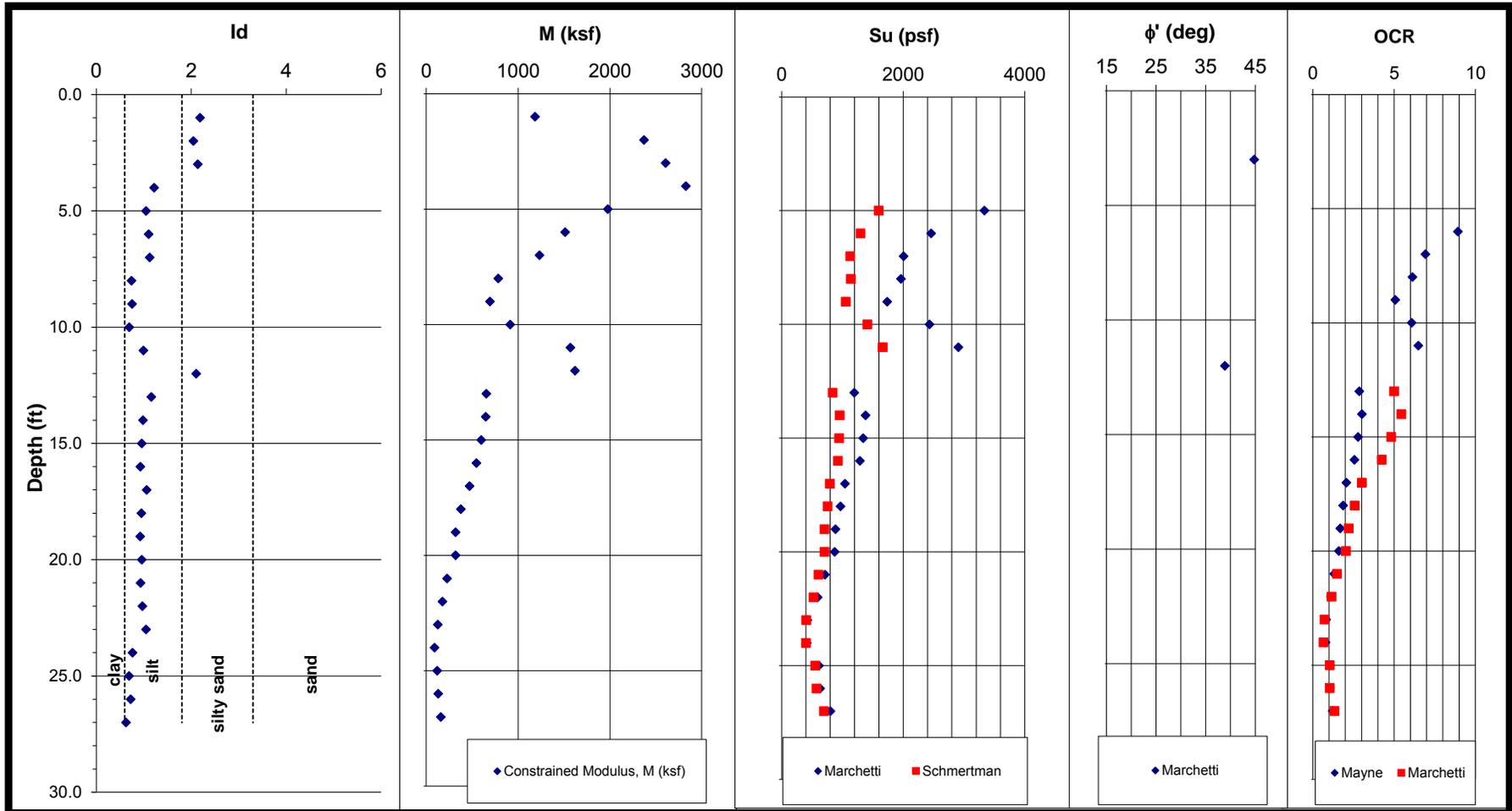
## DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112





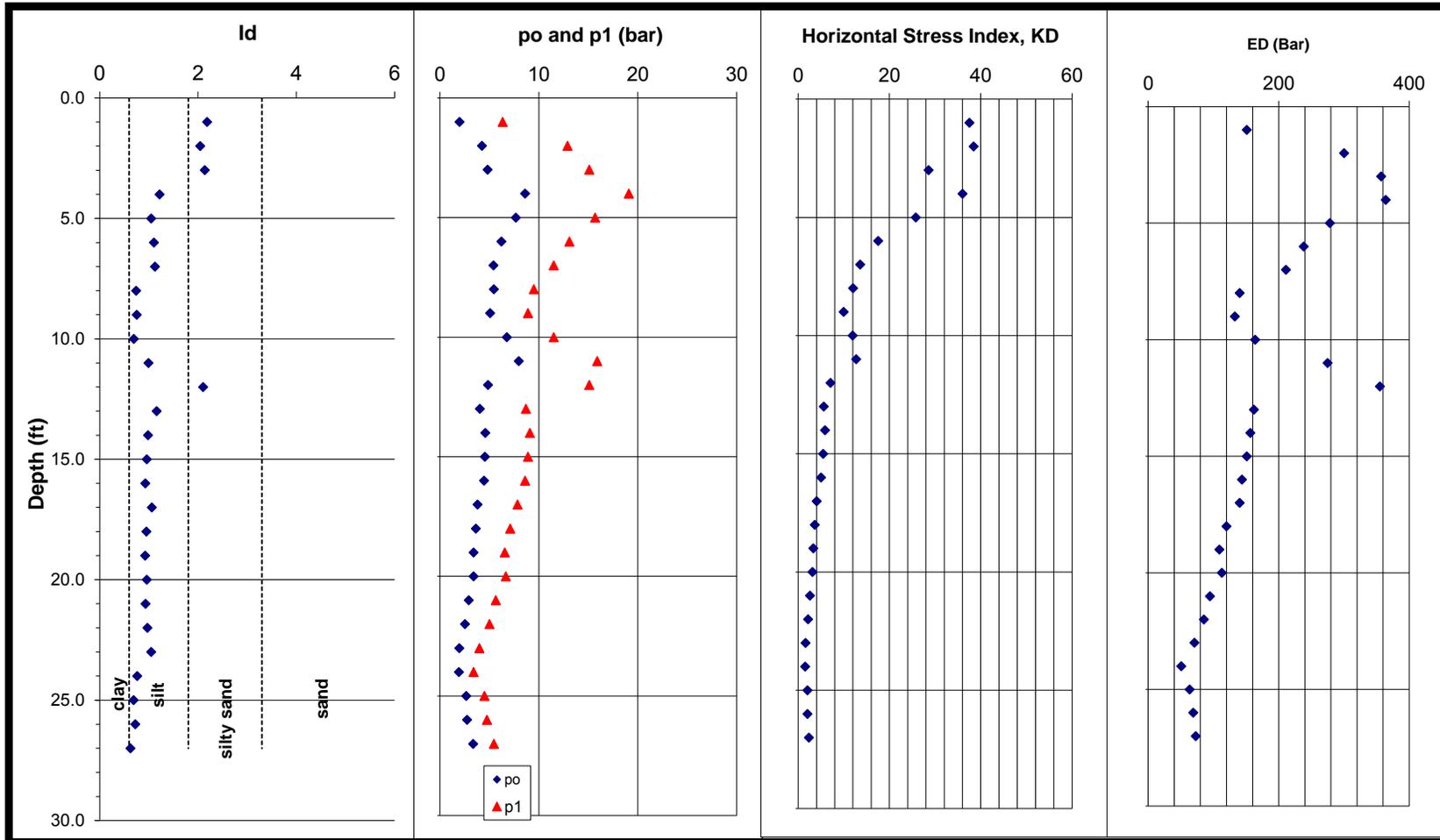
### DILATOMETER TEST RESULTS

Test ID: STR3\_EB2\_B3

Site: SITE #2 (STRUCTURE #2 AND #3) - BRIDGE NO 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)

Location: Greensboro, NC

Project No.: 16-54112



Job No: 16-54112  
 Job Name: SITE #2 (STRUCTURE #2 ANI  
 Job Location: Greensboro, NC  
 Date: 12-21-16  
 Sounding No: STR3\_EB2\_B3  
 Ground Water Depth (ft): N/A

|      | Membrane 1 | Membrane 2 | Membrane 3 |
|------|------------|------------|------------|
| ΔA = | 0.2        | 0          | 0          |
| ΔB = | 0.3        | 0          | 0          |
| Zm = | 0          | bar        |            |

Northing 874716  
 Easting 1777445

<sup>1</sup> Depth Below Existing Ground Surface  
<sup>2</sup> Mayne, 1995  
<sup>3</sup> Marchetti, 2001  
<sup>4</sup> Schmertman, 1991  
<sup>5</sup> Mayne, 2002



### DILATOMETER TEST RESULTS

| Depth <sup>1</sup><br>(ft) | A<br>(bar) | B<br>(bar) | C<br>(bar) | p <sub>o</sub><br>(bar) | p <sub>1</sub><br>(bar) | p <sub>2</sub><br>(bar) | u <sub>o</sub><br>(psf) | γ <sub>r</sub> <sup>5</sup><br>(pcf) | σ <sub>vo</sub><br>(psf) | σ <sub>vo</sub> <sup>1</sup><br>(psf) | l <sub>d</sub> | K <sub>D</sub> | E <sub>D</sub><br>(bar) | K <sub>o</sub> | OCR <sup>c</sup> | OCR <sup>2</sup> | φ <sup>3</sup><br>(deg) | R <sub>M</sub> | E <sub>D</sub><br>(ksf) | s <sub>u</sub> <sup>3</sup><br>(psf) | s <sub>u</sub> <sup>4</sup><br>(psf) | M<br>(ksf) |
|----------------------------|------------|------------|------------|-------------------------|-------------------------|-------------------------|-------------------------|--------------------------------------|--------------------------|---------------------------------------|----------------|----------------|-------------------------|----------------|------------------|------------------|-------------------------|----------------|-------------------------|--------------------------------------|--------------------------------------|------------|
| 1.0                        | 2          | 6.65       |            | 2.0                     | 6.35                    |                         | 0                       | 111                                  | 111                      | 111                                   | 2.19           | 37.5           | 151                     |                |                  |                  | 45.8                    | 3.75           | 316                     |                                      |                                      | 1185       |
| 2.0                        | 4.45       | 13.2       |            | 4.2                     | 12.9                    |                         | 0                       | 119                                  | 230                      | 230                                   | 2.04           | 38.5           | 301                     |                |                  |                  | 45.9                    | 3.78           | 628                     |                                      |                                      | 2370       |
| 3.0                        | 5.1        | 15.4       | 0          | 4.8                     | 15.1                    |                         | 0                       | 121                                  | 351                      | 351                                   | 2.14           | 28.6           | 357                     |                |                  |                  | 44.8                    | 3.50           | 746                     |                                      |                                      | 2607       |
| 4.0                        | 8.9        | 19.4       |            | 8.6                     | 19.1                    |                         | 0                       | 125                                  | 499                      | 499                                   | 1.22           | 36.0           | 364                     |                |                  |                  |                         | 3.71           | 761                     |                                      |                                      | 2826       |
| 5.0                        | 7.85       | 16         |            | 7.7                     | 15.7                    |                         | 0                       | 122                                  | 621                      | 621                                   | 1.05           | 25.8           | 279                     | 3.2            | 13.1             | 54.0             |                         | 3.40           | 582                     | 3338                                 | 1601                                 | 1978       |
| 6.0                        | 6.35       | 13.4       | 0          | 6.2                     | 13.1                    |                         | 0                       | 120                                  | 741                      | 741                                   | 1.11           | 17.5           | 239                     | 2.6            | 8.9              | 29.6             |                         | 3.03           | 498                     | 2460                                 | 1300                                 | 1511       |
| 7.0                        | 5.5        | 11.8       |            | 5.4                     | 11.5                    |                         | 0                       | 119                                  | 830                      | 830                                   | 1.13           | 13.6           | 211                     | 2.2            | 6.9              | 19.9             |                         | 2.79           | 441                     | 2008                                 | 1130                                 | 1232       |
| 8.0                        | 5.45       | 9.8        |            | 5.5                     | 9.5                     |                         | 0                       | 116                                  | 946                      | 946                                   | 0.74           | 12.1           | 140                     | 2.1            | 6.1              | 16.5             |                         | 2.68           | 293                     | 1964                                 | 1140                                 | 784        |
| 9.0                        | 5.05       | 9.2        | 0          | 5.1                     | 8.9                     |                         | 0                       | 115                                  | 1061                     | 1061                                  | 0.76           | 10.0           | 133                     | 1.8            | 5.1              | 12.3             |                         | 2.50           | 278                     | 1740                                 | 1058                                 | 694        |
| 10.0                       | 6.8        | 11.8       |            | 6.8                     | 11.5                    |                         | 0                       | 118                                  | 1183                     | 1183                                  | 0.70           | 12.0           | 164                     | 2.1            | 6.1              | 16.3             |                         | 2.67           | 342                     | 2434                                 | 1415                                 | 914        |
| 11.0                       | 8.15       | 16.2       |            | 8.0                     | 15.9                    |                         | 0                       | 122                                  | 1306                     | 1306                                  | 0.99           | 12.8           | 275                     | 2.1            | 6.5              | 18.0             |                         | 2.73           | 575                     | 2910                                 | 1665                                 | 1568       |
| 12.0                       | 5.15       | 15.4       | 0          | 4.9                     | 15.1                    |                         | 0                       | 121                                  | 1427                     | 1427                                  | 2.11           | 7.1            | 355                     |                |                  |                  | 38.9                    | 2.18           | 742                     |                                      |                                      | 1621       |
| 13.0                       | 4.05       | 9          |            | 4.0                     | 8.7                     |                         | 0                       | 115                                  | 1498                     | 1498                                  | 1.16           | 5.6            | 162                     | 1.3            | 2.9              | 5.0              |                         | 1.93           | 339                     | 1198                                 | 841                                  | 653        |
| 14.0                       | 4.6        | 9.4        |            | 4.6                     | 9.1                     |                         | 0                       | 116                                  | 1614                     | 1614                                  | 0.98           | 5.9            | 157                     | 1.3            | 3.0              | 5.5              |                         | 1.98           | 327                     | 1382                                 | 958                                  | 647        |
| 15.0                       | 4.55       | 9.2        | 0          | 4.5                     | 8.9                     |                         | 0                       | 116                                  | 1729                     | 1729                                  | 0.96           | 5.5            | 151                     | 1.2            | 2.8              | 4.8              |                         | 1.90           | 316                     | 1343                                 | 949                                  | 600        |
| 16.0                       | 4.45       | 8.9        |            | 4.5                     | 8.6                     |                         | 0                       | 115                                  | 1842                     | 1842                                  | 0.93           | 5.0            | 144                     | 1.2            | 2.6              | 4.2              |                         | 1.81           | 301                     | 1289                                 | 930                                  | 545        |
| 17.0                       | 3.8        | 8.15       |            | 3.8                     | 7.85                    |                         | 0                       | 114                                  | 1956                     | 1956                                  | 1.06           | 4.1            | 140                     | 1.0            | 2.1              | 3.0              |                         | 1.60           | 293                     | 1044                                 | 795                                  | 470        |
| 18.0                       | 3.6        | 7.4        | 0          | 3.6                     | 7.1                     |                         | 0                       | 113                                  | 2069                     | 2069                                  | 0.95           | 3.7            | 120                     | 0.9            | 1.9              | 2.6              |                         | 1.50           | 251                     | 972                                  | 759                                  | 376        |
| 19.0                       | 3.35       | 6.85       |            | 3.4                     | 6.55                    |                         | 0                       | 112                                  | 2129                     | 2129                                  | 0.93           | 3.3            | 109                     | 0.9            | 1.7              | 2.2              |                         | 1.40           | 228                     | 888                                  | 710                                  | 319        |
| 20.0                       | 3.35       | 6.95       |            | 3.4                     | 6.65                    |                         | 0                       | 112                                  | 2241                     | 2241                                  | 0.96           | 3.2            | 113                     | 0.8            | 1.6              | 2.0              |                         | 1.35           | 236                     | 875                                  | 709                                  | 318        |
| 21.0                       | 2.85       | 5.95       | 0          | 2.9                     | 5.65                    |                         | 0                       | 110                                  | 2351                     | 2351                                  | 0.93           | 2.6            | 95                      | 0.7            | 1.3              | 1.5              |                         | 1.15           | 198                     | 716                                  | 610                                  | 227        |
| 22.0                       | 2.45       | 5.3        |            | 2.5                     | 5                       |                         | 0                       | 109                                  | 2399                     | 2399                                  | 0.97           | 2.2            | 86                      | 0.6            | 1.1              | 1.2              |                         | 0.99           | 179                     | 596                                  | 529                                  | 177        |
| 23.0                       | 1.85       | 4.3        |            | 2.0                     | 4                       |                         | 0                       | 107                                  | 2506                     | 2506                                  | 1.05           | 1.6            | 71                      | 0.4            | 0.8              | 0.7              |                         | 0.85           | 148                     | 426                                  | 408                                  | 126        |
| 24.0                       | 1.8        | 3.7        | 0          | 1.9                     | 3.4                     |                         | 0                       | 105                                  | 2611                     | 2611                                  | 0.76           | 1.5            | 51                      | 0.4            | 0.8              | 0.7              |                         | 0.85           | 107                     | 416                                  | 403                                  | 91         |
| 25.0                       | 2.55       | 4.8        |            | 2.7                     | 4.5                     |                         | 0                       | 108                                  | 2693                     | 2693                                  | 0.69           | 2.1            | 64                      | 0.6            | 1.1              | 1.1              |                         | 0.89           | 133                     | 617                                  | 556                                  | 119        |
| 26.0                       | 2.65       | 5.05       |            | 2.8                     | 4.75                    |                         | 0                       | 108                                  | 2802                     | 2802                                  | 0.72           | 2.1            | 69                      | 0.6            | 1.0              | 1.0              |                         | 0.89           | 145                     | 637                                  | 575                                  | 129        |
| 27.0                       | 3.25       | 5.75       | 0          | 3.4                     | 5.45                    |                         | 0                       | 110                                  | 2911                     | 2911                                  | 0.63           | 2.4            | 73                      | 0.6            | 1.2              | 1.3              |                         | 1.04           | 152                     | 806                                  | 700                                  | 158        |

REFERENCE: U-2525C

PROJECT: 34821

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**STATE OF NORTH CAROLINA**  
**DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**

**STRUCTURE**  
**SUBSURFACE INVESTIGATION**

COUNTY GUILFORD  
PROJECT DESCRIPTION GREENSBORO EASTERN LOOP  
FROM US 29 NORTH OF GREENSBORO TO SR  
2303 (LAWNSDALE DRIVE)  
SITE DESCRIPTION MSE WALLS AT END BENT 1  
AND END BENT 2 - SITE #2 (STRUCTURE #2  
AND #3) ON I-85 BYPASS (-L-) OVER LEES  
CHAPEL ROAD (-Y1-)

| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
|-------|-----------------------------|-----------|--------------|
| N.C.  | U-2525C                     | 1         | 11           |

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**PERSONNEL**

D. KUBINSKI

R. TOOTHMAN

W. ALLEN

B. JOHNSON

INVESTIGATED BY D. KUBINSKI

DRAWN BY T. WELLS

CHECKED BY X. BARRETT

SUBMITTED BY KLEINFELDER, INC.

DATE NOVEMBER 2017

Prepared in the Office of:



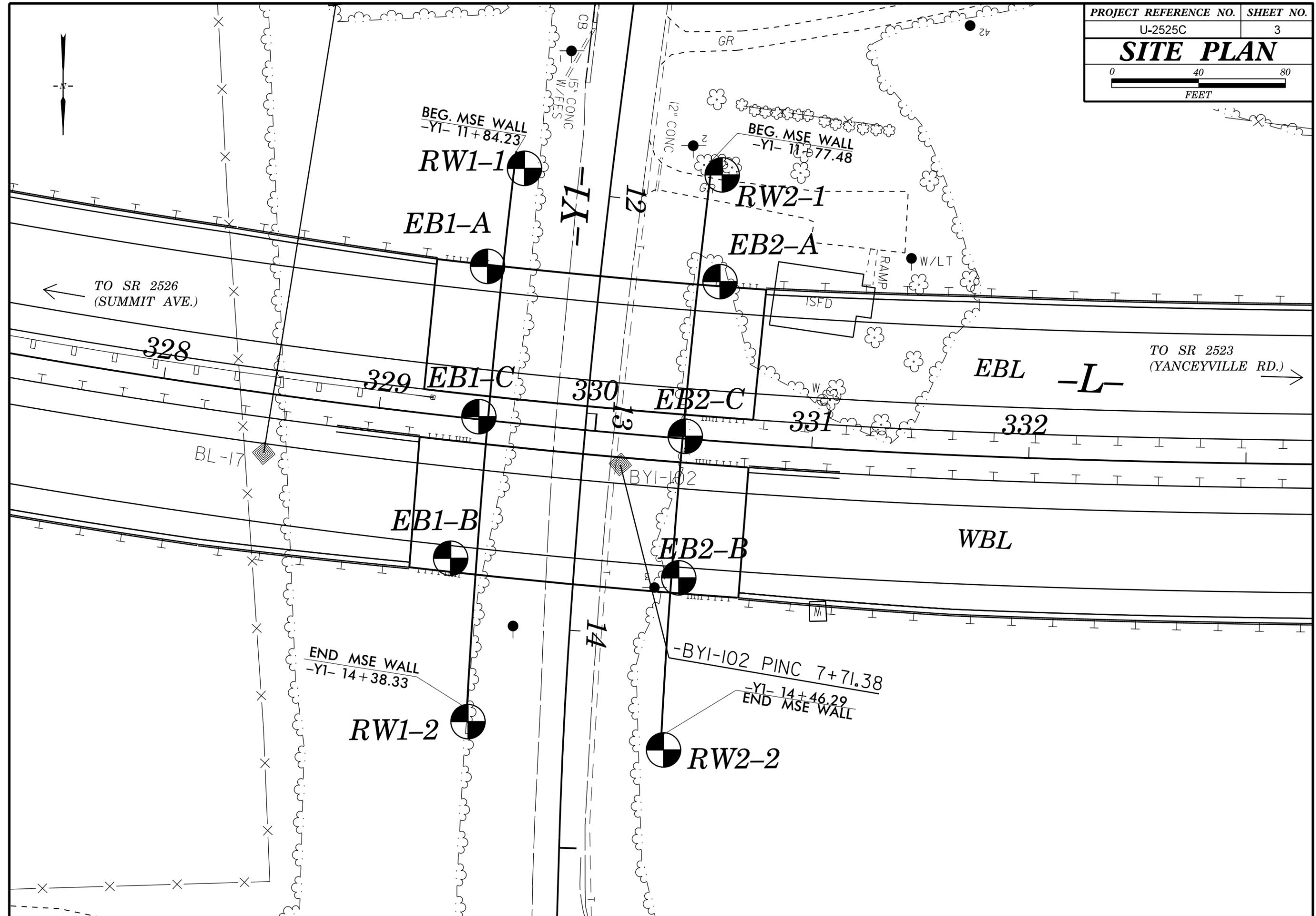
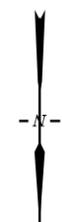
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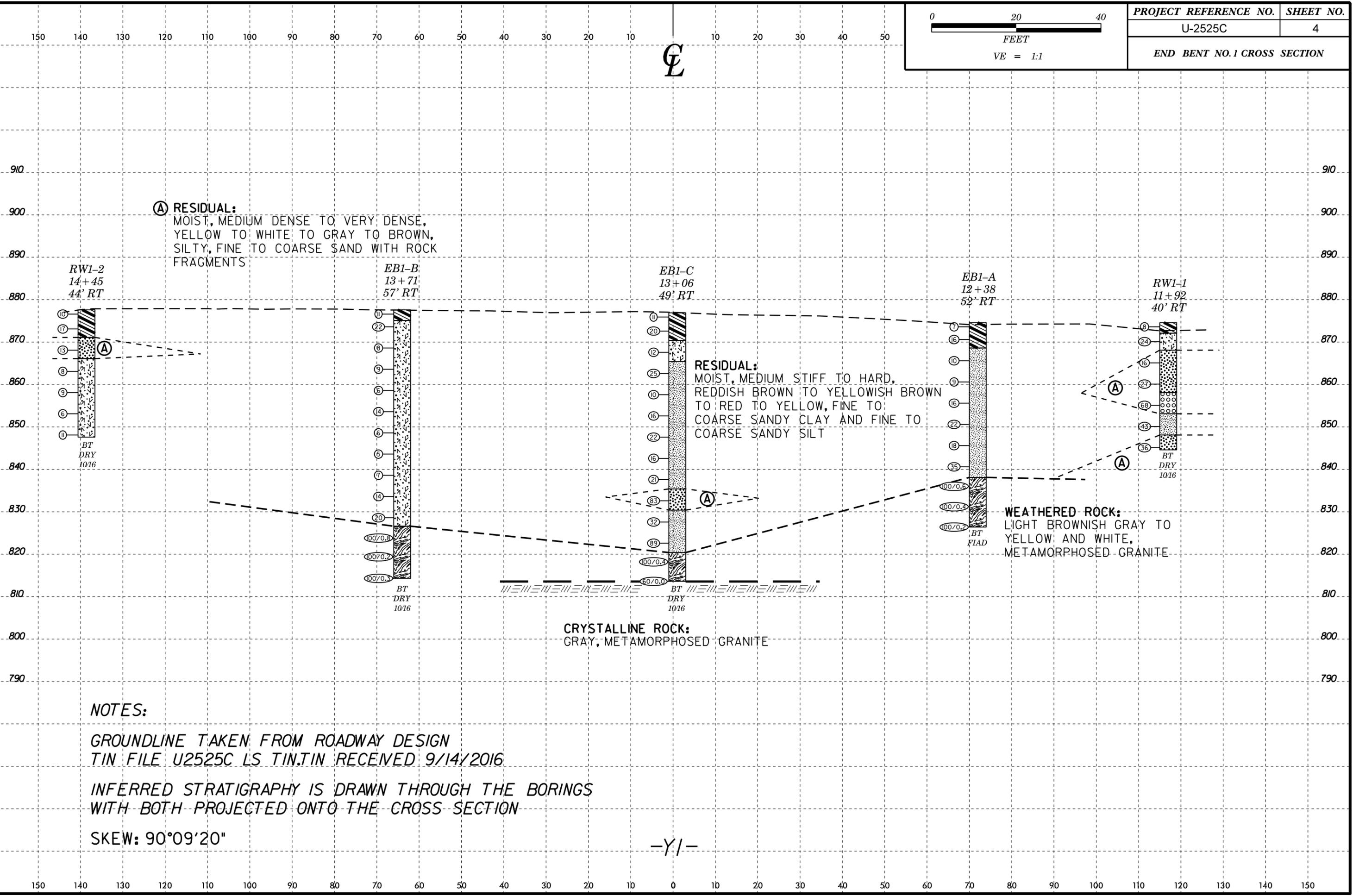
**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT  
SUBSURFACE INVESTIGATION  
SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

| SOIL DESCRIPTION   | GRADATION  | ROCK DESCRIPTION  | TERMS AND DEFINITIONS  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
|--|--|---|--|--|--|---|--|--|---|--|--|--|--|----------------------|--|---|----------|---------------|----------------|-------------------|-------|----------------------|--|-------------|-------|----------------|------------|---------------------|---|----------|-----------|---------------------|--------|----------------|--------------|-------------------------|-----------------|--------------------|------------------|-------------------|-------------------|------------------|-------------------|--|--|--|------------------------|-------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|----------------|-----------------|------------|--|----------------------------|------------|---------|-------------|-------------|-------------|-------------|-------------|---|--|-------------|-------------|---|--|----------------------|--|-------------|---|---|---|------|------|-------|-------|-------|--|--|--|--|--|--|--|--------------------------------|-------------------------------|-----------|---------------------------------|-------------|--------------|--|--|--|--|--|--|--|--|--|--|-------------------------|-------------------|--|--|--------------|--|--|--------------|------|-------------|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|---|
| <p>SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i></p>   | <p><b>WELL GRADED</b> - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.<br/><b>UNIFORMLY GRADED</b> - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.<br/><b>GAP-GRADED</b> - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.</p>  | <p>HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:</p>  | <p><b>ALLUVIUM (ALLUV.)</b> - SOILS THAT HAVE BEEN TRANSPORTED BY WATER.<br/><b>AQUIFER</b> - A WATER BEARING FORMATION OR STRATA.<br/><b>ARENACEOUS</b> - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.<br/><b>ARGILLACEOUS</b> - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.<br/><b>ARTESIAN</b> - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.<br/><b>CALCAREOUS (CALC.)</b> - SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.<br/><b>COLLUVIUM</b> - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.<br/><b>CORE RECOVERY (REC.)</b> - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/><b>DIKE</b> - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.<br/><b>DIP</b> - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.<br/><b>DIP DIRECTION (DIP AZIMUTH)</b> - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.<br/><b>FAULT</b> - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.<br/><b>FISSILE</b> - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.<br/><b>FLOAT</b> - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL.<br/><b>FLOOD PLAIN (FP)</b> - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.<br/><b>FORMATION (FM)</b> - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.<br/><b>JOINT</b> - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.<br/><b>LEDGE</b> - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.<br/><b>LENS</b> - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.<br/><b>MOTTLED (MOT.)</b> - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.<br/><b>PERCHED WATER</b> - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.<br/><b>RESIDUAL (RES.) SOIL</b> - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.<br/><b>ROCK QUALITY DESIGNATION (RQD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.<br/><b>SAPROLITE (SAP.)</b> - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.<br/><b>SILL</b> - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.<br/><b>SLICKENSIDE</b> - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.<br/><b>STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT)</b> - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.<br/><b>STRATA CORE RECOVERY (SREC.)</b> - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.<br/><b>STRATA ROCK QUALITY DESIGNATION (SROD)</b> - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.<br/><b>TOPSOIL (TS)</b> - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.</p> |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>SOIL LEGEND AND AASHTO CLASSIFICATION</b></p> <table border="1"> <thead> <tr> <th>GENERAL CLASS.</th> <th colspan="6">GRANULAR MATERIALS (≤ 35% PASSING #200)</th> <th colspan="4">SILT-CLAY MATERIALS (&gt; 35% PASSING #200)</th> <th colspan="3">ORGANIC MATERIALS</th> </tr> <tr> <th>GROUP CLASS.</th> <th>A-1</th> <th>A-1-b</th> <th>A-2</th> <th>A-2-4</th> <th>A-2-5</th> <th>A-2-6</th> <th>A-2-7</th> <th>A-4</th> <th>A-5</th> <th>A-6</th> <th>A-7</th> <th>A-1, A-2</th> <th>A-3</th> <th>A-4, A-5</th> <th>A-6, A-7</th> </tr> </thead> <tbody> <tr> <td>SYMBOL</td> <td></td> </tr> <tr> <td>% PASSING #10 #40 #200</td> <td>50 MX 30 MX 15 MX</td> <td>50 MX 25 MX</td> <td>51 MN 35 MX</td> <td>35 MX 35 MX</td> <td>35 MX 35 MX</td> <td>35 MX 35 MX</td> <td>36 MN 36 MN</td> <td>GRANULAR SOILS</td> <td>SILT-CLAY SOILS</td> <td>MUCK, PEAT</td> <td></td> </tr> <tr> <td>MATERIAL PASSING #40 LL PI</td> <td>- 6 MX</td> <td>-</td> <td>40 MX 10 MN</td> <td>41 MN 10 MN</td> <td>40 MX 11 MN</td> <td>41 MN 11 MN</td> <td>40 MX 10 MX</td> <td>41 MN 10 MX</td> <td>40 MX 10 MX</td> <td>41 MN 11 MN</td> <td>41 MN 11 MN</td> <td colspan="2">SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER</td> <td colspan="2">HIGHLY ORGANIC SOILS</td> </tr> <tr> <td>GROUP INDEX</td> <td>0</td> <td>0</td> <td>0</td> <td>4 MX</td> <td>8 MX</td> <td>12 MX</td> <td>16 MX</td> <td>NO MX</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>USUAL TYPES OF MAJOR MATERIALS</td> <td>STONE FRAGS. 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RATING AS SUBGRADE</td> <td colspan="3">EXCELLENT TO GOOD</td> <td colspan="3">FAIR TO POOR</td> <td>FAIR TO POOR</td> <td>POOR</td> <td>UNSATURABLE</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td colspan="6">PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS &gt; LL - 30</td> <td></td> </tr> </tbody> </table> | GENERAL CLASS.   | GRANULAR MATERIALS (≤ 35% PASSING #200)   |  |  |  |   |  | SILT-CLAY MATERIALS (> 35% PASSING #200) |   |  |  | ORGANIC MATERIALS  |  |                      | GROUP CLASS.   | A-1   | A-1-b    | A-2           | A-2-4          | A-2-5             | A-2-6 | A-2-7                | A-4  | A-5         | A-6   | A-7            | A-1, A-2   | A-3                 | A-4, A-5  | A-6, A-7 | SYMBOL    |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  | % PASSING #10 #40 #200 | 50 MX 30 MX 15 MX | 50 MX 25 MX | 51 MN 35 MX | 35 MX 35 MX | 35 MX 35 MX | 35 MX 35 MX | 36 MN 36 MN | GRANULAR SOILS | SILT-CLAY SOILS | MUCK, PEAT |  | MATERIAL PASSING #40 LL PI | - 6 MX     | -       | 40 MX 10 MN | 41 MN 10 MN | 40 MX 11 MN | 41 MN 11 MN | 40 MX 10 MX | 41 MN 10 MX   | 40 MX 10 MX  | 41 MN 11 MN | 41 MN 11 MN | SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER |  | HIGHLY ORGANIC SOILS |  | GROUP INDEX | 0 | 0 | 0 | 4 MX | 8 MX | 12 MX | 16 MX | NO MX |  |  |  |  |  |  |  | USUAL TYPES OF MAJOR MATERIALS | STONE FRAGS. GRAVEL, AND SAND | FINE SAND | SILTY OR CLAYEY GRAVEL AND SAND | SILTY SOILS | CLAYEY SOILS |  |  |  |  |  |  |  |  |  |  | GEN. RATING AS SUBGRADE | EXCELLENT TO GOOD |  |  | FAIR TO POOR |  |  | FAIR TO POOR | POOR | UNSATURABLE |  |  |  |  |  |  |  | PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | <p><b>ANGULARITY OF GRAINS</b></p> <p>THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: <b>ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.</b></p> | <p><b>WEATHERED ROCK (WR)</b></p> <p><b>CRYSTALLINE ROCK (CR)</b></p> <p><b>NON-CRYSTALLINE ROCK (NCR)</b></p> <p><b>COASTAL PLAIN SEDIMENTARY ROCK (CP)</b></p> | <p><b>WEATHERING</b></p> <p><b>FRESH</b> - ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.</p> <p><b>VERY SLIGHT (V SL.)</b> - ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.</p> <p><b>SLIGHT (SL.)</b> - ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.</p> <p><b>MODERATE (MOD.)</b> - SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.</p> <p><b>MODERATELY SEVERE (MOD. SEV.)</b> - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i></p> <p><b>SEVERE (SEV.)</b> - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &gt; 100 BPF</i></p> <p><b>VERY SEVERE (V SEV.)</b> - ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</i></p> <p><b>COMPLETE</b> - ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.</p> |
| GENERAL CLASS.   | GRANULAR MATERIALS (≤ 35% PASSING #200)  |   |  |  |  |   | SILT-CLAY MATERIALS (> 35% PASSING #200)       |  |   |  | ORGANIC MATERIALS                                      |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GROUP CLASS.   | A-1  | A-1-b   | A-2  | A-2-4  | A-2-5                                      | A-2-6   | A-2-7  | A-4                                      | A-5   | A-6  | A-7  | A-1, A-2   | A-3  | A-4, A-5             | A-6, A-7   |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| SYMBOL   |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| % PASSING #10 #40 #200   | 50 MX 30 MX 15 MX  | 50 MX 25 MX   | 51 MN 35 MX  | 35 MX 35 MX  | 35 MX 35 MX                                | 35 MX 35 MX   | 36 MN 36 MN                                    | 36 MN 36 MN                              | 36 MN 36 MN   | 36 MN 36 MN  | 36 MN 36 MN  | GRANULAR SOILS   | SILT-CLAY SOILS  | MUCK, PEAT           |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| MATERIAL PASSING #40 LL PI   | - 6 MX   | -   | 40 MX 10 MN  | 41 MN 10 MN  | 40 MX 11 MN                                | 41 MN 11 MN   | 40 MX 10 MX                                    | 41 MN 10 MX                              | 40 MX 10 MX   | 41 MN 11 MN  | 41 MN 11 MN  | SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER        |  | HIGHLY ORGANIC SOILS |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GROUP INDEX  | 0  | 0   | 0  | 4 MX   | 8 MX                                       | 12 MX   | 16 MX  | NO MX                                    |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| USUAL TYPES OF MAJOR MATERIALS   | STONE FRAGS. GRAVEL, AND SAND  | FINE SAND   | SILTY OR CLAYEY GRAVEL AND SAND  | SILTY SOILS  | CLAYEY SOILS                               |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GEN. RATING AS SUBGRADE  | EXCELLENT TO GOOD  |   |  | FAIR TO POOR   |  |   | FAIR TO POOR                                   | POOR                                     | UNSATURABLE   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
|  | PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>MINERALOGICAL COMPOSITION</b></p> <p>MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.</p>   | <p><b>COMPRESSION</b></p> <p>SLIGHTLY COMPRESSIBLE LL &lt; 31<br/>MODERATELY COMPRESSIBLE LL = 31 - 50<br/>HIGHLY COMPRESSIBLE LL &gt; 50</p>  | <p><b>PERCENTAGE OF MATERIAL</b></p> <table border="1"> <thead> <tr> <th>ORGANIC MATERIAL</th> <th>GRANULAR SOILS</th> <th>SILT - CLAY SOILS</th> <th>OTHER MATERIAL</th> </tr> </thead> <tbody> <tr> <td>TRACE OF ORGANIC MATTER</td> <td>2 - 3%</td> <td>3 - 5%</td> <td>TRACE 1 - 10%</td> </tr> <tr> <td>LITTLE ORGANIC MATTER</td> <td>3 - 5%</td> <td>5 - 12%</td> <td>LITTLE 10 - 20%</td> </tr> <tr> <td>MODERATELY ORGANIC</td> <td>5 - 10%</td> <td>12 - 20%</td> <td>SOME 20 - 35%</td> </tr> <tr> <td>HIGHLY ORGANIC</td> <td>&gt; 10%</td> <td>&gt; 20%</td> <td>HIGHLY 35% AND ABOVE</td> </tr> </tbody> </table> | ORGANIC MATERIAL   | GRANULAR SOILS   | SILT - CLAY SOILS                          | OTHER MATERIAL  | TRACE OF ORGANIC MATTER                        | 2 - 3%                                   | 3 - 5%  | TRACE 1 - 10%  | LITTLE ORGANIC MATTER                                  | 3 - 5%   | 5 - 12%  | LITTLE 10 - 20%      | MODERATELY ORGANIC                                   | 5 - 10%   | 12 - 20% | SOME 20 - 35% | HIGHLY ORGANIC | > 10%             | > 20% | HIGHLY 35% AND ABOVE | <p><b>GROUND WATER</b></p> <p> WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING</p> <p> STATIC WATER LEVEL AFTER 24 HOURS</p> <p> PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA</p> <p> SPRING OR SEEP</p> |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| ORGANIC MATERIAL   | GRANULAR SOILS   | SILT - CLAY SOILS   | OTHER MATERIAL   |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| TRACE OF ORGANIC MATTER  | 2 - 3%   | 3 - 5%  | TRACE 1 - 10%  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| LITTLE ORGANIC MATTER  | 3 - 5%   | 5 - 12%   | LITTLE 10 - 20%  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| MODERATELY ORGANIC   | 5 - 10%  | 12 - 20%  | SOME 20 - 35%  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| HIGHLY ORGANIC   | > 10%  | > 20%   | HIGHLY 35% AND ABOVE   |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>CONSISTENCY OR DENSENESS</b></p> <table border="1"> <thead> <tr> <th>PRIMARY SOIL TYPE</th> <th>COMPACTNESS OR CONSISTENCY</th> <th>RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)</th> <th>RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT<sup>2</sup>)</th> </tr> </thead> <tbody> <tr> <td>GENERALLY GRANULAR MATERIAL (NON-COHESIVE)</td> <td>VERY LOOSE<br/>LOOSE<br/>MEDIUM DENSE<br/>DENSE<br/>VERY DENSE</td> <td>&lt; 4<br/>4 TO 10<br/>10 TO 30<br/>30 TO 50<br/>&gt; 50</td> <td>N/A</td> </tr> <tr> <td>GENERALLY SILT-CLAY MATERIAL (COHESIVE)</td> <td>VERY SOFT<br/>SOFT<br/>MEDIUM STIFF<br/>STIFF<br/>VERY STIFF<br/>HARD</td> <td>&lt; 2<br/>2 TO 4<br/>4 TO 8<br/>8 TO 15<br/>15 TO 30<br/>&gt; 30</td> <td>&lt; 0.25<br/>0.25 TO 0.5<br/>0.5 TO 1.0<br/>1 TO 2<br/>2 TO 4<br/>&gt; 4</td> </tr> </tbody> </table>  | PRIMARY SOIL TYPE  | COMPACTNESS OR CONSISTENCY  | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)   | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) | GENERALLY GRANULAR MATERIAL (NON-COHESIVE) | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE          | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50 | N/A                                      | GENERALLY SILT-CLAY MATERIAL (COHESIVE)               | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30 | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4 | <p><b>MISCELLANEOUS SYMBOLS</b></p> <p> ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION</p> <p> SOIL SYMBOL</p> <p> ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT</p> <p> INFERRED SOIL BOUNDARY</p> <p> INFERRED ROCK LINE</p> <p> ALLUVIAL SOIL BOUNDARY</p> <p> DIP &amp; DIP DIRECTION OF ROCK STRUCTURES</p> <p> SPT TEST BORING</p> <p> AUGER BORING</p> <p> CORE BORING</p> <p> MONITORING WELL</p> <p> PIEZOMETER INSTALLATION</p> <p> SLOPE INDICATOR INSTALLATION</p> <p> CONE PENETROMETER TEST</p> <p> SOUNDING ROD</p> <p> TEST BORING WITH CORE</p> <p> SPT N-VALUE</p> |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| PRIMARY SOIL TYPE  | COMPACTNESS OR CONSISTENCY   | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)  | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> )   |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GENERALLY GRANULAR MATERIAL (NON-COHESIVE)   | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE   | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50  | N/A  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
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| <p><b>TEXTURE OR GRAIN SIZE</b></p> <table border="1"> <thead> <tr> <th>U.S. STD. SIEVE SIZE OPENING (MM)</th> <th>4</th> <th>10</th> <th>40</th> <th>60</th> <th>200</th> <th>270</th> </tr> </thead> <tbody> <tr> <td></td> <td>4.76</td> <td>2.00</td> <td>0.42</td> <td>0.25</td> <td>0.075</td> <td>0.053</td> </tr> <tr> <td>BOULDER (BLDR.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>COBBLE (COB.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>GRAVEL (GR.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>COARSE SAND (CS.E. SD.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>FINE SAND (F SD.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>SILT (SL.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>CLAY (CL.)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>GRAIN SIZE</td> <td>305 IN.</td> <td>75 IN.</td> <td>2.0</td> <td>0.25</td> <td>0.05</td> <td>0.005</td> </tr> </tbody> </table>   | U.S. STD. SIEVE SIZE OPENING (MM)  | 4   | 10   | 40   | 60   | 200   | 270  |  | 4.76  | 2.00   | 0.42   | 0.25   | 0.075  | 0.053                | BOULDER (BLDR.)                                      |   |          |               |                |                   |       | COBBLE (COB.)        |  |             |       |                |            |                     | GRAVEL (GR.)  |          |           |                     |        |                |              | COARSE SAND (CS.E. SD.) |                 |                    |                  |                   |                   |                  | FINE SAND (F SD.) |  |  |  |                        |                   |             | SILT (SL.)  |             |             |             |             |             |             | CLAY (CL.)  |             |                |                 |            |  |                            | GRAIN SIZE | 305 IN. | 75 IN.      | 2.0         | 0.25        | 0.05        | 0.005       | <p><b>RECOMMENDATION SYMBOLS</b></p> <p> UNDERCUT</p> <p> SHALLOW UNDERCUT</p> <p> UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE</p> <p> UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADED ROCK</p> <p> UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL</p> | <p><b>ABBREVIATIONS</b></p> <p>AR - AUGER REFUSAL<br/>BT - BORING TERMINATED<br/>CL - CLAY<br/>CPT - CONE PENETRATION TEST<br/>CSE - COARSE<br/>DMT - DILATOMETER TEST<br/>DPT - DYNAMIC PENETRATION TEST<br/>e - VOID RATIO<br/>F - FINE<br/>FOSS. - FOSSILIFEROUS<br/>FRAC. - FRACTURED, FRACTURES<br/>FRAGS. - FRAGMENTS<br/>HI. - HIGHLY</p> <p>MED. - MEDIUM<br/>MICA - MICACEOUS<br/>MOD. - MODERATELY<br/>NP - NON PLASTIC<br/>ORG. - ORGANIC<br/>PMT - PRESSUREMETER TEST<br/>SAP. - SAPROLITIC<br/>SD. - SAND, SANDY<br/>SL. - SILT, SILTY<br/>SLI. - SLIGHTLY<br/>TCR - TRICONE REFUSAL<br/>w - MOISTURE CONTENT<br/>V - VERY</p> <p>VST - VANE SHEAR TEST<br/>WEA. - WEATHERED<br/>% - UNIT WEIGHT<br/>%g - DRY UNIT WEIGHT</p> <p><b>SAMPLE ABBREVIATIONS</b></p> <p>S - BULK<br/>SS - SPLIT SPOON<br/>ST - SHELBY TUBE<br/>RS - ROCK<br/>RT - RECOMPACTED TRIAXIAL<br/>CBR - CALIFORNIA BEARING RATIO</p> |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| U.S. STD. SIEVE SIZE OPENING (MM)  | 4  | 10  | 40   | 60   | 200  | 270   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
|  | 4.76   | 2.00  | 0.42   | 0.25   | 0.075                                      | 0.053   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| BOULDER (BLDR.)  |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| COBBLE (COB.)  |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GRAVEL (GR.)   |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| COARSE SAND (CS.E. SD.)  |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| FINE SAND (F SD.)  |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| SILT (SL.)   |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| CLAY (CL.)   |  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| GRAIN SIZE   | 305 IN.  | 75 IN.  | 2.0  | 0.25   | 0.05                                       | 0.005   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>SOIL MOISTURE - CORRELATION OF TERMS</b></p> <table border="1"> <thead> <tr> <th>SOIL MOISTURE SCALE (ATTERBERG LIMITS)</th> <th>FIELD MOISTURE DESCRIPTION</th> <th>GUIDE FOR FIELD MOISTURE DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td>LL - LIQUID LIMIT</td> <td>- SATURATED - (SAT.)</td> <td>USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE</td> </tr> <tr> <td>PL - PLASTIC LIMIT</td> <td>- WET - (W)</td> <td>SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE</td> </tr> <tr> <td>OM - OPTIMUM MOISTURE SHRINKAGE LIMIT</td> <td>- MOIST - (M)</td> <td>SOLID; AT OR NEAR OPTIMUM MOISTURE</td> </tr> <tr> <td>SL - SHRINKAGE LIMIT</td> <td>- DRY - (D)</td> <td>REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE</td> </tr> </tbody> </table>   | SOIL MOISTURE SCALE (ATTERBERG LIMITS)   | FIELD MOISTURE DESCRIPTION  | GUIDE FOR FIELD MOISTURE DESCRIPTION   | LL - LIQUID LIMIT  | - SATURATED - (SAT.)                       | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE | PL - PLASTIC LIMIT                             | - WET - (W)                              | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE | OM - OPTIMUM MOISTURE SHRINKAGE LIMIT                            | - MOIST - (M)  | SOLID; AT OR NEAR OPTIMUM MOISTURE                             | SL - SHRINKAGE LIMIT   | - DRY - (D)          | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE | <p><b>EQUIPMENT USED ON SUBJECT PROJECT</b></p> <p>DRILL UNITS:</p> <p><input type="checkbox"/> CME-45C</p> <p><input checked="" type="checkbox"/> CME-55</p> <p><input type="checkbox"/> CME-550</p> <p><input type="checkbox"/> VANE SHEAR TEST</p> <p><input type="checkbox"/> PORTABLE HOIST</p> <p>ADVANCING TOOLS:</p> <p><input type="checkbox"/> CLAY BITS</p> <p><input checked="" type="checkbox"/> 6" CONTINUOUS FLIGHT AUGER</p> <p><input type="checkbox"/> 8" HOLLOW AUGERS</p> <p><input type="checkbox"/> HARD FACED FINGER BITS</p> <p><input type="checkbox"/> TUNG-CARBIDE INSERTS</p> <p><input type="checkbox"/> CASING <input type="checkbox"/> W/ ADVANCER</p> <p><input checked="" type="checkbox"/> TRICONE 2-1/8" STEEL TEETH</p> <p><input type="checkbox"/> TRICONE " TUNG-CARB.</p> <p><input type="checkbox"/> CORE BIT</p> <p>HAMMER TYPE:</p> <p><input checked="" type="checkbox"/> AUTOMATIC <input type="checkbox"/> MANUAL</p> <p>CORE SIZE:</p> <p><input type="checkbox"/> -B <input type="checkbox"/> -H <input type="checkbox"/> -N</p> <p>HAND TOOLS:</p> <p><input type="checkbox"/> POST HOLE DIGGER</p> <p><input type="checkbox"/> HAND AUGER</p> <p><input type="checkbox"/> SOUNDING ROD</p> <p><input type="checkbox"/> VANE SHEAR TEST</p> |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| SOIL MOISTURE SCALE (ATTERBERG LIMITS)   | FIELD MOISTURE DESCRIPTION   | GUIDE FOR FIELD MOISTURE DESCRIPTION  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| LL - LIQUID LIMIT  | - SATURATED - (SAT.)   | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| PL - PLASTIC LIMIT   | - WET - (W)  | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| OM - OPTIMUM MOISTURE SHRINKAGE LIMIT  | - MOIST - (M)  | SOLID; AT OR NEAR OPTIMUM MOISTURE  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| SL - SHRINKAGE LIMIT   | - DRY - (D)  | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>PLASTICITY</b></p> <table border="1"> <thead> <tr> <th>NON PLASTIC</th> <th>PLASTICITY INDEX (PI)</th> <th>DRY STRENGTH</th> </tr> </thead> <tbody> <tr> <td>SLIGHTLY PLASTIC</td> <td>0-5</td> <td>VERY LOW</td> </tr> <tr> <td>MODERATELY PLASTIC</td> <td>6-15</td> <td>SLIGHT</td> </tr> <tr> <td>HIGHLY PLASTIC</td> <td>16-25</td> <td>MEDIUM</td> </tr> <tr> <td></td> <td>26 OR MORE</td> <td>HIGH</td> </tr> </tbody> </table>  | NON PLASTIC  | PLASTICITY INDEX (PI)   | DRY STRENGTH   | SLIGHTLY PLASTIC   | 0-5  | VERY LOW  | MODERATELY PLASTIC                             | 6-15                                     | SLIGHT  | HIGHLY PLASTIC   | 16-25  | MEDIUM   |  | 26 OR MORE           | HIGH   | <p><b>FRACTURE SPACING</b></p> <table border="1"> <thead> <tr> <th>TERM</th> <th>SPACING</th> </tr> </thead> <tbody> <tr> <td>VERY WIDE</td> <td>MORE THAN 10 FEET</td> </tr> <tr> <td>WIDE</td> <td>3 TO 10 FEET</td> </tr> <tr> <td>MODERATELY CLOSE</td> <td>1 TO 3 FEET</td> </tr> <tr> <td>CLOSE</td> <td>0.16 TO 1 FOOT</td> </tr> <tr> <td>VERY CLOSE</td> <td>LESS THAN 0.16 FEET</td> </tr> </tbody> </table>  | TERM     | SPACING       | VERY WIDE      | MORE THAN 10 FEET | WIDE  | 3 TO 10 FEET         | MODERATELY CLOSE   | 1 TO 3 FEET | CLOSE | 0.16 TO 1 FOOT | VERY CLOSE | LESS THAN 0.16 FEET | <p><b>BEDDING</b></p> <table border="1"> <thead> <tr> <th>TERM</th> <th>THICKNESS</th> </tr> </thead> <tbody> <tr> <td>VERY THICKLY BEDDED</td> <td>4 FEET</td> </tr> <tr> <td>THICKLY BEDDED</td> <td>1.5 - 4 FEET</td> </tr> <tr> <td>THINLY BEDDED</td> <td>0.16 - 1.5 FEET</td> </tr> <tr> <td>VERY THINLY BEDDED</td> <td>0.03 - 0.16 FEET</td> </tr> <tr> <td>THICKLY LAMINATED</td> <td>0.008 - 0.03 FEET</td> </tr> <tr> <td>THINLY LAMINATED</td> <td>&lt; 0.008 FEET</td> </tr> </tbody> </table> | TERM     | THICKNESS | VERY THICKLY BEDDED | 4 FEET | THICKLY BEDDED | 1.5 - 4 FEET | THINLY BEDDED           | 0.16 - 1.5 FEET | VERY THINLY BEDDED | 0.03 - 0.16 FEET | THICKLY LAMINATED | 0.008 - 0.03 FEET | THINLY LAMINATED | < 0.008 FEET      |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| NON PLASTIC  | PLASTICITY INDEX (PI)  | DRY STRENGTH  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| SLIGHTLY PLASTIC   | 0-5  | VERY LOW  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| MODERATELY PLASTIC   | 6-15   | SLIGHT  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| HIGHLY PLASTIC   | 16-25  | MEDIUM  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
|  | 26 OR MORE   | HIGH  |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| TERM   | SPACING  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| VERY WIDE  | MORE THAN 10 FEET  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| WIDE   | 3 TO 10 FEET   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| MODERATELY CLOSE   | 1 TO 3 FEET  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| CLOSE  | 0.16 TO 1 FOOT   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| VERY CLOSE   | LESS THAN 0.16 FEET  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| TERM   | THICKNESS  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| VERY THICKLY BEDDED  | 4 FEET   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| THICKLY BEDDED   | 1.5 - 4 FEET   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| THINLY BEDDED  | 0.16 - 1.5 FEET  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| VERY THINLY BEDDED   | 0.03 - 0.16 FEET   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| THICKLY LAMINATED  | 0.008 - 0.03 FEET  |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| THINLY LAMINATED   | < 0.008 FEET   |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>COLOR</b></p> <p>DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.</p>  | <p><b>INDURATION</b></p> <p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p><b>FRIABLE</b> - RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.</p> <p><b>MODERATELY INDURATED</b> - GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.</p> <p><b>INDURATED</b> - GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.</p> <p><b>EXTREMELY INDURATED</b> - SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.</p> |   |  |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |
| <p><b>FRAC. SPACING</b></p> <p>VERY WIDE MORE THAN 10 FEET<br/>WIDE 3 TO 10 FEET<br/>MODERATELY CLOSE 1 TO 3 FEET<br/>CLOSE 0.16 TO 1 FOOT<br/>VERY CLOSE LESS THAN 0.16 FEET</p>  | <p><b>BEDDING</b></p> <p>VERY THICKLY BEDDED 4 FEET<br/>THICKLY BEDDED 1.5 - 4 FEET<br/>THINLY BEDDED 0.16 - 1.5 FEET<br/>VERY THINLY BEDDED 0.03 - 0.16 FEET<br/>THICKLY LAMINATED 0.008 - 0.03 FEET<br/>THINLY LAMINATED &lt; 0.008 FEET</p>   | <p><b>INDURATION</b></p> <p>FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.</p> <p><b>FRIABLE</b> - RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.</p> <p><b>MODERATELY INDURATED</b> - GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.</p> <p><b>INDURATED</b> - GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.</p> <p><b>EXTREMELY INDURATED</b> - SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.</p>                      | <p><b>BENCH MARK: BYI-102; -YI- STA. 7+71.38, (874,678 FT. N, 1,777,494 FT. E)</b></p> <p align="right">ELEVATION: 874.57 FEET</p> <p><b>NOTES:</b></p> <p>FIAD: FILLED IMMEDIATELY AFTER DRILLING</p>   |  |  |   |  |  |   |  |  |  |  |                      |  |   |          |               |                |                   |       |                      |  |             |       |                |            |                     |   |          |           |                     |        |                |              |                         |                 |                    |                  |                   |                   |                  |                   |  |  |  |                        |                   |             |             |             |             |             |             |             |             |             |             |                |                 |            |  |                            |            |         |             |             |             |             |             |   |  |             |             |   |  |                      |  |             |   |   |   |      |      |       |       |       |  |  |  |  |  |  |  |                                |                               |           |                                 |             |              |  |  |  |  |  |  |  |  |  |  |                         |                   |  |  |              |  |  |              |      |             |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |



27-OCT-2017 13:48  
W:\Share\GEO\TECHNICAL\Projects\Active Projects\2015\1548.0046A U-2525C Site #2 Retaining Walls\U2525C.GEO\_RWAL\_Site2\CADD\_GEO\TECH\Site\Sub\U2525C.geo\_xsc.sheet.dgn  
6/23/16

|                             |           |    |
|-----------------------------|-----------|----|
| 0                           | 20        | 40 |
| FEET                        |           |    |
| VE = 1:1                    |           |    |
| PROJECT REFERENCE NO.       | SHEET NO. |    |
| U-2525C                     | 4         |    |
| END BENT NO.1 CROSS SECTION |           |    |



**(A) RESIDUAL:**  
MOIST, MEDIUM DENSE TO VERY DENSE,  
YELLOW TO WHITE TO GRAY TO BROWN,  
SILTY, FINE TO COARSE SAND WITH ROCK  
FRAGMENTS

**RESIDUAL:**  
MOIST, MEDIUM STIFF TO HARD,  
REDDISH BROWN TO YELLOWISH BROWN  
TO RED TO YELLOW, FINE TO  
COARSE SANDY CLAY AND FINE TO  
COARSE SANDY SILT

**WEATHERED ROCK:**  
LIGHT BROWNISH GRAY TO  
YELLOW AND WHITE,  
METAMORPHOSED GRANITE

**CRYSTALLINE ROCK:**  
GRAY, METAMORPHOSED GRANITE

**NOTES:**  
GROUNDLINE TAKEN FROM ROADWAY DESIGN  
TIN FILE U2525C LS TIN.TIN RECEIVED 9/14/2016  
INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
WITH BOTH PROJECTED ONTO THE CROSS SECTION  
SKEW: 90°09'20"

-Y/-



# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |   |      |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|---|------|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |   |      |
| BORING NO. EB1-A  |                 | STATION 12+38       |            | OFFSET 52 ft RT         |       | ALIGNMENT -Y1-          |                 |    |    |     |           |     |                           |            |   |      |
| COLLAR ELEV. 874.6 ft   |                 | TOTAL DEPTH 48.2 ft |            | NORTHING 874,587        |       | EASTING 1,777,555       |                 |    |    |     |           |     |                           |            |   |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |   |      |
| DRILLER Toothman, R.  |                 | START DATE 10/10/16 |            | COMP. DATE 10/10/16     |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |   |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |   |      |
| 875   | 874.6           | 0.0                 | 2          | 2                       | 5     |                         |                 |    |    |     |           |     |                           | 874.6      | GROUND SURFACE  | 0.0  |
|   | 871.6           | 3.0                 | 7          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            | <b>RESIDUAL</b><br>Brown and Yellowish Brown to Red, Fine Sandy CLAY  |      |
| 870   | 866.6           | 8.0                 | 4          | 5                       | 5     |                         |                 |    |    |     |           |     |                           | 868.6      | Yellowish Brown and Yellow to Gray to Olive Yellow, Fine to Coarse Sandy SILT                                   | 6.0  |
| 865   | 861.6           | 13.0                | 3          | 4                       | 5     |                         |                 |    |    |     |           |     |                           |            |   |      |
| 860   | 856.6           | 18.0                | 5          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            |   |      |
| 855   | 851.6           | 23.0                | 5          | 10                      | 12    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 850   | 846.6           | 28.0                | 5          | 8                       | 10    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 845   | 841.6           | 33.0                | 12         | 15                      | 20    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 840   | 836.6           | 38.0                | 84         | 16/0.1                  |       |                         |                 |    |    |     |           |     |                           | 838.1      | <b>WEATHERED ROCK</b><br>Light Brownish Gray, METAMORPHOSED GRANITE   | 36.5 |
| 835   | 831.6           | 43.0                | 100/0.4    |                         |       |                         |                 |    |    |     |           |     |                           |            |   |      |
| 830   | 826.6           | 48.0                | 100/0.2    |                         |       |                         |                 |    |    |     |           |     |                           | 826.4      | Boring Terminated at Elevation 826.4 ft in WEATHERED ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.4 foot | 48.2 |

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |  |      |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|--|------|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |  |      |
| BORING NO. EB1-C  |                 | STATION 13+06       |            | OFFSET 49 ft RT         |       | ALIGNMENT -Y1-          |                 |    |    |     |           |     |                           |            |  |      |
| COLLAR ELEV. 876.9 ft   |                 | TOTAL DEPTH 63.3 ft |            | NORTHING 874,656        |       | EASTING 1,777,559       |                 |    |    |     |           |     |                           |            |  |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |                 |    |    |     |           |     |                           |            |  |      |
| DRILLER Toothman, R.  |                 | START DATE 10/06/16 |            | COMP. DATE 10/06/16     |       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |  |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |  |      |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |  |      |
| 880   | 876.9           | 0.0                 | 5          | 6                       | 5     |                         |                 |    |    |     |           |     |                           | 876.9      | GROUND SURFACE   | 0.0  |
| 875   | 873.6           | 3.3                 | 6          | 9                       | 11    |                         |                 |    |    |     |           |     |                           |            | <b>RESIDUAL</b><br>Red, Fine Sandy CLAY with Trace Mica  |      |
| 870   | 868.6           | 8.3                 | 5          | 5                       | 7     |                         |                 |    |    |     |           |     |                           | 870.4      | Red, Fine Sandy SILT with Trace Mica   | 6.5  |
| 865   | 863.6           | 13.3                | 8          | 11                      | 14    |                         |                 |    |    |     |           |     |                           | 865.4      | Red to Olive and Yellow to Light Brownish Gray, Fine Sandy SILT with Trace Mica  | 11.5 |
| 860   | 858.6           | 18.3                | 5          | 4                       | 6     |                         |                 |    |    |     |           |     |                           |            |  |      |
| 855   | 853.6           | 23.3                | 4          | 6                       | 10    |                         |                 |    |    |     |           |     |                           |            |  |      |
| 850   | 848.6           | 28.3                | 7          | 10                      | 12    |                         |                 |    |    |     |           |     |                           |            |  |      |
| 845   | 843.6           | 33.3                | 8          | 7                       | 9     |                         |                 |    |    |     |           |     |                           |            |  |      |
| 840   | 838.6           | 38.3                | 6          | 9                       | 12    |                         |                 |    |    |     |           |     |                           |            |  |      |
| 835   | 833.6           | 43.3                | 21         | 32                      | 51    |                         |                 |    |    |     |           |     |                           | 835.4      | Olive, Silty, Fine to Coarse SAND  | 41.5 |
| 830   | 828.6           | 48.3                | 13         | 14                      | 18    |                         |                 |    |    |     |           |     |                           | 830.4      | Olive and Yellow, Fine Sandy SILT with Trace Mica  | 46.5 |
| 825   | 823.6           | 53.3                | 17         | 31                      | 58    |                         |                 |    |    |     |           |     |                           |            |  |      |
| 820   | 818.6           | 58.3                | 100/0.4    |                         |       |                         |                 |    |    |     |           |     |                           | 820.4      | <b>WEATHERED ROCK</b><br>Light Brownish Gray, METAMORPHOSED GRANITE  | 56.5 |
| 815   | 813.6           | 63.3                | 60/0.0     |                         |       |                         |                 |    |    |     |           |     |                           | 813.6      | Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 813.6 ft on CRYSTALLINE ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.4 foot | 63.3 |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE#2.GPJ NC\_DOT.GDT 11/13/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |    |    |    |     |           |     |                           |            |   |      |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|----|----|----|-----|-----------|-----|---------------------------|------------|---|------|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       | GROUND WTR (ft)         |    |    |    |     |           |     |                           |            |   |      |
| BORING NO. EB1-B  |                 | STATION 13+71       |            | OFFSET 57 ft RT         |       | ALIGNMENT -Y1-          |    |    |    |     |           |     |                           |            |   |      |
| COLLAR ELEV. 877.6 ft   |                 | TOTAL DEPTH 63.3 ft |            | NORTHING 874,721        |       | EASTING 1,777,572       |    |    |    |     |           |     |                           |            |   |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |    |    |    |     |           |     |                           |            |   |      |
| DRILLER Toothman, R.  |                 | START DATE 10/06/16 |            | COMP. DATE 10/06/16     |       | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |                           |            |   |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25 | 50 | 75 | 100 |           |     |                           |            |   |      |
| 880   | 877.6           | 0.0                 |            |                         |       |                         |    |    |    |     |           |     |                           | 877.6      | GROUND SURFACE  | 0.0  |
| 875   | 874.6           | 3.0                 | 5          | 5                       | 6     | 11                      |    |    |    |     |           |     | M                         | 875.1      | RESIDUAL<br>Reddish Brown, Fine Sandy CLAY  | 2.5  |
| 870   | 869.6           | 8.0                 | 6          | 10                      | 12    | 22                      |    |    |    |     |           |     | M                         |            | Reddish Brown to Gray and Yellow to Light Brownish Gray, Fine to Coarse Sandy SILT with Trace Mica          |      |
| 865   | 864.6           | 13.0                | 3          | 4                       | 4     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 860   | 859.6           | 18.0                | 3          | 4                       | 5     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 855   | 854.6           | 23.0                | 3          | 2                       | 4     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 850   | 849.6           | 28.0                | 5          | 6                       | 8     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 845   | 844.6           | 33.0                | 2          | 3                       | 3     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 840   | 839.6           | 38.0                | 2          | 2                       | 3     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 835   | 834.6           | 43.0                | 3          | 3                       | 4     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 830   | 829.6           | 48.0                | 3          | 6                       | 8     |                         |    |    |    |     |           |     | M                         |            |   |      |
| 825   | 824.6           | 53.0                | 3          | 7                       | 13    |                         |    |    |    |     |           |     | M                         |            |   |      |
| 820   | 819.6           | 58.0                | 40         | 60/0.3                  |       |                         |    |    |    |     | 100/0.8   |     |                           |            |   |      |
| 815   | 814.6           | 63.0                | 100/0.2    |                         |       |                         |    |    |    |     | 100/0.2   |     |                           |            |   |      |
|   |                 |                     | 100/0.3    |                         |       |                         |    |    |    |     | 100/0.3   |     |                           |            |   |      |
|   |                 |                     |            |                         |       |                         |    |    |    |     |           |     |                           | 826.6      | WEATHERED ROCK<br>Yellow and Gray, METAMORPHOSED GRANITE  | 51.0 |
|   |                 |                     |            |                         |       |                         |    |    |    |     |           |     |                           | 814.3      | Boring Terminated at Elevation 814.3 ft in WEATHERED ROCK: METAMORPHOSED GRANITE<br>Topsoil 0.0 to 0.5 foot | 63.3 |

| WBS 34821.1.5   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |    |    |    |     |           |     |                           |            |  |      |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|----|----|----|-----|-----------|-----|---------------------------|------------|--|------|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |            |                         |       | GROUND WTR (ft)         |    |    |    |     |           |     |                           |            |  |      |
| BORING NO. EB2-A  |                 | STATION 12+33       |            | OFFSET 55 ft LT         |       | ALIGNMENT -Y1-          |    |    |    |     |           |     |                           |            |  |      |
| COLLAR ELEV. 873.1 ft   |                 | TOTAL DEPTH 50.0 ft |            | NORTHING 874,594        |       | EASTING 1,777,448       |    |    |    |     |           |     |                           |            |  |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |    |    |    |     |           |     |                           |            |  |      |
| DRILLER Toothman, R.  |                 | START DATE 10/03/16 |            | COMP. DATE 10/03/16     |       | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |                           |            |  |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |  |      |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25 | 50 | 75 | 100 |           |     |                           |            |  |      |
| 875   | 873.1           | 0.0                 |            |                         |       |                         |    |    |    |     |           |     |                           | 873.1      | GROUND SURFACE   | 0.0  |
| 870   | 869.6           | 3.5                 | 4          | 6                       | 9     | 15                      |    |    |    |     |           |     | M                         | 871.1      | RESIDUAL<br>Brown to Tan, Silty, Fine SAND with Trace of Organic Matter                    | 2.0  |
| 865   | 864.6           | 8.5                 | 6          | 7                       | 6     | 13                      |    |    |    |     |           |     | M                         | 866.6      | Tan, Fine Sandy CLAY   | 6.5  |
| 860   | 859.6           | 13.5                | 8          | 11                      | 10    | 21                      |    |    |    |     |           |     | W                         |            | Tan, Micaceous, Fine Sandy SILT  |      |
| 855   | 854.6           | 18.5                | 17         | 19                      | 20    | 39                      |    |    |    |     |           |     | W                         |            |  |      |
| 850   | 849.6           | 23.5                | 6          | 8                       | 15    | 23                      |    |    |    |     |           |     | W                         |            |  |      |
| 845   | 844.6           | 28.5                | 3          | 6                       | 8     | 14                      |    |    |    |     |           |     | W                         | 847.1      | WEATHERED ROCK<br>Tan, METAMORPHOSED GRANITE   | 26.0 |
| 840   | 839.6           | 33.5                | 53         | 47/0.3                  |       |                         |    |    |    |     | 100/0.8   |     | W                         | 841.6      | RESIDUAL<br>Brown and Tan, Fine Sandy SILT with Trace Mica                                 | 31.5 |
| 835   | 834.6           | 38.5                | 20         | 33                      | 62    |                         |    |    |    |     | 95        |     | W                         | 836.6      | Tan, Silty, Fine to Coarse SAND  | 36.5 |
| 830   | 829.6           | 43.5                | 35         | 27                      | 36    |                         |    |    |    |     | 63        |     | W                         | 832.1      | Brown, Fine Sandy SILT with Trace Mica   | 41.0 |
| 825   | 824.6           | 48.5                | 14         | 20                      | 31    |                         |    |    |    |     | 51        |     | W                         |            |  |      |
|   |                 |                     | 23         | 32                      | 66    |                         |    |    |    |     | 98        |     | W                         | 823.1      | Boring Terminated at Elevation 823.1 ft in RESIDUAL: Sandy SILT<br>Topsoil 0.0 to 0.3 foot | 50.0 |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE#2.GPJ NC\_DOT.GDT 11/13/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

|   |  |                     |  |                         |  |                         |  |
|---|--|---------------------|--|-------------------------|--|-------------------------|--|
| WBS 34821.1.5   |  | TIP U-2525C         |  | COUNTY GUILFORD         |  | GEOLOGIST Kubinski, D.  |  |
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |  |                     |  |                         |  | GROUND WTR (ft)         |  |
| BORING NO. EB2-C  |  | STATION 13+07       |  | OFFSET 46 ft LT         |  | ALIGNMENT -Y1-          |  |
| COLLAR ELEV. 873.7 ft   |  | TOTAL DEPTH 58.6 ft |  | NORTHING 874,665        |  | EASTING 1,777,464       |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |  |                     |  | DRILL METHOD Mud Rotary |  | HAMMER TYPE Automatic   |  |
| DRILLER Toothman, R.  |  | START DATE 10/04/16 |  | COMP. DATE 10/04/16     |  | SURFACE WATER DEPTH N/A |  |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |        |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | MOI | LOG | SOIL AND ROCK DESCRIPTION |            |   |
|-----------|-----------------|------------|------------|--------|-------|----------------|----|----|----|-----|-----------|-----|-----|---------------------------|------------|---|
|           |                 |            | 0.5ft      | 0.5ft  | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     |     | ELEV. (ft)                | DEPTH (ft) |   |
| 875       | 873.7           | 0.0        | 3          | 5      | 6     |                |    |    |    |     |           |     |     | 873.7                     | 0.0        | GROUND SURFACE  |
| 870       | 870.2           | 3.5        | 6          | 8      | 9     |                |    |    |    |     |           |     |     | 871.2                     | 2.5        | RESIDUAL<br>Reddish Brown, Fine Sandy CLAY<br>Red and Light Brown and Brown to Red to White, Fine to Coarse Sandy SILT with Trace Mica  |
| 865       | 865.2           | 8.5        | 4          | 4      | 5     |                |    |    |    |     |           |     |     |                           |            |   |
| 860       | 860.2           | 13.5       | 3          | 3      | 4     |                |    |    |    |     |           |     |     |                           |            |   |
| 855       | 855.2           | 18.5       | 3          | 3      | 4     |                |    |    |    |     |           |     |     |                           |            |   |
| 850       | 850.2           | 23.5       | 3          | 3      | 4     |                |    |    |    |     |           |     |     |                           |            |   |
| 845       | 845.2           | 28.5       | 4          | 4      | 6     |                |    |    |    |     |           |     |     | 846.7                     | 27.0       | Light Brown to Gray, Silty, Fine to Coarse SAND   |
| 840       | 840.2           | 33.5       | 6          | 9      | 12    |                |    |    |    |     |           |     |     |                           |            |   |
| 835       | 835.2           | 38.5       | 18         | 32     | 55    |                |    |    |    |     |           |     |     |                           |            |   |
| 830       | 830.2           | 43.5       | 14         | 19     | 30    |                |    |    |    |     |           |     |     |                           |            |   |
| 825       | 825.2           | 48.5       | 28         | 72/0.4 |       |                |    |    |    |     |           |     |     | 827.7                     | 46.0       | WEATHERED ROCK<br>Light Brownish Gray, METAMORPHOSED GRANITE  |
| 820       | 820.2           | 53.5       | 100/0.2    |        |       |                |    |    |    |     |           |     |     |                           |            |   |
|           | 815.2           | 58.5       | 60/0.1     |        |       |                |    |    |    |     |           |     |     | 815.2                     | 58.5       | CRYSTALLINE ROCK<br>METAMORPHOSED GRANITE<br>Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 815.1 ft IN CRYSTALLINE ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.3 foot |

|   |  |                     |  |                         |  |                         |  |
|---|--|---------------------|--|-------------------------|--|-------------------------|--|
| WBS 34821.1.5   |  | TIP U-2525C         |  | COUNTY GUILFORD         |  | GEOLOGIST Kubinski, D.  |  |
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |  |                     |  |                         |  | GROUND WTR (ft)         |  |
| BORING NO. EB2-B  |  | STATION 13+72       |  | OFFSET 49 ft LT         |  | ALIGNMENT -Y1-          |  |
| COLLAR ELEV. 872.8 ft   |  | TOTAL DEPTH 63.7 ft |  | NORTHING 874,730        |  | EASTING 1,777,467       |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |  |                     |  | DRILL METHOD Mud Rotary |  | HAMMER TYPE Automatic   |  |
| DRILLER Toothman, R.  |  | START DATE 10/04/16 |  | COMP. DATE 10/04/16     |  | SURFACE WATER DEPTH N/A |  |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |        | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | MOI | LOG | SOIL AND ROCK DESCRIPTION |            |   |
|-----------|-----------------|------------|------------|-------|--------|----------------|----|----|----|-----|-----------|-----|-----|---------------------------|------------|---|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft  | 0              | 25 | 50 | 75 | 100 |           |     |     | ELEV. (ft)                | DEPTH (ft) |   |
| 875       | 872.8           | 0.0        | 2          | 3     | 5      |                |    |    |    |     |           |     |     | 872.8                     | 0.0        | GROUND SURFACE  |
| 870       | 869.3           | 3.5        | 6          | 6     | 9      |                |    |    |    |     |           |     |     | 870.3                     | 2.5        | RESIDUAL<br>Brown, Fine Sandy CLAY<br>Reddish Brown to Dark Reddish Brown to Yellow to Yellow and White, Fine to Coarse Sandy SILT with Trace Mica          |
| 865       | 864.3           | 8.5        | 4          | 7     | 9      |                |    |    |    |     |           |     |     |                           |            |   |
| 860       | 859.3           | 13.5       | 2          | 2     | 3      |                |    |    |    |     |           |     |     |                           |            |   |
| 855       | 854.3           | 18.5       | 2          | 2     | 3      |                |    |    |    |     |           |     |     |                           |            |   |
| 850       | 849.3           | 23.5       | 2          | 1     | 2      |                |    |    |    |     |           |     |     |                           |            |   |
| 845       | 844.3           | 28.5       | 2          | 1     | 2      |                |    |    |    |     |           |     |     |                           |            |   |
| 840       | 839.3           | 33.5       | 3          | 3     | 4      |                |    |    |    |     |           |     |     | 841.8                     | 31.0       | Yellow and White, Silty, Fine to Coarse SAND  |
| 835       | 834.3           | 38.5       | 4          | 5     | 6      |                |    |    |    |     |           |     |     |                           |            |   |
| 830       | 829.3           | 43.5       | 7          | 10    | 12     |                |    |    |    |     |           |     |     |                           |            |   |
| 825       | 824.3           | 48.5       | 21         | 36    | 46     |                |    |    |    |     |           |     |     |                           |            |   |
| 820       | 819.3           | 53.5       | 38         | 61    | 39/0.3 |                |    |    |    |     |           |     |     | 818.8                     | 54.0       | WEATHERED ROCK<br>Yellow and White, METAMORPHOSED GRANITE   |
| 815       | 814.3           | 58.5       | 100/0.3    |       |        |                |    |    |    |     |           |     |     |                           |            |   |
| 810       | 809.3           | 63.5       | 100/0.2    |       |        |                |    |    |    |     |           |     |     | 809.1                     | 63.7       | Boring Terminated at Elevation 809.1 ft in WEATHERED ROCK: METAMORPHOSED GRANITE<br><br>Topsoil 0.0 to 0.7 foot<br><br>Other Samples:<br>ST-1 (15.1 - 16.8) |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE#2.GPJ NC\_DOT.GDT 11/13/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

|  |                            |                                 |                                |
|--|----------------------------|---------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.5   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD          | <b>GEOLOGIST</b> Kubinski, D.  |
| <b>SITE DESCRIPTION</b> Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                            |                                 | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> RW1-1  | <b>STATION</b> 11+92       | <b>OFFSET</b> 40 ft RT          | <b>ALIGNMENT</b> -Y1-          |
| <b>COLLAR ELEV.</b> 874.6 ft   | <b>TOTAL DEPTH</b> 30.0 ft | <b>NORTHING</b> 874,542         | <b>EASTING</b> 1,777,538       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> TRI0055 CME-55 77% 02/22/2016  |                            | <b>DRILL METHOD</b> H.S. Augers | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> Toothman, R.  | <b>START DATE</b> 10/05/16 | <b>COMP. DATE</b> 10/05/16      | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION   | DEPTH (ft) |
|-----------|-----------------|------------|------------|-------|-------|----------------|----|----|----|-----|-----------|-----|---|------------|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     |   |            |
| 875       | 874.6           | 0.0        | 3          | 4     | 4     |                |    |    |    |     |           | M   | GROUND SURFACE  | 0.0        |
|           |                 |            |            |       |       |                |    |    |    |     |           |     | <b>RESIDUAL</b>   |            |
|           | 871.1           | 3.5        | 8          | 10    | 14    |                |    |    |    |     |           | M   | Yellowish Brown, Fine Sandy CLAY  | 2.5        |
| 870       |                 |            |            |       |       |                |    |    |    |     |           |     | Yellow and Red, Fine Sandy SILT   |            |
|           | 866.1           | 8.5        | 4          | 6     | 10    |                |    |    |    |     |           | M   | Yellow to Yellow and Gray, Silty, Fine to Coarse SAND with Some Rock Fragments and Trace Mica | 6.5        |
| 865       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 861.1           | 13.5       | 10         | 13    | 14    |                |    |    |    |     |           | M   | White, Gray and Brown, Silty, Fine to Coarse Sandy Rock Fragments                             | 16.5       |
| 860       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 856.1           | 18.5       | 15         | 40    | 28    |                |    |    |    |     |           | M   | Olive and Gray, Fine to Coarse Sandy SILT with Little Rock Fragments and Trace Mica           | 21.5       |
| 855       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 851.1           | 23.5       | 8          | 17    | 26    |                |    |    |    |     |           | M   | Gray, Silty, Fine to Coarse SAND with Trace Mica  | 26.5       |
| 850       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 846.1           | 28.5       | 6          | 12    | 24    |                |    |    |    |     |           | M   |   | 30.0       |

Boring Terminated at Elevation 844.6 ft in RESIDUAL: Silty SAND  
Topsoil 0.0 to 0.7 foot

|  |                            |                                 |                                |
|--|----------------------------|---------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.5   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD          | <b>GEOLOGIST</b> Kubinski, D.  |
| <b>SITE DESCRIPTION</b> Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                            |                                 | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> RW1-2  | <b>STATION</b> 14+45       | <b>OFFSET</b> 44 ft RT          | <b>ALIGNMENT</b> -Y1-          |
| <b>COLLAR ELEV.</b> 877.6 ft   | <b>TOTAL DEPTH</b> 30.0 ft | <b>NORTHING</b> 874,796         | <b>EASTING</b> 1,777,564       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> TRI0055 CME-55 77% 02/22/2016  |                            | <b>DRILL METHOD</b> H.S. Augers | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> Toothman, R.  | <b>START DATE</b> 10/05/16 | <b>COMP. DATE</b> 10/05/16      | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION   | DEPTH (ft) |
|-----------|-----------------|------------|------------|-------|-------|----------------|----|----|----|-----|-----------|-----|---|------------|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     |   |            |
| 880       |                 |            |            |       |       |                |    |    |    |     |           |     | GROUND SURFACE  | 0.0        |
|           |                 |            |            |       |       |                |    |    |    |     |           |     | <b>RESIDUAL</b>   |            |
|           | 877.6           | 0.0        | 3          | 4     | 6     |                |    |    |    |     |           | M   | Reddish Brown, Fine Sandy CLAY  | 0.0        |
| 875       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 874.1           | 3.5        | 7          | 8     | 9     |                |    |    |    |     |           | M   | Red, Silty, Fine to Coarse SAND   | 6.5        |
| 870       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 869.1           | 8.5        | 5          | 6     | 7     |                |    |    |    |     |           | M   | Red and Yellow to Red, Brown and Yellow, Micaceous, Fine to Coarse Sandy SILT | 11.5       |
| 865       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 864.1           | 13.5       | 3          | 3     | 5     |                |    |    |    |     |           | M   |   |            |
| 860       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 859.1           | 18.5       | 3          | 4     | 5     |                |    |    |    |     |           | M   |   |            |
| 855       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 854.1           | 23.5       | 2          | 3     | 3     |                |    |    |    |     |           | M   |   |            |
| 850       |                 |            |            |       |       |                |    |    |    |     |           |     |   |            |
|           | 849.1           | 28.5       | 1          | 5     | 6     |                |    |    |    |     |           | M   |   |            |

Boring Terminated at Elevation 847.6 ft in RESIDUAL: Sandy SILT  
Topsoil 0.0 to 0.4 foot

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE#2.GPJ NC\_DOT.GDT 11/13/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.5   |                 | TIP U-2525C         |                          | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |   |  |
|---|-----------------|---------------------|--------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|---|--|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |                          |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |   |  |
| BORING NO. RW2-1  |                 | STATION 11+84       |                          | OFFSET 50 ft LT     |                       | ALIGNMENT -Y1-          |                 |    |    |     |           |     |                           |   |  |
| COLLAR ELEV. 873.7 ft   |                 | TOTAL DEPTH 29.1 ft |                          | NORTHING 874,545    |                       | EASTING 1,777,447       |                 |    |    |     |           |     |                           |   |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     | DRILL METHOD H.S. Augers |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |   |  |
| DRILLER Toothman, R.  |                 | START DATE 10/05/16 |                          | COMP. DATE 10/05/16 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |   |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT               |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft)  |  |
|   |                 |                     | 0.5ft                    | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |   |  |
| 875   | 873.7           | 0.0                 | 2                        | 5                   | 9                     |                         |                 |    |    |     |           |     | M                         | 873.7 GROUND SURFACE 0.0  |  |
| 870   | 870.2           | 3.5                 | 8                        | 8                   | 8                     |                         |                 |    |    |     |           |     | M                         | 871.2 RESIDUAL Brown, Silty, Fine SAND 2.5  |  |
|   |                 |                     |                          |                     |                       |                         |                 |    |    |     |           |     | M                         | 867.2 Yellowish Brown, Fine Sandy CLAY 6.5  |  |
| 865   | 865.2           | 8.5                 | 31                       | 28                  | 37                    |                         |                 |    |    |     |           |     | M                         | 867.2 White and Yellow to Olive, Fine Sandy SILT with Trace Mica 6.5                        |  |
| 860   | 860.2           | 13.5                | 10                       | 10                  | 16                    |                         |                 |    |    |     |           |     | M                         |   |  |
| 855   | 855.2           | 18.5                | 11                       | 20                  | 44                    |                         |                 |    |    |     |           |     | M                         |   |  |
| 850   | 850.2           | 23.5                | 10                       | 15                  | 27                    |                         |                 |    |    |     |           |     | M                         |   |  |
| 845   | 845.2           | 28.5                | 88                       | 12/0.1              |                       |                         |                 |    |    |     |           |     | M                         | 846.2 WEATHERED ROCK Gray, METAMORPHOSED GRANITE 27.5                                       |  |
|   |                 |                     |                          |                     |                       |                         |                 |    |    |     |           |     |                           | 844.6 Boring Terminated at Elevation 844.6 ft in WEATHERED ROCK: METAMORPHOSED GRANITE 29.1 |  |
|   |                 |                     |                          |                     |                       |                         |                 |    |    |     |           |     |                           | Topsoil 0.0 to 0.9 foot   |  |

| WBS 34821.1.5   |                 | TIP U-2525C         |                          | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |  |  |
|---|-----------------|---------------------|--------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|--|--|
| SITE DESCRIPTION Site #2 (Structure #2 and #3) - Bridge No. 1241 and 1242 on I-85 Bypass (-L-) over Lees Chapel Road (-Y1-) |                 |                     |                          |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |  |  |
| BORING NO. RW2-2  |                 | STATION 14+53       |                          | OFFSET 46 ft LT     |                       | ALIGNMENT -Y1-          |                 |    |    |     |           |     |                           |  |  |
| COLLAR ELEV. 873.0 ft   |                 | TOTAL DEPTH 30.0 ft |                          | NORTHING 874,809    |                       | EASTING 1,777,474       |                 |    |    |     |           |     |                           |  |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 77% 02/22/2016  |                 |                     | DRILL METHOD H.S. Augers |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |  |  |
| DRILLER Toothman, R.  |                 | START DATE 10/05/16 |                          | COMP. DATE 10/05/16 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |  |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT               |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft)   |  |
|   |                 |                     | 0.5ft                    | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |  |  |
| 875   | 873.0           | 0.0                 | 1                        | 2                   | 4                     |                         |                 |    |    |     |           |     | M                         | 873.0 GROUND SURFACE 0.0   |  |
| 870   | 869.5           | 3.5                 | 4                        | 6                   | 7                     |                         |                 |    |    |     |           |     | M                         | 870.5 RESIDUAL Reddish Brown, Fine Sandy CLAY 2.5                          |  |
|   |                 |                     |                          |                     |                       |                         |                 |    |    |     |           |     | M                         | 870.5 Reddish Brown to Yellow and Red, Fine Sandy SILT with Trace Mica 2.5 |  |
| 865   | 864.5           | 8.5                 | 5                        | 5                   | 8                     |                         |                 |    |    |     |           |     | M                         |  |  |
| 860   | 859.5           | 13.5                | 3                        | 2                   | 4                     |                         |                 |    |    |     |           |     | M                         |  |  |
| 855   | 854.5           | 18.5                | 2                        | 2                   | 3                     |                         |                 |    |    |     |           |     | M                         |  |  |
| 850   | 849.5           | 23.5                | 2                        | 2                   | 3                     |                         |                 |    |    |     |           |     | M                         |  |  |
| 845   | 844.5           | 28.5                | 4                        | 5                   | 9                     |                         |                 |    |    |     |           |     | M                         | 843.0 Boring Terminated at Elevation 843.0 ft in RESIDUAL: Sandy SILT 30.0 |  |
|   |                 |                     |                          |                     |                       |                         |                 |    |    |     |           |     |                           | Topsoil 0.0 to 0.4 foot  |  |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE#2.GPJ NC\_DOT.GDT 11/13/17

**SUMMARY OF LABORATORY TEST DATA**

**PROJECT NO. 34821.1.5 (U-2525C)**

**COUNTY: GUILFORD**

**SITE #2 (STRUCTURE #2 AND #3) – BRIDGE NO. 1241 AND 1242 ON I-85 BYPASS (-L-) OVER LEES CHAPEL ROAD (-Y1-)**

| Sample No. | Boring Number | Station | Offset | Alignment | Sample Depth (ft.) | AASHTO Class | Atterberg Limits |      |      | Gradation Results |          |           |               |             |           |          |          |
|------------|---------------|---------|--------|-----------|--------------------|--------------|------------------|------|------|-------------------|----------|-----------|---------------|-------------|-----------|----------|----------|
|            |               |         |        |           |                    |              | L.L.             | P.L. | P.I. | Pass #10          | Pass #40 | Pass #200 | Retained #270 | Coarse Sand | Fine Sand | Silt (%) | Clay (%) |
| ST-1 *     | EB2-B         | 330+44  | 64' RT | -L-       | 15.1-16.8          | A-5 (3)      | 45               | 38   | 7    | 99.71             | 77.34    | 52.28     | 53.6          | 29.89       | 23.71     | 37.21    | 9.19     |

SS = Split-Barrel Sample (ASTM-D-1586) ST = Shelby Tube (Undisturbed) Sample

S = Grab Sample

NP -- Non Plastic

NA-- Non Applicable

\* CONSOLIDATION TEST RESULTS CAN BE FOUND UNDER SEPARATE COVER

Page: 1 of 1

Lab Technician: NCDOT Certification No.: 129-01-0411 – Geotechnics, Raleigh, NC



REFERENCE: U-2525C

PROJECT: 34821

STATE OF NORTH CAROLINA  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

STRUCTURE  
SUBSURFACE INVESTIGATION

COUNTY GUILFORD  
PROJECT DESCRIPTION GREENSBORO EASTERN LOOP  
I-85 BYPASS (-L-) FROM US 29 NORTH OF  
GREENSBORO TO EAST OF LAWDALE DRIVE  
SITE DESCRIPTION SITE #3 (STRUCTURE #4 AND #5)  
BRIDGE NO. 1243 AND 1244 ON I-85 BYPASS (-L-)  
OVER NORFOLK SOUTHERN RAILROAD (-Y2-)

CONTENTS

| SHEET NO. | DESCRIPTION                                 |
|-----------|---|
| 1         | TITLE SHEET                                 |
| 2         | LEGEND (SOIL & ROCK)                        |
| 2A        | SUPPLEMENTAL LEGEND (GSI)                   |
| 3         | SITE PLAN                                   |
| 4         | PROFILE                                     |
| 5-8       | CROSS SECTIONS                              |
| 9-27      | BORE LOGS, CORE REPORTS, & CORE PHOTOGRAPHS |
| 28        | ROCK CORE TEST RESULTS                      |
| 29        | SITE PHOTOGRAPHS                            |

| STATE | STATE PROJECT REFERENCE NO. | SHEET NO. | TOTAL SHEETS |
|-------|-----------------------------|-----------|--------------|
| N.C.  | U-2525C                     | 1         | 30           |

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PERSONNEL

D. KUBINSKI

R. TOOTHMAN

W. ALLEN

INVESTIGATED BY D. KUBINSKI

DRAWN BY T. WELLS

CHECKED BY X. BARRETT

SUBMITTED BY KLEINFELDER, INC.

DATE SEPTEMBER 2017

Prepared in the Office of:



DocuSigned by:

Thomas R. Wells

10/10/2017

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SIGNATURE

DATE

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**NORTH CAROLINA DEPARTMENT OF TRANSPORTATION**  
**DIVISION OF HIGHWAYS**  
**GEOTECHNICAL ENGINEERING UNIT**  
**SUBSURFACE INVESTIGATION**  
**SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS**

| SOIL DESCRIPTION  |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |
|---|---|-------------|-------------|-------------|---------------------------------|-------------|--|-------------|--------------|-------------------|-------------|---|----------------------|------------|----------|--|--|
| SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 206, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, <i>VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6</i> |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |
| SOIL LEGEND AND AASHTO CLASSIFICATION   |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |
| GENERAL CLASS.  | GRANULAR MATERIALS (≤ 35% PASSING #200) |             |             |             |                                 |             | SILT-CLAY MATERIALS (> 35% PASSING #200) |             |              | ORGANIC MATERIALS |             |   |                      |            |          |  |  |
| GROUP CLASS.  | A-1                                     | A-1-b       | A-2         | A-2-4       | A-2-5                           | A-2-6       | A-2-7                                    | A-4         | A-5          | A-6               | A-7         | A-1, A-2  | A-3                  | A-4, A-5   | A-6, A-7 |  |  |
| SYMBOL  |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |
| % PASSING #10 #40 #200  | 50 MX 30 MX 15 MX                       | 50 MX 25 MX | 51 MN 35 MX | 35 MX 35 MX | 35 MX 35 MX                     | 35 MX 35 MX | 36 MN 36 MN                              | 36 MN 36 MN | 36 MN 36 MN  | 36 MN 36 MN       | 36 MN 36 MN | GRANULAR SOILS  | SILT-CLAY SOILS      | MUCK, PEAT |          |  |  |
| MATERIAL PASSING #40 LL PI  |   |             |             |             |                                 |             |  |             |              |                   |             | SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER | HIGHLY ORGANIC SOILS |            |          |  |  |
| GROUP INDEX   |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |
| USUAL TYPES OF MAJOR MATERIALS  | STONE FRAGS. GRAVEL, AND SAND           |             | FINE SAND   |             | SILTY OR CLAYEY GRAVEL AND SAND |             | SILTY SOILS                              |             | CLAYEY SOILS |                   |             |   |                      |            |          |  |  |
| GEN. RATING AS SUBGRADE   | EXCELLENT TO GOOD                       |             |             |             |                                 |             | FAIR TO POOR                             |             |              | FAIR TO POOR      | POOR        | UNSATURABLE   |                      |            |          |  |  |
| PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30   |   |             |             |             |                                 |             |  |             |              |                   |             |   |                      |            |          |  |  |

| CONSISTENCY OR DENSENESS                   |  |  |  |
|--|--|--|--|
| PRIMARY SOIL TYPE                          | COMPACTNESS OR CONSISTENCY                                       | RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)     | RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT <sup>2</sup> ) |
| GENERALLY GRANULAR MATERIAL (NON-COHESIVE) | VERY LOOSE<br>LOOSE<br>MEDIUM DENSE<br>DENSE<br>VERY DENSE       | < 4<br>4 TO 10<br>10 TO 30<br>30 TO 50<br>> 50         | N/A  |
| GENERALLY SILT-CLAY MATERIAL (COHESIVE)    | VERY SOFT<br>SOFT<br>MEDIUM STIFF<br>STIFF<br>VERY STIFF<br>HARD | < 2<br>2 TO 4<br>4 TO 8<br>8 TO 15<br>15 TO 30<br>> 30 | < 0.25<br>0.25 TO 0.5<br>0.5 TO 1.0<br>1 TO 2<br>2 TO 4<br>> 4   |

| TEXTURE OR GRAIN SIZE             |               |              |                        |                   |            |            |  |
|-----------------------------------|---------------|--------------|------------------------|-------------------|------------|------------|--|
| U.S. STD. SIEVE SIZE OPENING (MM) | 4             | 10           | 40                     | 60                | 200        | 270        |  |
|                                   | 4.76          | 2.00         | 0.42                   | 0.25              | 0.075      | 0.053      |  |
| BOULDER (BLDR.)                   | COBBLE (COB.) | GRAVEL (GR.) | COARSE SAND (CSE. SD.) | FINE SAND (F SD.) | SILT (SL.) | CLAY (CL.) |  |
| GRAIN SIZE                        | MM 305        | 75           | 2.0                    | 0.25              | 0.05       | 0.005      |  |
|                                   | IN. 12        | 3            |                        |                   |            |            |  |

| SOIL MOISTURE - CORRELATION OF TERMS   |                            |   |
|--|----------------------------|---|
| SOIL MOISTURE SCALE (ATTERBERG LIMITS) | FIELD MOISTURE DESCRIPTION | GUIDE FOR FIELD MOISTURE DESCRIPTION                                |
| LL<br>PLASTIC RANGE (PI)<br>PL         | - SATURATED - (SAT.)       | USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE |
|  | - WET - (W)                | SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE               |
|  | - MOIST - (M)              | SOLID; AT OR NEAR OPTIMUM MOISTURE                                  |
| OM<br>SL                               | - DRY - (D)                | REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE                |

| PLASTICITY         |                       |              |
|--------------------|-----------------------|--------------|
| NON PLASTIC        | PLASTICITY INDEX (PI) | DRY STRENGTH |
| SLIGHTLY PLASTIC   | 0-5                   | VERY LOW     |
| MODERATELY PLASTIC | 6-15                  | SLIGHT       |
| HIGHLY PLASTIC     | 16-25                 | MEDIUM       |
|                    | 26 OR MORE            | HIGH         |

| COLOR  |  |
|--|--|
| DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE. |  |

| GRADATION   |  |                   |                      |
|---|--|-------------------|----------------------|
| WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.  |  |                   |                      |
| UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.   |  |                   |                      |
| GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.  |  |                   |                      |
| ANGULARITY OF GRAINS  |  |                   |                      |
| THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.                 |  |                   |                      |
| MINERALOGICAL COMPOSITION   |  |                   |                      |
| MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE. |  |                   |                      |
| COMPRESSIBILITY   |  |                   |                      |
| SLIGHTLY COMPRESSIBLE   | LL < 31  |                   |                      |
| MODERATELY COMPRESSIBLE   | LL = 31 - 50   |                   |                      |
| HIGHLY COMPRESSIBLE   | LL > 50  |                   |                      |
| PERCENTAGE OF MATERIAL  |  |                   |                      |
| ORGANIC MATERIAL  | GRANULAR SOILS   | SILT - CLAY SOILS | OTHER MATERIAL       |
| TRACE OF ORGANIC MATTER   | 2 - 3%   | 3 - 5%            | TRACE 1 - 10%        |
| LITTLE ORGANIC MATTER   | 3 - 5%   | 5 - 12%           | LITTLE 10 - 20%      |
| MODERATELY ORGANIC  | 5 - 10%  | 12 - 20%          | SOME 20 - 35%        |
| HIGHLY ORGANIC  | > 10%  | > 20%             | HIGHLY 35% AND ABOVE |
| GROUND WATER  |  |                   |                      |
|   | WATER LEVEL IN BORE HOLE IMMEDIATELY AFTER DRILLING    |                   |                      |
|   | STATIC WATER LEVEL AFTER 24 HOURS                      |                   |                      |
|   | PERCHED WATER, SATURATED ZONE, OR WATER BEARING STRATA |                   |                      |
|   | SPRING OR SEEP   |                   |                      |

| MISCELLANEOUS SYMBOLS |  |  |  |
|-----------------------|--|--|--|
|                       | ROADWAY EMBANKMENT (RE) WITH SOIL DESCRIPTION      |  | DIP & DIP DIRECTION OF ROCK STRUCTURES |
|                       | SOIL SYMBOL  |  | TEST BORING                            |
|                       | ARTIFICIAL FILL (AF) OTHER THAN ROADWAY EMBANKMENT |  | AUGER BORING                           |
|                       | INFERRED SOIL BOUNDARY                             |  | CORE BORING                            |
|                       | INFERRED ROCK LINE                                 |  | MONITORING WELL                        |
|                       | ALLUVIAL SOIL BOUNDARY                             |  | PIEZOMETER INSTALLATION                |
|                       | SLOPE INDICATOR INSTALLATION                       |  | CONE PENETROMETER TEST                 |
|                       | SOUNDING ROD                                       |  | TEST BORING WITH CORE                  |
|                       | SPT N-VALUE  |  | SPT N-VALUE                            |

| RECOMMENDATION SYMBOLS |  |  |  |
|------------------------|--|--|--|
|                        | UNDERCUT   |  | UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE           |
|                        | SHALLOW UNDERCUT   |  | UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK |
|                        | UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL |  |  |

| ABBREVIATIONS                  |                          |                                |
|--------------------------------|--------------------------|--------------------------------|
| AR - AUGER REFUSAL             | MD. - MEDIUM             | VST - VANE SHEAR TEST          |
| BT - BORING TERMINATED         | MICA - MICACEOUS         | WEA. - WEATHERED               |
| CL. - CLAY                     | MOD. - MODERATELY        | UNIT WEIGHT                    |
| CPT - CONE PENETRATION TEST    | NP - NON PLASTIC         | DRY UNIT WEIGHT                |
| CSE. - COARSE                  | ORG. - ORGANIC           | SAMPLE ABBREVIATIONS           |
| DMT - DILATOMETER TEST         | PMT - PRESSUREMETER TEST | S - BULK                       |
| DPT - DYNAMIC PENETRATION TEST | SAP. - SAPROLITIC        | SS - SPLIT SPOON               |
| e - VOID RATIO                 | SD. - SAND, SANDY        | ST - SHELBY TUBE               |
| F - FINE                       | SL. - SILTY, SILTY       | RS - ROCK                      |
| FOSS. - FOSSILIFEROUS          | SLI. - SLIGHTLY          | RT - RECOMPACTED TRIAXIAL      |
| FRAC. - FRACTURED, FRACTURES   | TCR - TRICONE REFUSAL    | CBR - CALIFORNIA BEARING RATIO |
| FRAGS. - FRAGMENTS             | w - MOISTURE CONTENT     |                                |
| HI. - HIGHLY                   | V - VERY                 |                                |

| EQUIPMENT USED ON SUBJECT PROJECT          |   |   |
|--|---|---|
| DRILL UNITS:                               | ADVANCING TOOLS:  | HAMMER TYPE:  |
| <input type="checkbox"/> CME-45C           | <input type="checkbox"/> CLAY BITS  | <input checked="" type="checkbox"/> AUTOMATIC <input type="checkbox"/> MANUAL |
| <input checked="" type="checkbox"/> CME-55 | <input type="checkbox"/> 6" CONTINUOUS FLIGHT AUGER                             | CORE SIZE:  |
| <input type="checkbox"/> CME-550           | <input checked="" type="checkbox"/> 8" HOLLOW AUGERS                            | <input type="checkbox"/> -B <input type="checkbox"/> -H                       |
| <input type="checkbox"/> VANE SHEAR TEST   | <input type="checkbox"/> HARD FACED FINGER BITS                                 | <input checked="" type="checkbox"/> -N Q                                      |
| <input type="checkbox"/> PORTABLE HOIST    | <input type="checkbox"/> TUNG-CARBIDE INSERTS                                   | HAND TOOLS:   |
| <input type="checkbox"/>                   | <input checked="" type="checkbox"/> CASING <input type="checkbox"/> W/ ADVANCER | <input type="checkbox"/> POST HOLE DIGGER                                     |
| <input type="checkbox"/>                   | <input type="checkbox"/> TRICONE <input type="checkbox"/> STEEL TEETH           | <input type="checkbox"/> HAND AUGER   |
| <input type="checkbox"/>                   | <input checked="" type="checkbox"/> TRICONE 2-1/8" TUNG-CARB.                   | <input type="checkbox"/> SOUNDING ROD   |
| <input type="checkbox"/>                   | <input checked="" type="checkbox"/> CORE BIT                                    | <input type="checkbox"/> VANE SHEAR TEST                                      |
| <input type="checkbox"/>                   |   |   |

| ROCK DESCRIPTION  |   |
|---|---|
| HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL. SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS: |   |
| WEATHERED ROCK (WR)   | NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT N VALUES > 100 BLOWS PER FOOT IF TESTED.  |
| CRYSTALLINE ROCK (CR)   | FINE TO COARSE GRAIN IGNEOUS AND METAMORPHIC ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES GRANITE, GNEISS, GABBRO, SCHIST, ETC.  |
| NON-CRYSTALLINE ROCK (NCR)  | FINE TO COARSE GRAIN METAMORPHIC AND NON-COASTAL PLAIN SEDIMENTARY ROCK THAT WOULD YIELD SPT REFUSAL IF TESTED. ROCK TYPE INCLUDES PHYLLITE, SLATE, SANDSTONE, ETC.   |
| COASTAL PLAIN SEDIMENTARY ROCK (CP)   | COASTAL PLAIN SEDIMENTS CEMENTED INTO ROCK, BUT MAY NOT YIELD SPT REFUSAL. ROCK TYPE INCLUDES LIMESTONE, SANDSTONE, CEMENTED SHELL BEDS, ETC.   |
| WEATHERING  |   |
| FRESH   | ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.   |
| VERY SLIGHT (V SL.)   | ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN. CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.   |
| SLIGHT (SL.)  | ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.   |
| MODERATE (MOD.)   | SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.  |
| MODERATELY SEVERE (MOD. SEV.)   | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. <i>IF TESTED, WOULD YIELD SPT REFUSAL</i>   |
| SEVERE (SEV.)   | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &gt; 100 BPF</i>   |
| VERY SEVERE (V SEV.)  | ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. <i>IF TESTED, WOULD YIELD SPT N VALUES &lt; 100 BPF</i> |
| COMPLETE  | ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.  |

| ROCK HARDNESS   |   |
|-----------------|---|
| VERY HARD       | CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.   |
| HARD            | CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.   |
| MODERATELY HARD | CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.                               |
| MEDIUM HARD     | CAN BE GROUDED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.            |
| SOFT            | CAN BE GROUDED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE. |
| VERY SOFT       | CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.                          |

| FRACTURE SPACING |                     | BEDDING             |                   |
|------------------|---------------------|---------------------|-------------------|
| TERM             | SPACING             | TERM                | THICKNESS         |
| VERY WIDE        | MORE THAN 10 FEET   | VERY THICKLY BEDDED | 4 FEET            |
| WIDE             | 3 TO 10 FEET        | THICKLY BEDDED      | 1.5 - 4 FEET      |
| MODERATELY CLOSE | 1 TO 3 FEET         | THINLY BEDDED       | 0.16 - 1.5 FEET   |
| CLOSE            | 0.16 TO 1 FOOT      | VERY THINLY BEDDED  | 0.03 - 0.16 FEET  |
| VERY CLOSE       | LESS THAN 0.16 FEET | THICKLY LAMINATED   | 0.008 - 0.03 FEET |
|                  |                     | THINLY LAMINATED    | < 0.008 FEET      |

| INDURATION  |   |
|---|---|
| FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC. |   |
| FRIABLE   | RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.    |
| MODERATELY INDURATED  | GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER. |
| INDURATED   | GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.        |
| EXTREMELY INDURATED   | SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.                 |

| TERMS AND DEFINITIONS                                    |  |
|--|--|
| ALLUVIUM (ALLUV.)  | SOILS THAT HAVE BEEN TRANSPORTED BY WATER.   |
| AQUIFER  | A WATER BEARING FORMATION OR STRATA.   |
| ARENACEOUS   | APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.  |
| ARGILLACEOUS   | APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.  |
| ARTESIAN   | GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.   |
| CALCAREOUS (CALC.)                                       | SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.   |
| COLLUVIUM  | ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.  |
| CORE RECOVERY (REC.)                                     | TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.   |
| DIKE   | A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.  |
| DIP  | THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.  |
| DIP DIRECTION (DIP AZIMUTH)                              | THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.  |
| FAULT  | A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.   |
| FISSILE  | A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.  |
| FLOAT  | ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLOGGED FROM PARENT MATERIAL.   |
| FLOOD PLAIN (FP)   | LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.   |
| FORMATION (FM)   | A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.   |
| JOINT  | FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.   |
| LEDGE  | A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.  |
| LENS   | A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.   |
| MOTTLED (MOT.)   | IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.  |
| PERCHED WATER  | WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.   |
| RESIDUAL (RES.) SOIL                                     | SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.  |
| ROCK QUALITY DESIGNATION (ROD)                           | A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.  |
| SAPROLITE (SAP.)   | RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.   |
| SILL   | AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.                                    |
| SLICKENSIDE  | POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.  |
| STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) | NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS. |
| STRATA CORE RECOVERY (SREC.)                             | TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.  |
| STRATA ROCK QUALITY DESIGNATION (SROD)                   | A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.   |
| TOPSOIL (TS.)  | SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.   |

BENCH MARK: BYIA-105, STA 10+39.32 -BYIA- (874,899 FT. N, 1,776,817 FT. E)  
ELEVATION: 851.37 FEET

NOTES:  
FIAD: FILLED IMMEDIATELY AFTER DRILLING  
BORINGS EB5-C AND EB6-C WERE OBTAINED FROM THE ROADWAY INVESTIGATION PERFORMED BY S&ME FROM 11-15 TO 12-15.

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS  
GEOTECHNICAL ENGINEERING UNIT

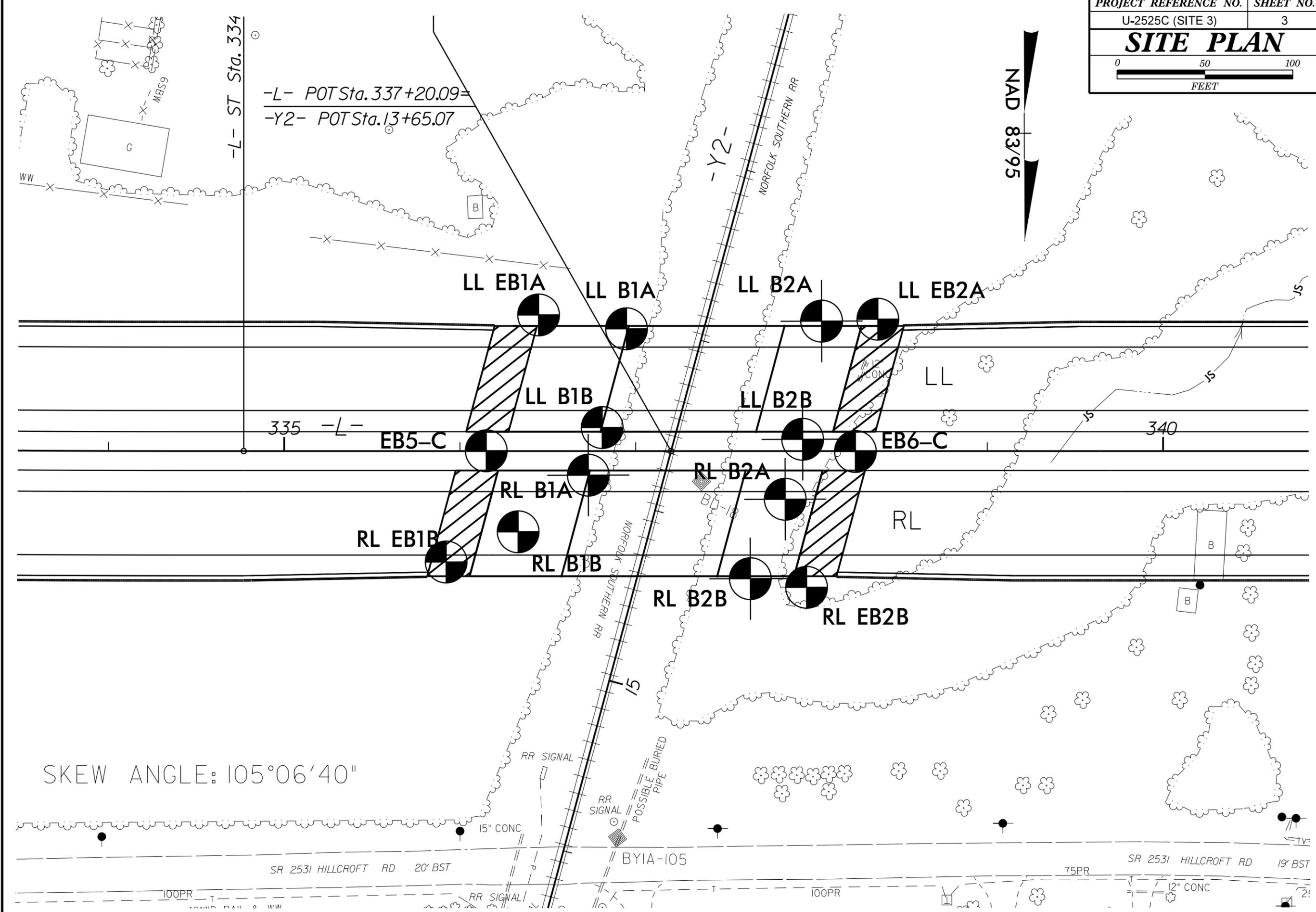
**SUBSURFACE INVESTIGATION**

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES  
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

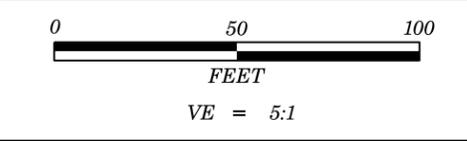
| GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)   |  | SURFACE CONDITIONS           |      |      |      |           | GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)   |   | SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes) |      |      |      |           |
|--|--|------------------------------|------|------|------|-----------|---|---|--|------|------|------|-----------|
| From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis. |  | VERY GOOD                    | GOOD | FAIR | POOR | VERY POOR | From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis. |   | VERY GOOD  | GOOD | FAIR | POOR | VERY POOR |
| STRUCTURE  |  | DECREASING SURFACE QUALITY → |      |      |      |           | COMPOSITION AND STRUCTURE   |   |  |      |      |      |           |
|  | INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities   | 90                           |      |      | N/A  | N/A       |   | A | 70   |      |      |      |           |
|  | BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets                     | 80                           |      |      |      |           |   | B | 60   |      |      |      |           |
|  | VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets                             |                              | 70   |      |      |           |   | C |  | 50   |      |      |           |
|  | BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity |                              | 60   |      |      |           |   | D |  | 40   |      |      |           |
|  | DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces                                     |                              |      | 50   |      |           |   | E |  |      | 30   |      |           |
|  | LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes  |                              |      |      | 40   |           |   | F |  |      |      | 20   |           |
|  |  |                              |      |      | 30   |           |   | G |  |      |      |      | 10        |
|  |  |                              |      |      | 20   |           |   | H |  |      |      |      |           |
|  |  |                              |      |      | 10   |           |   |   |  |      |      |      |           |
|  |  | N/A                          | N/A  |      |      |           |   |   |  |      |      |      |           |



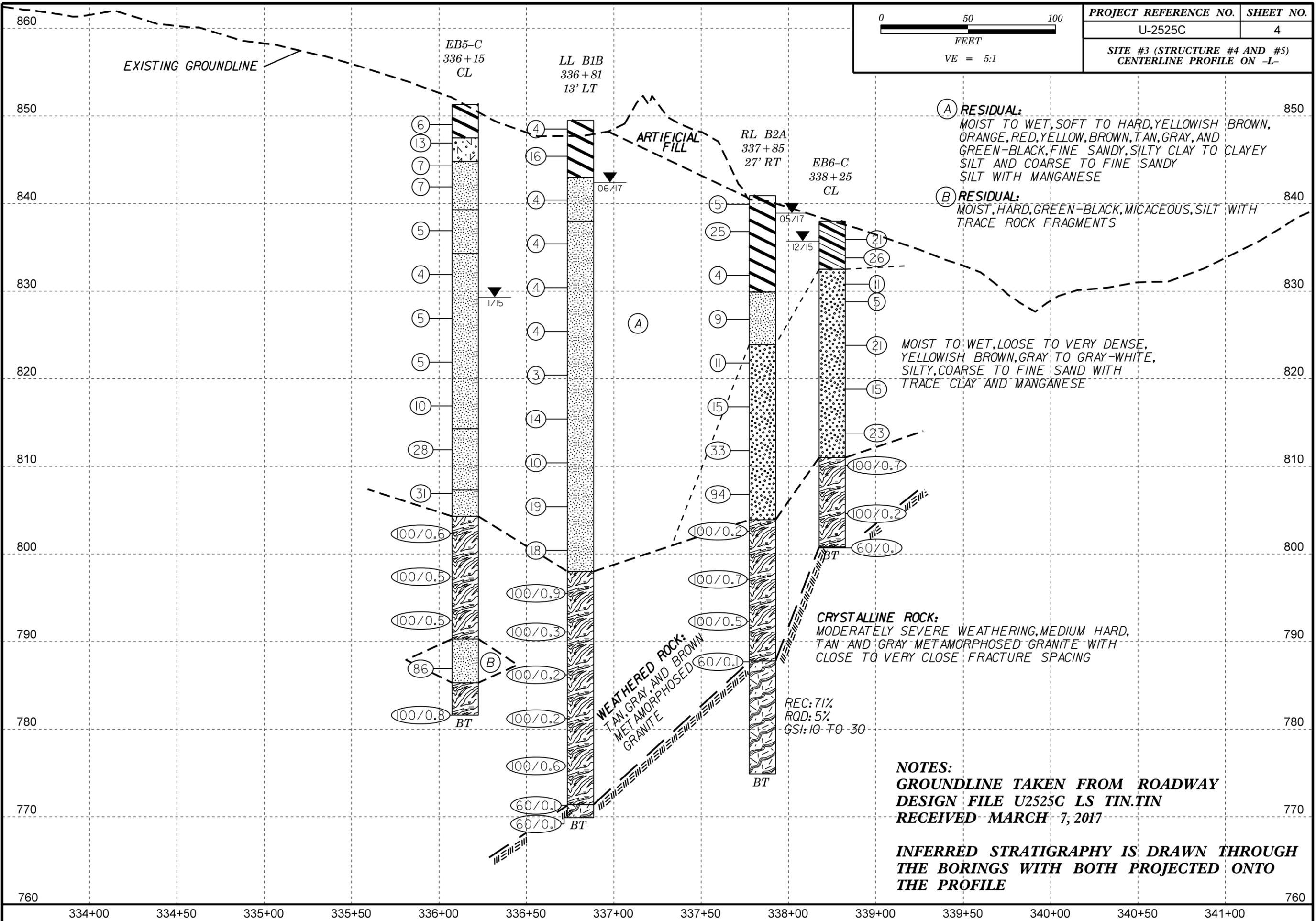
-L- POT Sta. 337+20.09=  
 -Y2- POT Sta. 13+65.07

SKEW ANGLE: 105°06'40"

100PR  
 SR 2531 HILLCROFT RD 20' BST  
 RR SIGNAL  
 15' CONC  
 RR SIGNAL  
 POSSIBLE BURIED PIPE  
 BYIA-105  
 100PR  
 75PR  
 SR 2531 HILLCROFT RD 19' BST  
 12" CONC  
 2'



|  |                  |
|--|------------------|
| <b>PROJECT REFERENCE NO.</b>                               | <b>SHEET NO.</b> |
| U-2525C  | 4                |
| SITE #3 (STRUCTURE #4 AND #5)<br>CENTERLINE PROFILE ON -L- |                  |



**(A) RESIDUAL:**  
MOIST TO WET, SOFT TO HARD, YELLOWISH BROWN, ORANGE, RED, YELLOW, BROWN, TAN, GRAY, AND GREEN-BLACK, FINE SANDY, SILTY CLAY TO CLAYEY SILT AND COARSE TO FINE SANDY SILT WITH MANGANESE

**(B) RESIDUAL:**  
MOIST, HARD, GREEN-BLACK, MICACEOUS, SILT WITH TRACE ROCK FRAGMENTS

MOIST TO WET, LOOSE TO VERY DENSE, YELLOWISH BROWN, GRAY TO GRAY-WHITE, SILTY, COARSE TO FINE SAND WITH TRACE CLAY AND MANGANESE

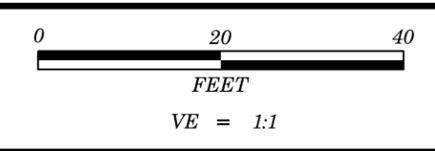
**CRYSTALLINE ROCK:**  
MODERATELY SEVERE WEATHERING, MEDIUM HARD, TAN AND GRAY METAMORPHOSED GRANITE WITH CLOSE TO VERY CLOSE FRACTURE SPACING

REC: 71%  
RQD: 5%  
GSI: 10 TO 30

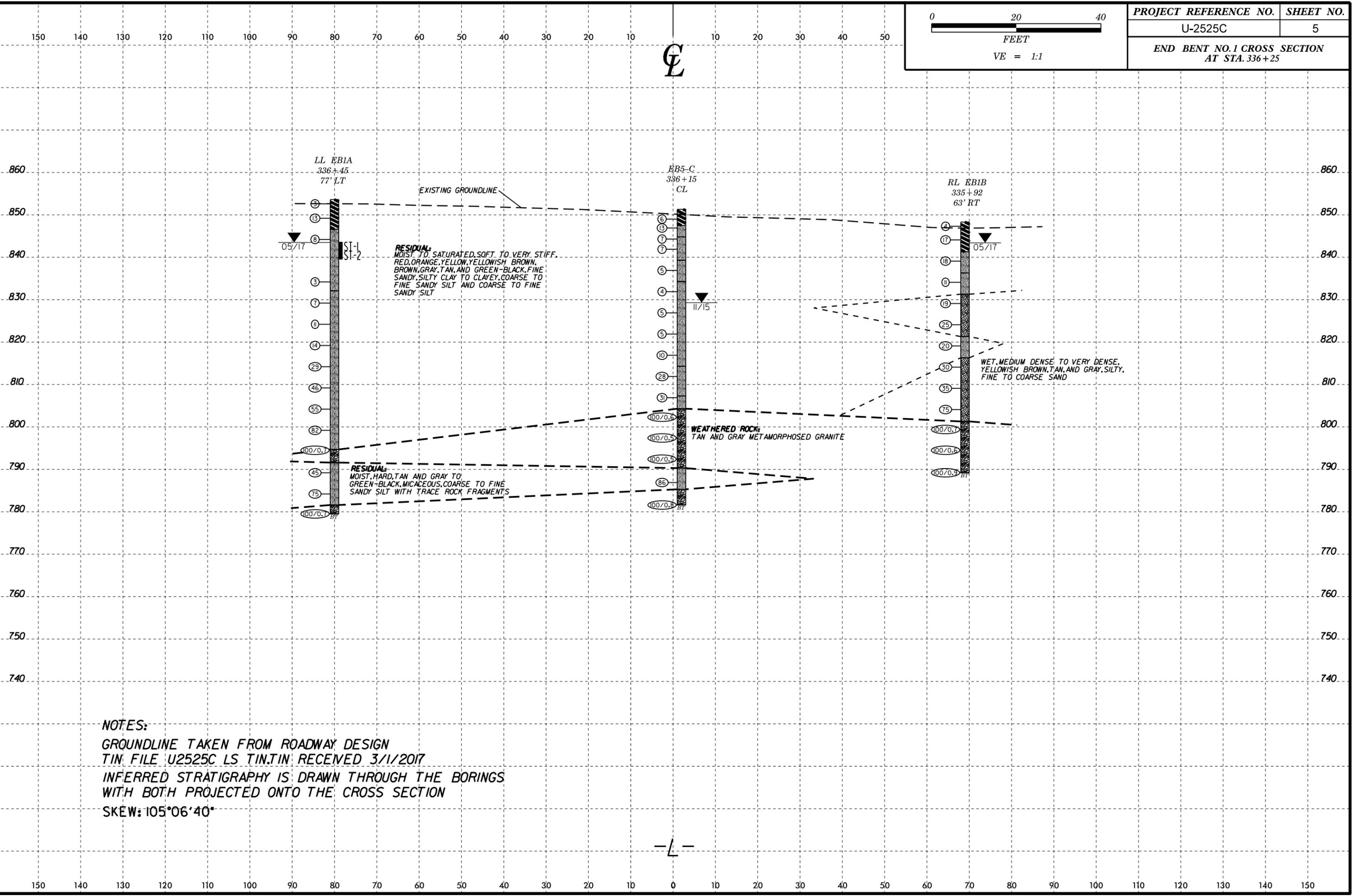
**NOTES:**  
GROUNDLINE TAKEN FROM ROADWAY DESIGN FILE U2525C LS TIN TIN  
RECEIVED MARCH 7, 2017

**INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILE**

6/23/16



|  |           |
|--|-----------|
| PROJECT REFERENCE NO.                          | SHEET NO. |
| U-2525C  | 5         |
| END BENT NO. 1 CROSS SECTION<br>AT STA. 336+25 |           |



LL EB1A  
336+45  
77' LT

BB5-C  
336+15  
CL

RL EB1B  
335+92  
63' RT

EXISTING GROUNDLINE

**RESIDUAL:**  
MOIST TO SATURATED, SOFT TO VERY STIFF,  
RED, ORANGE, YELLOW, YELLOWISH BROWN,  
BROWN, GRAY, TAN, AND GREEN-BLACK, FINE  
SANDY, SILTY CLAY TO CLAYEY, COARSE TO  
FINE SANDY SILT AND COARSE TO FINE  
SANDY SILT

**WEATHERED ROCKS:**  
TAN AND GRAY METAMORPHOSED GRANITE

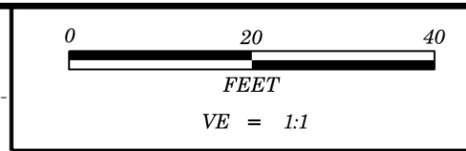
WET, MEDIUM DENSE TO VERY DENSE,  
YELLOWISH BROWN, TAN, AND GRAY, SILTY,  
FINE TO COARSE SAND

**RESIDUAL:**  
MOIST, HARD, TAN AND GRAY TO  
GREEN-BLACK, MICACEOUS, COARSE TO FINE  
SANDY SILT WITH TRACE ROCK FRAGMENTS

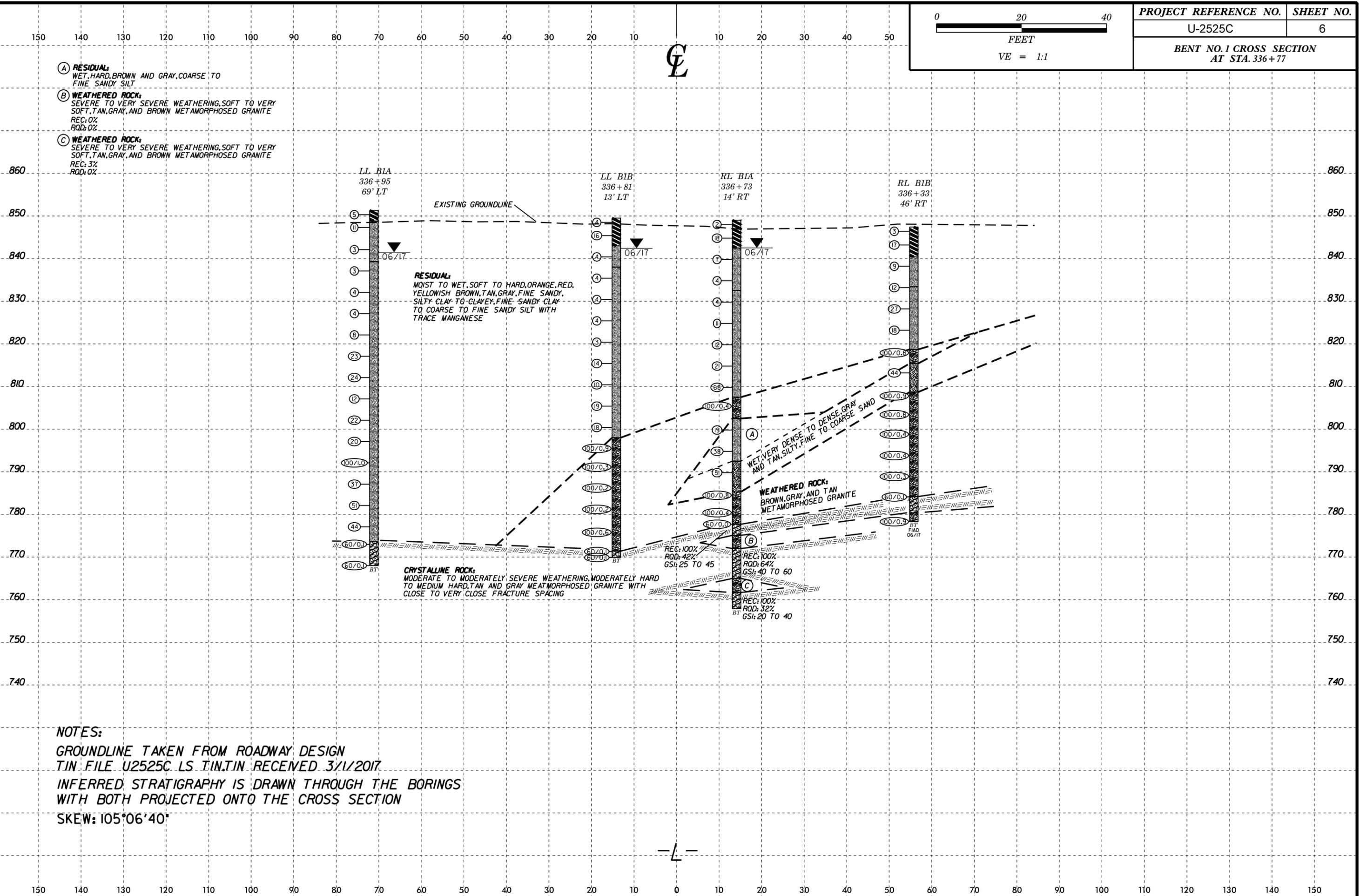
**NOTES:**  
GROUNDLINE TAKEN FROM ROADWAY DESIGN  
TIN FILE U2525C LS TINTIN RECEIVED 3/11/2017  
INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
WITH BOTH PROJECTED ONTO THE CROSS SECTION  
SKEW: 105°06'40"

03-AUG-2017 12:25  
W:\shere\GEO\TECHNICAL\Projects\Active Projects\20151548.038A U-2525C Site 5\U2525C\_GEO\_BROG\_Site#5\CADD\_GEO\BROG\_Site#5\U2525C\_GEO\_xsc\_sheet.dgn  
BAJohnson

03-AUG-2017 04:37  
 W:\shere\GEO\TECHNICAL\Projects\Active Projects\2015\151548.038A U-2525C Site 5\U2525C.GEO\BRDG\_Site#5\CADD\_GEO\TECH\Site#5\Sub\U2525C.GEO\_xsc\_sheet.dgn  
 BAJohnson AT K4206660



|  |           |
|--|-----------|
| PROJECT REFERENCE NO.                      | SHEET NO. |
| U-2525C                                    | 6         |
| BENT NO. 1 CROSS SECTION<br>AT STA. 336+77 |           |



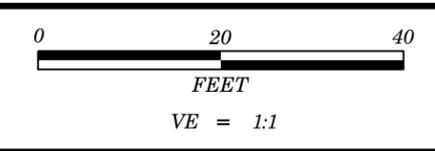
- (A) **RESIDUAL:**  
WET, HARD, BROWN AND GRAY, COARSE TO FINE SANDY SILT
- (B) **WEATHERED ROCK:**  
SEVERE TO VERY SEVERE WEATHERING, SOFT TO VERY SOFT, TAN, GRAY, AND BROWN METAMORPHOSED GRANITE  
REC: 0%  
ROD: 0%
- (C) **WEATHERED ROCK:**  
SEVERE TO VERY SEVERE WEATHERING, SOFT TO VERY SOFT, TAN, GRAY, AND BROWN METAMORPHOSED GRANITE  
REC: 3%  
ROD: 0%

**NOTES:**  
 GROUNDLINE TAKEN FROM ROADWAY DESIGN  
 TIN FILE U2525C.LS.TIN RECEIVED 3/11/2017  
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
 WITH BOTH PROJECTED ONTO THE CROSS SECTION  
 SKEW: 105°06'40"

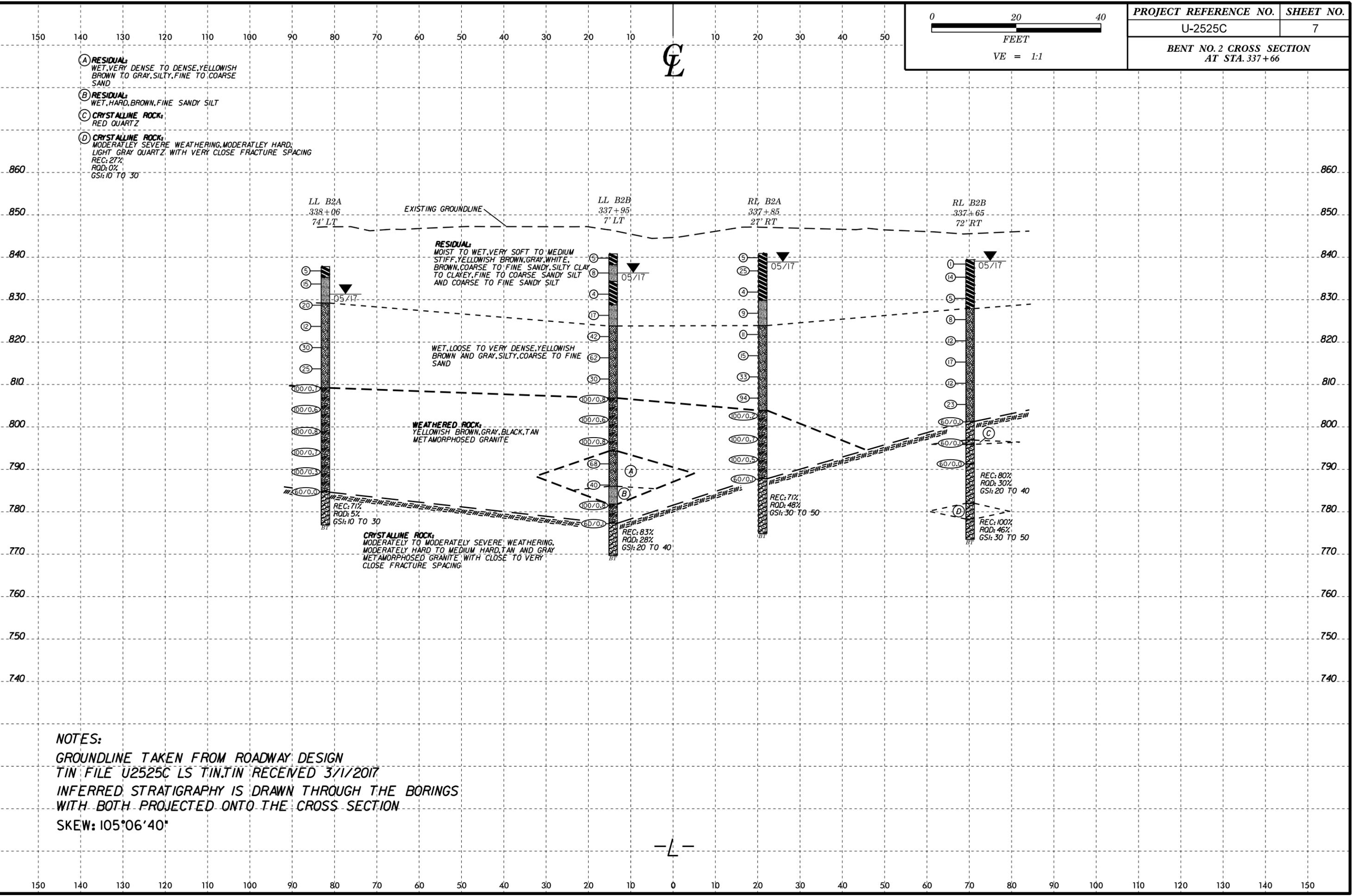
CL

-L-

6/23/16

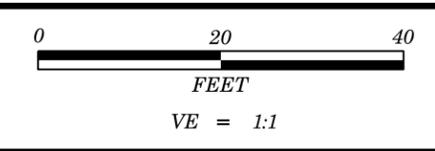


|  |           |
|--|-----------|
| PROJECT REFERENCE NO.                      | SHEET NO. |
| U-2525C                                    | 7         |
| BENT NO. 2 CROSS SECTION<br>AT STA. 337+66 |           |

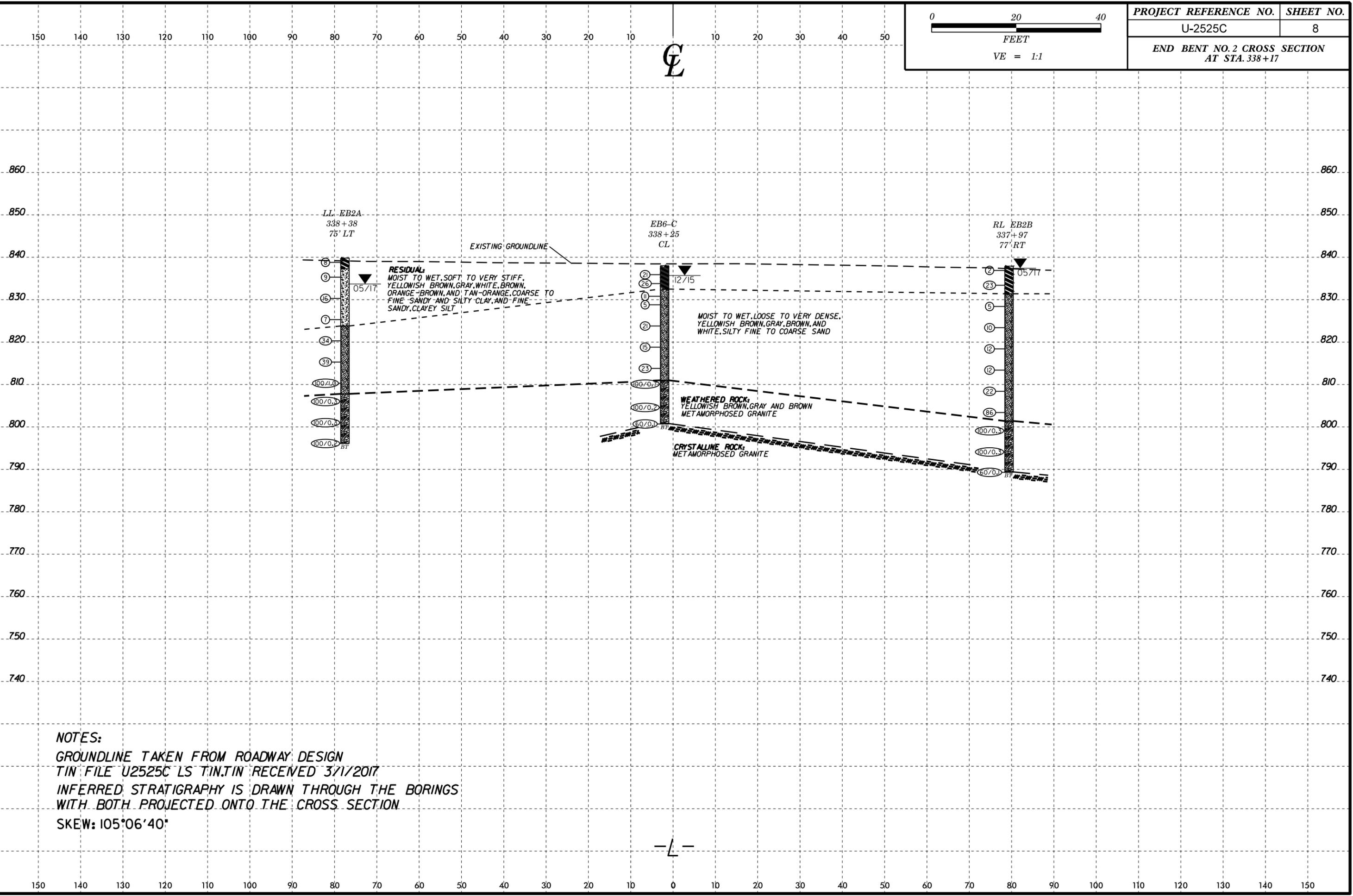


**NOTES:**  
 GROUNDLINE TAKEN FROM ROADWAY DESIGN  
 TIN FILE U2525C LS TIN.TIN RECEIVED 3/1/2017  
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
 WITH BOTH PROJECTED ONTO THE CROSS SECTION  
 SKEW: 105°06'40"

03-AUG-2017 09:37  
 W:\shere\GEO\TECHNICAL\Projects\Active Projects\2015\1548.038A U-2525C Site 5\U2525C.GEO\_BROG\_Site#5\CADD\GEO\TECH\Site#5\Sub\U2525C.GEO\_xsc\_sheet.dgn  
 BAJohnson AT KAZ06660



|  |           |
|--|-----------|
| PROJECT REFERENCE NO.                          | SHEET NO. |
| U-2525C  | 8         |
| END BENT NO. 2 CROSS SECTION<br>AT STA. 338+17 |           |



**NOTES:**  
 GROUNDLINE TAKEN FROM ROADWAY DESIGN  
 TIN FILE U2525C LS TIN.TIN RECEIVED 3/1/2017  
 INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS  
 WITH BOTH PROJECTED ONTO THE CROSS SECTION  
 SKEW: 105°06'40"

03-AUG-2017 04:38  
 W:\shere\GEO\TECHNICAL\Projects\Active Projects\2015\1548.0388A U-2525C Site 5\U2525C.GEO.BROG.Site#5\CADD.GEOTECH\Site#5\Sub\U2525C.GEO.xsc.sheet.dgn  
 BAJohnson AT K426666



# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.1   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |        | GEOLOGIST Butler, L.    |    |    |    |     |           |     |     |                           |            |   |
|---|-----------------|---------------------|------------|-------------------------|--------|-------------------------|----|----|----|-----|-----------|-----|-----|---------------------------|------------|---|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
| BORING NO. EB5-C  |                 | STATION 336+15      |            | OFFSET CL               |        | ALIGNMENT -L-           |    |    |    |     |           |     |     |                           |            |   |
| COLLAR ELEV. 851.3 ft   |                 | TOTAL DEPTH 69.7 ft |            | NORTHING 874,679        |        | EASTING 1,776,891       |    |    |    |     |           |     |     |                           |            |   |
| DRILL RIG/HAMMER EFF./DATE SME9403 CME-550X 83% 01/14/2016  |                 |                     |            | DRILL METHOD Mud Rotary |        | HAMMER TYPE Automatic   |    |    |    |     |           |     |     |                           |            |   |
| DRILLER Norwood, R.   |                 | START DATE 11/19/15 |            | COMP. DATE 11/20/15     |        | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |     |                           |            |   |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |        | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | MOI | LOG | SOIL AND ROCK DESCRIPTION |            |   |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft  | 0                       | 25 | 50 | 75 | 100 |           |     |     | ELEV. (ft)                | DEPTH (ft) |   |
| 855   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
| 850   | 850.0           | 1.3                 | 3          | 2                       | 4      |                         |    |    |    |     |           |     |     |                           |            | GROUND SURFACE 0.0                                      |
|   | 847.9           | 3.4                 | 4          | 5                       | 8      |                         |    |    |    |     |           |     |     |                           |            | RESIDUAL Orange-Brown Silty CLAY with Trace of Organics |
| 845   | 845.3           | 6.0                 | 3          | 3                       | 4      |                         |    |    |    |     |           |     |     |                           |            | Tan-Orange Clayey SILT                                  |
|   | 842.9           | 8.4                 | 2          | 3                       | 4      |                         |    |    |    |     |           |     |     |                           |            | Orange-Tan SILT   |
| 840   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 837.9           | 13.4                | 2          | 2                       | 3      |                         |    |    |    |     |           |     |     |                           |            | Orange-Gray SILT with Manganese                         |
| 835   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 832.9           | 18.4                | 2          | 2                       | 2      |                         |    |    |    |     |           |     |     |                           |            | Tan-Orange Fine Sandy SILT with Manganese               |
| 830   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 827.9           | 23.4                | 2          | 2                       | 3      |                         |    |    |    |     |           |     |     |                           |            |   |
| 825   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 822.9           | 28.4                | 2          | 2                       | 3      |                         |    |    |    |     |           |     |     |                           |            |   |
| 820   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 817.9           | 33.4                | 4          | 5                       | 5      |                         |    |    |    |     |           |     |     |                           |            |   |
| 815   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 812.9           | 38.4                | 7          | 13                      | 15     |                         |    |    |    |     |           |     |     |                           |            | Tan-Gray Fine Sandy SILT                                |
| 810   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 807.9           | 43.4                | 6          | 13                      | 18     |                         |    |    |    |     |           |     |     |                           |            |   |
| 805   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 802.9           | 48.4                | 90         | 10/0.1                  |        |                         |    |    |    |     |           |     |     |                           |            |   |
| 800   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 797.9           | 53.4                | 100/0.5    |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
| 795   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 792.9           | 58.4                | 100/0.5    |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
| 790   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 787.9           | 63.4                | 20         | 37                      | 49     |                         |    |    |    |     |           |     |     |                           |            |   |
| 785   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |
|   | 782.9           | 68.4                | 21         | 35                      | 65/0.3 |                         |    |    |    |     |           |     |     |                           |            |   |
|   |                 |                     |            |                         |        |                         |    |    |    |     |           |     |     |                           |            |   |

| WBS 34821.1.1   |                 | TIP U-2525C         |            | COUNTY GUILFORD         |       | GEOLOGIST Kubinski, D.  |    |    |    |     |           |     |     |                           |            |  |
|---|-----------------|---------------------|------------|-------------------------|-------|-------------------------|----|----|----|-----|-----------|-----|-----|---------------------------|------------|--|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |            |                         |       |                         |    |    |    |     |           |     |     |                           |            |  |
| BORING NO. RL_EB1B  |                 | STATION 335+92      |            | OFFSET 63 ft RT         |       | ALIGNMENT -L-           |    |    |    |     |           |     |     |                           |            |  |
| COLLAR ELEV. 848.3 ft   |                 | TOTAL DEPTH 59.1 ft |            | NORTHING 874,742        |       | EASTING 1,776,914       |    |    |    |     |           |     |     |                           |            |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     |            | DRILL METHOD Mud Rotary |       | HAMMER TYPE Automatic   |    |    |    |     |           |     |     |                           |            |  |
| DRILLER Toothman, R.  |                 | START DATE 05/24/17 |            | COMP. DATE 05/25/17     |       | SURFACE WATER DEPTH N/A |    |    |    |     |           |     |     |                           |            |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT |                         |       | BLOWS PER FOOT          |    |    |    |     | SAMP. NO. | MOI | LOG | SOIL AND ROCK DESCRIPTION |            |  |
|   |                 |                     | 0.5ft      | 0.5ft                   | 0.5ft | 0                       | 25 | 50 | 75 | 100 |           |     |     | ELEV. (ft)                | DEPTH (ft) |  |
| 850   |                 |                     |            |                         |       |                         |    |    |    |     |           |     |     |                           |            |  |
|   | 848.3           | 0.0                 | 1          | 1                       | 3     |                         |    |    |    |     |           |     |     |                           |            | GROUND SURFACE 0.0   |
| 845   | 845.1           | 3.2                 | 4          | 7                       | 10    |                         |    |    |    |     |           |     |     |                           |            | RESIDUAL Yellowish Brown, Tan, Red, and Orange, Fine Sandy, Silty CLAY |
| 840   | 840.1           | 8.2                 | 2          | 4                       | 14    |                         |    |    |    |     |           |     |     |                           |            | Orange and Gray, Clayey, Coarse to Fine Sandy SILT                     |
| 835   | 835.1           | 13.2                | 4          | 4                       | 7     |                         |    |    |    |     |           |     |     |                           |            | Orange, Tan, and Gray  |
| 830   | 830.1           | 18.2                | 7          | 9                       | 10    |                         |    |    |    |     |           |     |     |                           |            | Yellowish Brown, Tan, and Gray, Silty, Fine to Coarse SAND             |
| 825   | 825.1           | 23.2                | 9          | 10                      | 15    |                         |    |    |    |     |           |     |     |                           |            |  |
| 820   | 820.1           | 28.2                | 7          | 8                       | 12    |                         |    |    |    |     |           |     |     |                           |            | Yellowish Brown, Tan, and Gray, Coarse to Fine Sandy SILT              |
| 815   | 815.1           | 33.2                | 13         | 15                      | 15    |                         |    |    |    |     |           |     |     |                           |            | Yellowish Brown, Tan, and Gray, Silty, Fine to Coarse SAND             |
| 810   | 810.1           | 38.2                | 15         | 19                      | 16    |                         |    |    |    |     |           |     |     |                           |            |  |
| 805   | 805.1           | 43.2                | 15         | 27                      | 48    |                         |    |    |    |     |           |     |     |                           |            |  |
| 800   | 800.1           | 48.2                | 42         | 58/0.2                  |       |                         |    |    |    |     |           |     |     |                           |            |  |
| 795   | 795.1           | 53.2                | 55         | 45/0.1                  |       |                         |    |    |    |     |           |     |     |                           |            |  |
| 790   | 790.1           | 58.2                | 41         | 59/0.4                  |       |                         |    |    |    |     |           |     |     |                           |            |  |
|   |                 |                     |            |                         |       |                         |    |    |    |     |           |     |     |                           |            |  |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITES.GPJ NC\_DOT.GDT 9/29/17

# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |       |  |
|---|-----------------|---------------------|-------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|-------|--|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |                         |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |       |  |
| BORING NO. LL_B1A   |                 | STATION 336+95      |                         | OFFSET 69 ft LT     |                       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |       |  |
| COLLAR ELEV. 851.3 ft   |                 | TOTAL DEPTH 83.3 ft |                         | NORTHING 874,610    |                       | EASTING 1,776,811       |                 |    |    |     |           |     |                           |            |       |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     | DRILL METHOD Mud Rotary |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |            |       |  |
| DRILLER Toothman, R.  |                 | START DATE 05/30/17 |                         | COMP. DATE 05/31/17 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |       |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |       |  |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |       |  |
| 855   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |       |  |
|   | 851.3           | 0.0                 | 1                       | 2                   | 3                     |                         |                 |    |    |     |           |     |                           |            | 851.3 | GROUND SURFACE   |
| 850   | 848.3           | 3.0                 | 4                       | 5                   | 6                     |                         |                 |    |    |     |           |     |                           |            | 848.8 | RESIDUAL<br>Orange, Fine Sandy, Silty CLAY<br>Red, Orange, and Yellow, Clayey, Fine Sandy, SILT      |
| 845   | 843.1           | 8.2                 | 2                       | 1                   | 2                     |                         |                 |    |    |     |           |     |                           |            |       |  |
| 840   | 838.1           | 13.2                | 1                       | 2                   | 1                     |                         |                 |    |    |     |           |     |                           |            | 839.3 | Red, Yellowish Brown, Tan, and Gray to Brown, Gray, and Yellow, Fine Sandy SILT with Manganese Seams |
| 835   | 833.1           | 18.2                | 2                       | 2                   | 2                     |                         |                 |    |    |     |           |     |                           |            |       |  |
| 830   | 828.1           | 23.2                | 2                       | 2                   | 2                     |                         |                 |    |    |     |           |     |                           |            |       |  |
| 825   | 823.1           | 28.2                | 2                       | 3                   | 5                     |                         |                 |    |    |     |           |     |                           |            |       |  |
| 820   | 818.1           | 33.2                | 4                       | 10                  | 13                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 815   | 813.1           | 38.2                | 6                       | 12                  | 12                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 810   | 808.1           | 43.2                | 3                       | 4                   | 8                     |                         |                 |    |    |     |           |     |                           |            |       |  |
| 805   | 803.1           | 48.2                | 9                       | 10                  | 12                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 800   | 798.1           | 53.2                | 4                       | 7                   | 13                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 795   | 793.1           | 58.2                | 19                      | 41                  | 59                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 790   | 788.1           | 63.2                | 11                      | 17                  | 20                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 785   | 783.1           | 68.2                | 16                      | 22                  | 29                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 780   | 778.1           | 73.2                | 18                      | 20                  | 24                    |                         |                 |    |    |     |           |     |                           |            |       |  |
| 775   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |       |  |

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |       |  |
|---|-----------------|---------------------|-------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|-------|--|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |                         |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |       |  |
| BORING NO. LL_B1A   |                 | STATION 336+95      |                         | OFFSET 69 ft LT     |                       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |       |  |
| COLLAR ELEV. 851.3 ft   |                 | TOTAL DEPTH 83.3 ft |                         | NORTHING 874,610    |                       | EASTING 1,776,811       |                 |    |    |     |           |     |                           |            |       |  |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     | DRILL METHOD Mud Rotary |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |            |       |  |
| DRILLER Toothman, R.  |                 | START DATE 05/30/17 |                         | COMP. DATE 05/31/17 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |       |  |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |       |  |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |       |  |
| 775   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |       |  |
|   | 773.1           | 78.2                |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            | 773.6 | CRISTALLINE ROCK<br>Tan and Gray, METAMORPHOSED GRANITE  |
| 770   | 768.1           | 83.2                |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            | 768.0 | Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 768.0 ft in CRISTALLINE ROCK (METAMORPHOSED GRANITE)<br><br>Topsoil (0.5 foot) |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITES.GPJ NC\_DOT.GDT 9/29/17



# GEOTECHNICAL BORING REPORT

## BORE LOG

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |   |      |
|---|-----------------|---------------------|-------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|---|------|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |                         |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |   |      |
| BORING NO. RL_B1A   |                 | STATION 336+73      |                         | OFFSET 14 ft RT     |                       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |   |      |
| COLLAR ELEV. 849.0 ft   |                 | TOTAL DEPTH 91.1 ft |                         | NORTHING 874,693    |                       | EASTING 1,776,833       |                 |    |    |     |           |     |                           |            |   |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     | DRILL METHOD Mud Rotary |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |            |   |      |
| DRILLER Toothman, R.  |                 | START DATE 06/01/17 |                         | COMP. DATE 06/02/17 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |   |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |   |      |
| 850   | 849.0           | 0.0                 | WOH                     | WOH                 | 2                     |                         |                 |    |    |     |           |     |                           | 849.0      | GROUND SURFACE  | 0.0  |
| 845   | 845.8           | 3.2                 | 4                       | 8                   | 10                    |                         |                 |    |    |     |           |     |                           | 842.5      | RESIDUAL<br>Orange, Yellowish, and Brown, Fine Sandy, Silty CLAY                        | 6.5  |
| 840   | 840.8           | 8.2                 | 2                       | 3                   | 4                     |                         |                 |    |    |     |           |     |                           | 832.5      | Red, Gray, and Yellow, Clayey, Fine Sandy SILT  | 16.5 |
| 835   | 835.8           | 13.2                | 2                       | 1                   | 3                     |                         |                 |    |    |     |           |     |                           | 807.5      | WEATHERED ROCK<br>Tan and Gray, METAMORPHOSED GRANITE                                   | 41.5 |
| 830   | 830.8           | 18.2                | 2                       | 1                   | 3                     |                         |                 |    |    |     |           |     |                           | 802.5      | RESIDUAL<br>Brown and Gray, Coarse to Fine Sandy SILT                                   | 46.5 |
| 825   | 825.8           | 23.2                | 2                       | 4                   | 7                     |                         |                 |    |    |     |           |     |                           | 792.5      | Gray, Silty, Fine to Coarse SAND  | 56.5 |
| 820   | 820.8           | 28.2                | 3                       | 4                   | 8                     |                         |                 |    |    |     |           |     |                           | 785.3      | WEATHERED ROCK<br>Brown, Gray, and Tan, METAMORPHOSED GRANITE with Manganese and Quartz | 63.7 |
| 815   | 815.8           | 33.2                | 5                       | 8                   | 13                    |                         |                 |    |    |     |           |     |                           | 777.7      | CRYSTALLINE ROCK<br>Tan and Gray, METAMORPHOSED GRANITE                                 | 71.3 |
| 810   | 810.8           | 38.2                | 17                      | 28                  | 40                    |                         |                 |    |    |     |           |     |                           | 775.1      | Tan and Gray, METAMORPHOSED GRANITE   | 73.9 |
| 805   | 805.8           | 43.2                | 100/0.4                 |                     |                       |                         |                 |    |    |     |           |     |                           | 772.0      | WEATHERED ROCK<br>Tan and Gray, METAMORPHOSED GRANITE                                   | 77.0 |
| 800   | 800.8           | 48.2                | 5                       | 6                   | 13                    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 795   | 795.8           | 53.2                | 8                       | 17                  | 21                    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 790   | 790.8           | 58.2                | 8                       | 10                  | 41                    |                         |                 |    |    |     |           |     |                           |            |   |      |
| 785   | 785.8           | 63.2                | 20                      | 50                  | 50/0.3                |                         |                 |    |    |     |           |     |                           |            |   |      |
| 780   | 780.8           | 68.2                | 100/0.4                 |                     |                       |                         |                 |    |    |     |           |     |                           |            |   |      |
| 775   | 777.7           | 71.3                | 60/0.0                  |                     |                       |                         |                 |    |    |     |           |     |                           |            |   |      |
| 770   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |   |      |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITES.GPJ NC\_DOT\_GDT 9/29/17

| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |   |      |
|---|-----------------|---------------------|-------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|---|------|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |                         |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |   |      |
| BORING NO. RL_B1A   |                 | STATION 336+73      |                         | OFFSET 14 ft RT     |                       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |   |      |
| COLLAR ELEV. 849.0 ft   |                 | TOTAL DEPTH 91.1 ft |                         | NORTHING 874,693    |                       | EASTING 1,776,833       |                 |    |    |     |           |     |                           |            |   |      |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     | DRILL METHOD Mud Rotary |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |            |   |      |
| DRILLER Toothman, R.  |                 | START DATE 06/01/17 |                         | COMP. DATE 06/02/17 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |   |      |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |      |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     |                           |            |   |      |
| 770   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           | 770        | Match Line  |      |
| 765   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           | 765.0      | CRYSTALLINE ROCK<br>Tan and Gray, METAMORPHOSED GRANITE (continued)                 | 84.0 |
| 760   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           | 761.7      | WEATHERED ROCK<br>Brown, METAMORPHOSED GRANITE                                      | 87.3 |
|   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           | 757.9      | CRYSTALLINE ROCK<br>Tan and Gray, METAMORPHOSED GRANITE                             | 91.1 |
|   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            | Boring Terminated at Elevation 757.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE) |      |
|   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            | Topsoil (0.4 foot)  |      |

# GEOTECHNICAL BORING REPORT

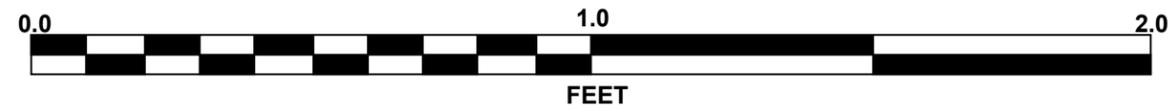
## CORE LOG

| WBS 34821.1.1   |               | TIP U-2525C         |          | COUNTY GUILFORD                                      |              | GEOLOGIST Kubinski, D.  |                 |              |     |  |            |
|---|---------------|---------------------|----------|--|--------------|-------------------------|-----------------|--------------|-----|--|------------|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |               |                     |          |  |              |                         | GROUND WTR (ft) |              |     |  |            |
| BORING NO. RL_B1A   |               | STATION 336+73      |          | OFFSET 14 ft RT                                      |              | ALIGNMENT -L-           |                 |              |     |  |            |
| COLLAR ELEV. 849.0 ft   |               | TOTAL DEPTH 91.1 ft |          | NORTHING 874,693                                     |              | EASTING 1,776,833       |                 |              |     |  |            |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |               |                     |          | DRILL METHOD Mud Rotary                              |              | HAMMER TYPE Automatic   |                 |              |     |  |            |
| DRILLER Toothman, R.  |               | START DATE 06/01/17 |          | COMP. DATE 06/02/17                                  |              | SURFACE WATER DEPTH N/A |                 |              |     |  |            |
| CORE SIZE NQ  |               | TOTAL RUN 19.8 ft   |          |  |              |                         |                 |              |     |  |            |
| ELEV (ft)   | RUN ELEV (ft) | DEPTH (ft)          | RUN (ft) | DRILL RATE (Min/ft)                                  | RUN          |                         | STRATA          |              | LOG | DESCRIPTION AND REMARKS  | DEPTH (ft) |
|   |               |                     |          |  | REC. (ft) %  | RQD (ft) %              | REC. (ft) %     | RQD (ft) %   |     |  |            |
| 777.7   | 777.7         | 71.3                | 4.8      | N=60/0.0<br>2:29/0.8<br>2:56<br>3:42<br>2:02<br>2:15 | (2.6)<br>54% | (1.1)<br>23%            | (2.6)<br>100%   | (1.1)<br>42% |     | Begin Coring @ 71.3 ft   | 71.3       |
| 775   | 772.9         | 76.1                | 5.0      | 2:12<br>2:26<br>2:46<br>2:44<br>2:04                 | (4.1)<br>82% | (2.7)<br>54%            | (7.0)<br>100%   | (4.5)<br>64% |     | Moderate to Moderately Severe Weathering, Moderately Hard to Medium Hard, Tan and Gray METAMORPHOSED GRANITE with Close to Very Close Fracture Spacing                   | 73.9       |
| 770   | 767.9         | 81.1                | 5.0      | 2:35<br>2:48<br>2:36<br>4:55<br>4:46                 | (3.0)<br>60% | (1.8)<br>36%            | (0.1)<br>3%     | N/A          |     | GSI 25 to 45<br>7 Fractures at 0 to 20 Degrees   | 77.0       |
| 765   | 762.9         | 86.1                | 5.0      | 2:31<br>3:24<br>2:07<br>3:14<br>3:25                 | (3.8)<br>76% | (1.2)<br>24%            | (3.8)<br>100%   | (1.2)<br>32% |     | SEVERE WEATHERING, SOFT, TAN AND GRAY METAMORPHOSED GRANITE  | 78.0       |
| 760   | 757.9         | 91.1                |          |  |              |                         |                 |              |     | Moderate to Moderately Severe Weathering, Moderately Hard to Medium Hard, Tan and Gray METAMORPHOSED GRANITE with Close to Very Close Fracture Spacing, Quartz Injection | 84.0       |
|   |               |                     |          |  |              |                         |                 |              |     | GSI 40 to 60<br>7 Fractures at 0 to 10 Degrees<br>4 Fractures at 40 to 60 Degrees  | 87.3       |
|   |               |                     |          |  |              |                         |                 |              |     | SEVERE WEATHERING, SOFT TO VERY SOFT, BROWN, METAMORPHOSED GRANITE   | 91.1       |
|   |               |                     |          |  |              |                         |                 |              |     | Moderate to Moderately Severe Weathering, Moderately Hard to Medium Hard, Tan and Gray METAMORPHOSED GRANITE with Close to Very Close Fracture Spacing, Quartz Injection |            |
|   |               |                     |          |  |              |                         |                 |              |     | GSI 20 to 40<br>3 Fractures at 0 to 10 Degrees<br>3 Fractures at 20 to 40 Degrees<br>3 Fractures at 50 to 70 Degrees   |            |
|   |               |                     |          |  |              |                         |                 |              |     | Boring Terminated at Elevation 757.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)  |            |
|   |               |                     |          |  |              |                         |                 |              |     | Topsoil (0.4 foot)   |            |

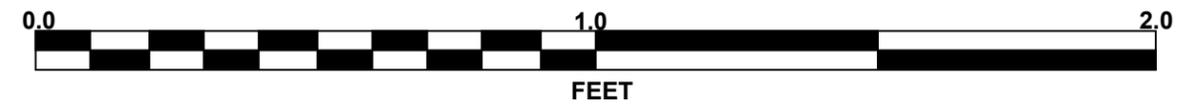
NCDOT CORE DOUBLE U2525C\_GEO\_BRDG\_SITE5.GPJ NC\_DOT\_GDT 9/29/17

# CORE PHOTOGRAPHS

**RL\_B1A**  
BOX 1: 71.3 to 86.1 FEET



**RL\_B1A**  
BOX 2: 86.1 to 91.1 FEET





# GEOTECHNICAL BORING REPORT BORE LOG

# GEOTECHNICAL BORING REPORT CORE LOG

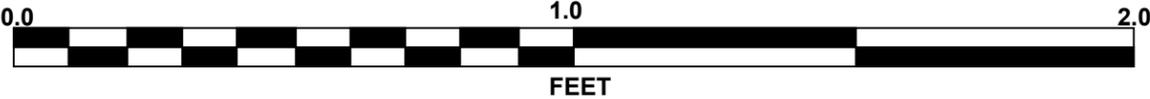
| WBS 34821.1.1   |                 | TIP U-2525C         |                         | COUNTY GUILFORD     |                       | GEOLOGIST Kubinski, D.  |                 |    |    |     |           |     |                           |            |      |   |
|---|-----------------|---------------------|-------------------------|---------------------|-----------------------|-------------------------|-----------------|----|----|-----|-----------|-----|---------------------------|------------|------|---|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                 |                     |                         |                     |                       |                         | GROUND WTR (ft) |    |    |     |           |     |                           |            |      |   |
| BORING NO. LL_B2A   |                 | STATION 338+06      |                         | OFFSET 74 ft LT     |                       | ALIGNMENT -L-           |                 |    |    |     |           |     |                           |            |      |   |
| COLLAR ELEV. 837.8 ft   |                 | TOTAL DEPTH 60.9 ft |                         | NORTHING 874,606    |                       | EASTING 1,776,700       |                 |    |    |     |           |     |                           |            |      |   |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                 |                     | DRILL METHOD Mud Rotary |                     | HAMMER TYPE Automatic |                         |                 |    |    |     |           |     |                           |            |      |   |
| DRILLER Toothman, R.  |                 | START DATE 05/17/17 |                         | COMP. DATE 05/18/17 |                       | SURFACE WATER DEPTH N/A |                 |    |    |     |           |     |                           |            |      |   |
| ELEV (ft)   | DRIVE ELEV (ft) | DEPTH (ft)          | BLOW COUNT              |                     |                       | BLOWS PER FOOT          |                 |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |      |   |
|   |                 |                     | 0.5ft                   | 0.5ft               | 0.5ft                 | 0                       | 25              | 50 | 75 | 100 |           |     | ELEV. (ft)                | DEPTH (ft) |      |   |
| 840   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |      |   |
|   | 837.8           | 0.0                 | 1                       | 2                   | 3                     |                         |                 |    |    |     |           |     |                           | 837.8      | 0.0  | GROUND SURFACE  |
|   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |      | <b>RESIDUAL</b>   |
| 835   | 834.7           | 3.1                 | 6                       | 7                   | 8                     |                         |                 |    |    |     |           |     |                           | 835.3      | 2.5  | Yellowish Brown, Fine Sandy, Silty CLAY   |
|   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           |            |      | Yellowish Brown and Gray, Clayey, Fine Sandy SILT   |
| 830   | 829.7           | 8.1                 | 6                       | 8                   | 12                    |                         |                 |    |    |     |           |     |                           | 829.2      | 8.8  | Yellowish Brown and Gray, Silty, Fine to Coarse SAND  |
| 825   | 824.7           | 13.1                | 3                       | 5                   | 7                     |                         |                 |    |    |     |           |     |                           |            |      |   |
| 820   | 819.7           | 18.1                | 9                       | 14                  | 16                    |                         |                 |    |    |     |           |     |                           |            |      |   |
| 815   | 814.7           | 23.1                | 11                      | 10                  | 15                    |                         |                 |    |    |     |           |     |                           |            |      |   |
| 810   | 809.7           | 28.1                | 30                      | 60                  | 40/0.2                |                         |                 |    |    |     |           |     |                           | 809.2      | 28.6 | <b>WEATHERED ROCK</b><br>Yellowish Brown, Tan, Gray, and Brown, METAMORPHOSED GRANITE                         |
| 805   | 804.7           | 33.1                | 78                      | 22/0.1              |                       |                         |                 |    |    |     |           |     |                           |            |      |   |
| 800   | 799.7           | 38.1                | 40                      | 60/0.3              |                       |                         |                 |    |    |     |           |     |                           |            |      |   |
| 795   | 794.7           | 43.1                | 65                      | 35/0.2              |                       |                         |                 |    |    |     |           |     |                           |            |      |   |
| 790   | 789.7           | 48.1                | 100/0.3                 |                     |                       |                         |                 |    |    |     |           |     |                           |            |      |   |
| 785   | 784.7           | 53.1                | 60/0.0                  |                     |                       |                         |                 |    |    |     |           |     |                           | 784.7      | 53.1 | <b>CRYSTALLINE ROCK</b><br>Tan and Gray, METAMORPHOSED GRANITE  |
| 780   |                 |                     |                         |                     |                       |                         |                 |    |    |     |           |     |                           | 776.9      | 60.9 | Boring Terminated at Elevation 776.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)<br><br>Topsoil (0.7 foot) |

| WBS 34821.1.1  |               | TIP U-2525C         |                         | COUNTY GUILFORD                      |                       | GEOLOGIST Kubinski, D.  |                 |
|--|---------------|---------------------|-------------------------|--------------------------------------|-----------------------|-------------------------|-----------------|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2)  |               |                     |                         |                                      |                       |                         | GROUND WTR (ft) |
| BORING NO. LL_B2A  |               | STATION 338+06      |                         | OFFSET 74 ft LT                      |                       | ALIGNMENT -L-           |                 |
| COLLAR ELEV. 837.8 ft  |               | TOTAL DEPTH 60.9 ft |                         | NORTHING 874,606                     |                       | EASTING 1,776,700       |                 |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017   |               |                     | DRILL METHOD Mud Rotary |                                      | HAMMER TYPE Automatic |                         |                 |
| DRILLER Toothman, R.   |               | START DATE 05/17/17 |                         | COMP. DATE 05/18/17                  |                       | SURFACE WATER DEPTH N/A |                 |
| CORE SIZE NQ   |               | TOTAL RUN 7.8 ft    |                         | DESCRIPTION AND REMARKS              |                       |                         |                 |
| ELEV (ft)  | RUN ELEV (ft) | DEPTH (ft)          | RUN (ft)                | DRILL RATE (Min/ft)                  | RUN REC. (%)          | RQD (%)                 | SAMP. NO.       |
| 784.7  | 784.7         | 53.1                | 2.8                     | N=60/0.0<br>1:35/0.8<br>1:33<br>1:34 | (1.2)<br>43%          | (0.0)<br>0%             |                 |
|  | 781.9         | 55.9                | 5.0                     | 3:21<br>2:46<br>3:20<br>2:51<br>1:30 | (3.3)<br>66%          | (0.4)<br>8%             |                 |
| 780  |               |                     |                         |                                      |                       |                         |                 |
|  | 776.9         | 60.9                |                         |                                      |                       |                         |                 |
| Begin Coring @ 53.1 ft<br><b>CRYSTALLINE ROCK</b><br>Moderately Severe Weathering, Medium Hard, Tan and Gray, METAMORPHOSED GRANITE with Close to Very Close Fracture Spacing<br>GSI 10 to 30<br>6 Fractures at 0 to 10 Degrees<br>Boring Terminated at Elevation 776.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)<br>Topsoil (0.7 foot) |               |                     |                         |                                      |                       |                         |                 |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITES.GPJ NC\_DOT.GDT 9/29/17

# CORE PHOTOGRAPHS

**LL\_B2A**  
BOX 1: 53.1 to 60.9 FEET





# GEOTECHNICAL BORING REPORT

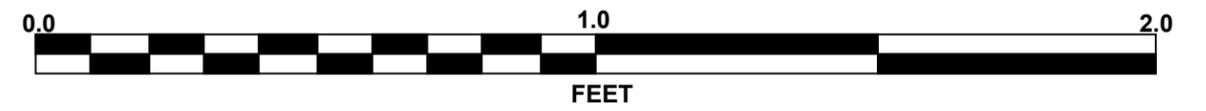
## CORE LOG

| WBS 34821.1.1   |               | TIP U-2525C         |          | COUNTY GUILFORD              |              | GEOLOGIST Kubinski, D.  |                 |              |     |  |            |
|---|---------------|---------------------|----------|------------------------------|--------------|-------------------------|-----------------|--------------|-----|--|------------|
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |               |                     |          |                              |              |                         | GROUND WTR (ft) |              |     |  |            |
| BORING NO. LL_B2B   |               | STATION 337+95      |          | OFFSET 7 ft LT               |              | ALIGNMENT -L-           |                 |              |     |  |            |
| COLLAR ELEV. 840.8 ft   |               | TOTAL DEPTH 71.1 ft |          | NORTHING 874,673             |              | EASTING 1,776,711       |                 |              |     |  |            |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |               |                     |          | DRILL METHOD Mud Rotary      |              | HAMMER TYPE Automatic   |                 |              |     |  |            |
| DRILLER Toothman, R.  |               | START DATE 05/18/17 |          | COMP. DATE 05/19/17          |              | SURFACE WATER DEPTH N/A |                 |              |     |  |            |
| CORE SIZE NQ  |               | TOTAL RUN 7.5 ft    |          |                              |              |                         |                 |              |     |  |            |
| ELEV (ft)   | RUN ELEV (ft) | DEPTH (ft)          | RUN (ft) | DRILL RATE (Min/ft)          | RUN          |                         | STRATA          |              | LOG | DESCRIPTION AND REMARKS  | DEPTH (ft) |
|   |               |                     |          |                              | REC. (ft) %  | RQD (ft) %              | REC. (ft) %     | RQD (ft) %   |     |  |            |
| 777.2   | 777.2         | 63.6                | 3.0      | 2:16<br>2:34<br>6:58         | (2.4)<br>80% | (1.1)<br>37%            | (6.2)<br>83%    | (2.1)<br>30% |     | Continued from previous page   |            |
| 775   | 774.2         | 66.6                | 4.5      | 3:21<br>2:46<br>3:34<br>2:32 | (3.8)<br>84% | (1.0)<br>22%            |                 |              |     | <p style="text-align: center;"><b>CRYSTALLINE ROCK</b></p> <p>Moderate to Moderately Severe Weathering, Moderately Hard to Medium Hard, Tan and Gray METAMORPHOSED GRANITE with Close to Very Close Fracture Spacing, Quartz Injection</p> <p style="text-align: center;">GSI 20 to 40<br/>3 Fractures at 10 to 20 Degrees<br/>8 Fractures at 60 to 70 Degrees</p> <p>Weathered Rock Seams Present From 66.0 to 66.6 feet and 70.4 and 71.1 feet <i>(continued)</i></p> <p>Boring Terminated at Elevation 769.7 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)</p> <p style="text-align: center;">Topsoil (0.4 foot)</p> |            |
| 770   | 769.7         | 71.1                |          | 5:22/0.5                     |              |                         |                 |              |     |  |            |

NCDOT CORE DOUBLE U2525C\_GEO\_BRDG\_SITE5.GPJ NC\_DOT.GDT 9/29/17

# CORE PHOTOGRAPHS

**LL\_B2B**  
BOX 1: 63.6 to 71.1 FEET



# GEOTECHNICAL BORING REPORT

## BORE LOG

|  |                            |                                |                                |
|--|----------------------------|--------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.1   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD         | <b>GEOLOGIST</b> Kubinski, D.  |
| <b>SITE DESCRIPTION</b> Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                            |                                | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> RL_B2A   | <b>STATION</b> 337+85      | <b>OFFSET</b> 27 ft RT         | <b>ALIGNMENT</b> -L-           |
| <b>COLLAR ELEV.</b> 840.9 ft   | <b>TOTAL DEPTH</b> 66.0 ft | <b>NORTHING</b> 874,707        | <b>EASTING</b> 1,776,721       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> TRI0055 CME-55 81% 02/20/2017  |                            | <b>DRILL METHOD</b> Mud Rotary | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> Toothman, R.  | <b>START DATE</b> 05/18/17 | <b>COMP. DATE</b> 05/22/17     | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |        |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION | DEPTH (ft) |   |
|-----------|-----------------|------------|------------|--------|-------|----------------|----|----|----|-----|-----------|-----|---------------------------|------------|---|
|           |                 |            | 0.5ft      | 0.5ft  | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     |                           |            |   |
| 845       |                 |            |            |        |       |                |    |    |    |     |           |     |                           |            |   |
| 840       | 840.9           | 0.0        | 2          | 2      | 3     |                |    |    |    |     |           |     |                           | 840.9      | GROUND SURFACE  |
| 835       | 837.8           | 3.1        | 6          | 11     | 14    |                |    |    |    |     |           |     |                           |            | <b>RESIDUAL</b><br>Yellowish Brown and Gray, Fine to Coarse Sandy, Silty CLAY                                 |
| 830       | 832.8           | 8.1        | 2          | 2      | 2     |                |    |    |    |     |           |     |                           |            | Brown to Gray, Clayey, Fine Sandy SILT with Manganese   |
| 825       | 827.8           | 13.1       | 3          | 5      | 4     |                |    |    |    |     |           |     |                           |            | Yellowish Brown and Gray, Silty, Fine to Coarse SAND  |
| 820       | 822.8           | 18.1       | 2          | 5      | 6     |                |    |    |    |     |           |     |                           |            |   |
| 815       | 817.8           | 23.1       | 4          | 6      | 9     |                |    |    |    |     |           |     |                           |            |   |
| 810       | 812.8           | 28.1       | 9          | 12     | 21    |                |    |    |    |     |           |     |                           |            |   |
| 805       | 807.8           | 33.1       | 17         | 25     | 69    |                |    |    |    |     |           |     |                           |            |   |
| 800       | 802.8           | 38.1       | 100/0.2    |        |       |                |    |    |    |     |           |     |                           |            | <b>WEATHERED ROCK</b><br>Gray, Tan, and Brown, METAMORPHOSED GRANITE  |
| 795       | 797.8           | 43.1       | 75         | 25/0.2 |       |                |    |    |    |     |           |     |                           |            |   |
| 790       | 792.8           | 48.1       | 100/0.5    |        |       |                |    |    |    |     |           |     |                           |            |   |
| 785       | 787.8           | 53.1       | 60/0.1     |        |       |                |    |    |    |     |           |     |                           |            | <b>CRYSTALLINE ROCK</b><br>Tan and Gray, METAMORPHOSED GRANITE  |
| 780       |                 |            |            |        |       |                |    |    |    |     |           |     |                           |            |   |
| 775       |                 |            |            |        |       |                |    |    |    |     |           |     |                           |            | Boring Terminated at Elevation 774.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)<br><br>Topsoil (0.7 foot) |

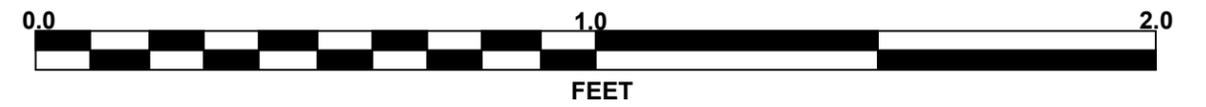
NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITES.GPJ NC\_DOT.GDT 9/29/17

|  |                            |                                |                                |
|--|----------------------------|--------------------------------|--------------------------------|
| <b>WBS</b> 34821.1.1   | <b>TIP</b> U-2525C         | <b>COUNTY</b> GUILFORD         | <b>GEOLOGIST</b> Kubinski, D.  |
| <b>SITE DESCRIPTION</b> Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                            |                                | <b>GROUND WTR (ft)</b>         |
| <b>BORING NO.</b> RL_B2A   | <b>STATION</b> 337+85      | <b>OFFSET</b> 27 ft RT         | <b>ALIGNMENT</b> -L-           |
| <b>COLLAR ELEV.</b> 840.9 ft   | <b>TOTAL DEPTH</b> 66.0 ft | <b>NORTHING</b> 874,707        | <b>EASTING</b> 1,776,721       |
| <b>DRILL RIG/HAMMER EFF./DATE</b> TRI0055 CME-55 81% 02/20/2017  |                            | <b>DRILL METHOD</b> Mud Rotary | <b>HAMMER TYPE</b> Automatic   |
| <b>DRILLER</b> Toothman, R.  | <b>START DATE</b> 05/18/17 | <b>COMP. DATE</b> 05/22/17     | <b>SURFACE WATER DEPTH</b> N/A |

| ELEV (ft) | RUN ELEV (ft) | DEPTH (ft) | RUN (ft) | DRILL RATE (Min/ft)                  | TOTAL RUN    |              | SAMP. NO. | STRATA       |              | LOG | DESCRIPTION AND REMARKS   |
|-----------|---------------|------------|----------|--------------------------------------|--------------|--------------|-----------|--------------|--------------|-----|---|
|           |               |            |          |                                      | REC. (ft) %  | RQD (ft) %   |           | REC. (ft) %  | RQD (ft) %   |     |   |
| 787.7     | 787.7         | 53.2       | 2.8      | 1:08/0.8<br>1:31<br>1:52             | (2.4)<br>86% | (1.9)<br>68% |           | (9.1)<br>71% | (6.2)<br>48% |     | Continued from previous page  |
| 785       | 784.9         | 56.0       | 5.0      | 2:16<br>2:19<br>3:09<br>2:49<br>2:56 | (3.0)<br>60% | (1.2)<br>24% |           |              |              |     | <b>CRYSTALLINE ROCK</b><br>Moderate to Moderately Severe Weathering, Moderately Hard to Medium Hard, Tan and Gray METAMORPHOSED GRANITE with Moderately Close to Very Close Fracture Spacing<br><br>GSI 30 to 50<br>7 Fractures at 0 to 20 Degrees<br>6 Fractures at 60 to 80 Degrees (continued) |
| 780       | 779.9         | 61.0       | 5.0      | 2:27<br>2:15<br>2:16<br>1:27<br>1:03 | (3.7)<br>74% | (3.1)<br>62% |           |              |              |     |   |
| 775       | 774.9         | 66.0       |          |                                      |              |              |           |              |              |     | Boring Terminated at Elevation 774.9 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE)<br><br>Topsoil (0.7 foot)   |

# CORE PHOTOGRAPHS

**RL\_B2A**  
BOX 1: 53.2 to 66.0 FEET



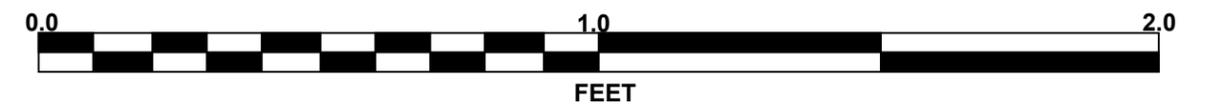
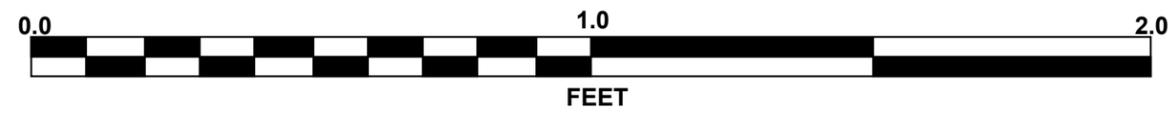


# CORE PHOTOGRAPHS

**RL\_B2B**  
BOX 1: 48.1 to 62.5 FEET



**RL\_B2B**  
BOX 2: 62.5 to 65.9 FEET





# GEOTECHNICAL BORING REPORT

## BORE LOG

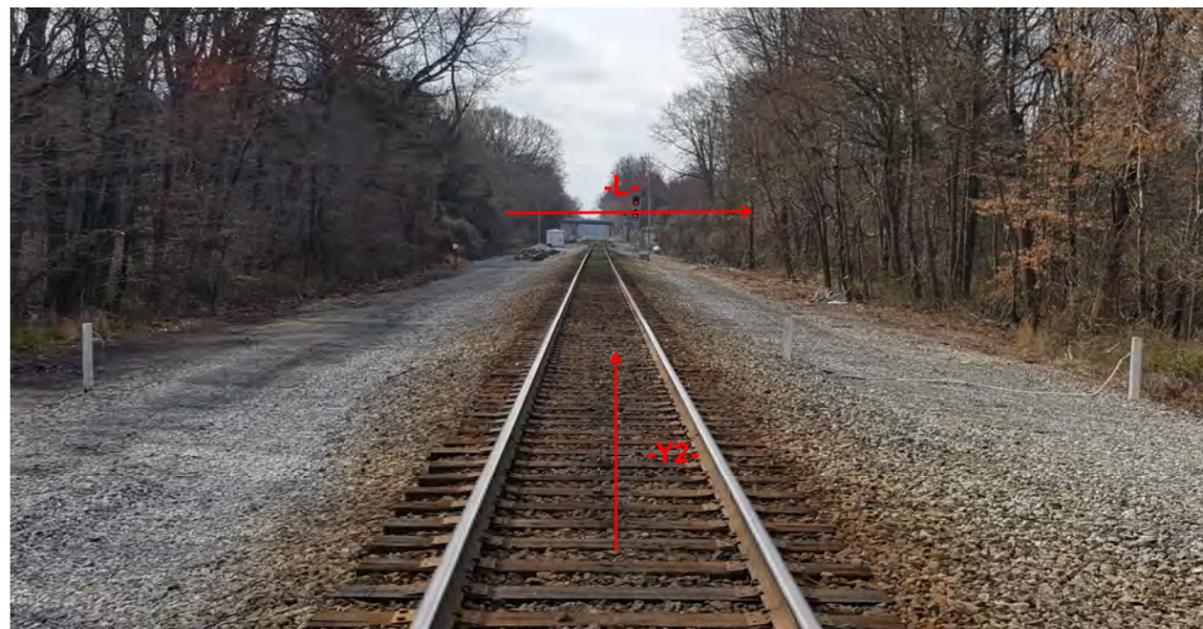
|   |                     |                         |                              |
|---|---------------------|-------------------------|------------------------------|
| WBS 34821.1.1   | TIP U-2525C         | COUNTY GUILFORD         | GEOLOGIST Kubinski, D.       |
| SITE DESCRIPTION Site #3 (Structure #4 & #5) - Bridge No. 1243 and 1244 on I-85 Bypass (-L-) over Norfolk Southern Railroad (-Y2) |                     |                         | GROUND WTR (ft)              |
| BORING NO. RL_EB2B  | STATION 337+97      | OFFSET 77 ft RT         | ALIGNMENT -L- 0 HR. 2.2      |
| COLLAR ELEV. 837.9 ft   | TOTAL DEPTH 48.6 ft | NORTHING 874,757        | EASTING 1,776,709 24 HR. 0.5 |
| DRILL RIG/HAMMER EFF./DATE TRI0055 CME-55 81% 02/20/2017  |                     | DRILL METHOD Mud Rotary | HAMMER TYPE Automatic        |
| DRILLER Toothman, R.  | START DATE 05/15/17 | COMP. DATE 05/15/17     | SURFACE WATER DEPTH N/A      |

| ELEV (ft) | DRIVE ELEV (ft) | DEPTH (ft) | BLOW COUNT |       |       | BLOWS PER FOOT |    |    |    |     | SAMP. NO. | LOG | SOIL AND ROCK DESCRIPTION |            |      |  |
|-----------|-----------------|------------|------------|-------|-------|----------------|----|----|----|-----|-----------|-----|---------------------------|------------|------|--|
|           |                 |            | 0.5ft      | 0.5ft | 0.5ft | 0              | 25 | 50 | 75 | 100 |           |     | ELEV. (ft)                | DEPTH (ft) |      |  |
| 840       |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      |  |
|           | 837.9           | 0.0        | 1          | 1     | 1     |                |    |    |    |     |           |     |                           | 837.9      | 0.0  | GROUND SURFACE   |
| 835       | 834.4           | 3.5        | 9          | 12    | 11    |                |    |    |    |     |           |     |                           |            |      | <b>RESIDUAL</b><br>Yellowish Brown and Gray, Coarse to Fine Sandy, Silty CLAY  |
| 830       | 829.4           | 8.5        | 3          | 2     | 3     |                |    |    |    |     |           |     |                           | 831.4      | 6.5  | Gray, Brown, and White, Silty, Fine to Coarse SAND   |
| 825       | 824.4           | 13.5       | 4          | 5     | 5     |                |    |    |    |     |           |     |                           |            |      |  |
| 820       | 819.4           | 18.5       | 5          | 5     | 7     |                |    |    |    |     |           |     |                           |            |      |  |
| 815       | 814.4           | 23.5       | 7          | 7     | 5     |                |    |    |    |     |           |     |                           |            |      |  |
| 810       | 809.4           | 28.5       | 10         | 10    | 12    |                |    |    |    |     |           |     |                           |            |      |  |
| 805       | 804.4           | 33.5       | 23         | 30    | 56    |                |    |    |    |     |           |     |                           |            |      |  |
| 800       | 799.4           | 38.5       | 100/0.3    |       |       |                |    |    |    |     |           |     |                           | 801.4      | 36.5 | <b>WEATHERED ROCK</b><br>Brown and Gray, METAMORPHOSED GRANITE   |
| 795       | 794.4           | 43.5       | 100/0.3    |       |       |                |    |    |    |     |           |     |                           |            |      |  |
| 790       | 789.4           | 48.5       | 60/0.1     |       |       |                |    |    |    |     |           |     |                           | 789.4      | 48.5 | <b>CRYSTALLINE ROCK</b><br>METAMORPHOSED GRANITE   |
|           |                 |            |            |       |       |                |    |    |    |     |           |     |                           | 789.3      | 48.6 | Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 789.3 ft in CRYSTALLINE ROCK (METAMORPHOSED GRANITE) |
|           |                 |            |            |       |       |                |    |    |    |     |           |     |                           |            |      | Topsail (0.6 foot)   |

NCDOT BORE DOUBLE U2525C\_GEO\_BRDG\_SITE5.GPJ NC\_DOT.GDT 9/29/17



SITE PHOTOGRAPHS



View Looking South along -Y2- from Hillcroft Road



View Looking West on East Side of Bridge along -L-